

## **Department of Energy**

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## DEC 1 1 2015

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Mr. Brian Begley Federal Facility Agreement Manager Division of Waste Management Kentucky Department for Environmental Protection 200 Fair Oaks Lane, 2nd Floor Frankfort, Kentucky 40601

Ms. Julie Corkran U.S. Environmental Protection Agency, Region 4 Federal Facilities Branch 61 Forsyth Street Atlanta, Georgia 30303

Dear Mr. Begley and Ms. Corkran:

## ADDENDUM TO FINAL CHARACTERIZATION REPORT FOR SOLID WASTE MANAGEMENT UNITS 211-A AND 211-B VOLATILE ORGANIC COMPOUND SOURCES FOR THE SOUTHWEST GROUNDWATER PLUME AT THE PADUCAH GASEOUS DIFFUSION PLANT, PADUCAH, KENTUCKY, DOE/LX/07-1288&D2/A1

Enclosed find for your review and approval the subject document, Addendum to Final Characterization Report for Solid Waste Management Units 211-A and 211-B Volatile Organic Compound Sources for the Southwest Groundwater Plume at the Paducah Gaseous Diffusion Plant, Paducah, Kentucky, DOE/LX/07-1288&D2/A1. The Addendum documents results of Regional Gravel Aquifer groundwater sampling in the area of the C-720 Maintenance and Stores Building.

If you have any questions or require additional information, please contact David Dollins at (270) 441-6819.

Sincerely,

-Tracey Duncan Federal Facility Agreement Manager Portsmouth/Paducah Project Office

Enclosure:

Addendum to the SWMUs 211-A and 211-B Final Characterization Report

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# **CLEARED FOR PUBLIC RELEASE**

## Addendum to the Final Characterization Report for Solid Waste Management Units 211-A and 211-B Volatile Organic Compound Sources for the Southwest Groundwater Plume at the Paducah Gaseous Diffusion Plant, Paducah, Kentucky

Date Issued—December 2015

U.S. DEPARTMENT OF ENERGY Office of Environmental Management

Prepared by FLUOR FEDERAL SERVICES, INC., Paducah Deactivation Project managing the Deactivation Project at the Paducah Gaseous Diffusion Plant under Task Order DE-DT0007774

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# ACRONYMS

CSM	conceptual site model
Dhc	Dehalococcoides mccartyi
DNAPL	dense nonaqueous-phase liquid
DOE	U.S. Department of Energy
DPT	direct push technology
DQO	data quality objective
DSS	Decision Support Software
EPA	U.S. Environmental Protection Agency
EVS-ES	Environmental Visualization Systems Expert System
FCR	final characterization report
FFS	focused feasibility study
GSD	grain size distribution
HU	hydrogeologic unit
ID	inside diameter
KOW	Kentucky Ordnance Works
LATA Kentucky	LATA Environmental Services of Kentucky, LLC
LCD	Lower Continental Deposits
LCS	laboratory control sample
LCSD	laboratory control sample duplicate
LUC	land use control
MCL	maximum contaminant level
MS	matrix spike
MSD	matrix spike duplicate
MW	monitoring well
OREIS	Oak Ridge Environmental Information System
OU	operable unit
PGDP	Paducah Gaseous Diffusion Plant
PID	photoionization detector
QAPP	quality assurance program plan
RDWP	remedial design work plan
RDSI	remedial design support investigation
RPD	relative percent difference
RGA	Regional Gravel Aquifer
RI	remedial investigation
ROD	record of decision
SI	site investigation
SWMU	solid waste management unit
UCD	Upper Continental Deposits
UCRS	Upper Continental Recharge System
VC	vinyl chloride
VOC	volatile organic compound
WAG	waste area group

## **EXECUTIVE SUMMARY**

This Final Characterization Report (FCR) presents the results of the remedial design support investigation (RDSI) for solid waste management units (SWMUs) 211-A and 211-B. Requirements for the RDSI are outlined in the Remedial Design Work Plan for Solid Waste Management Units 1, 211-A, 211-B, Volatile Organic Compound Sources for the Southwest Groundwater Plume at the Paducah Gaseous Diffusion Plant, Paducah, Kentucky (DOE 2012a) (RDWP). The RDSI was performed to better determine the lateral and vertical extent and distribution of volatile organic compounds (VOCs) and source material in the Southwest Plume source areas and to determine soil and groundwater parameters, including geochemical parameters, at each of the SWMUs to be used to design *in situ* bioremediation, if this alternative is selected. Soil sampling focused on soils in hydrogeologic units (HUs) HU1, HU2, HU3, and HU4 within the Upper Continental Deposits (UCD) and previously identified potential trichloroethene (TCE) source areas northeast and southeast of the C-720 Building. The Focused Feasibility Study (DOE 2011) identified a number of alternatives to remediate SWMU 211-A and 211-B, but ultimately concluded that the appropriate alternative would require an RDSI to provide sufficient information as a basis to select a remedial alternative. The selected remedy, as identified in the Record of Decision (ROD) for SWMUs 211-A and 211-B, pending this final characterization of source extent and magnitude, is enhanced in situ bioremediation with interim land use controls (LUCs) (Alternative 8) or long-term monitoring with interim LUCs (Alternative 2).

## SWMU 211-A RDSI SUMMARY

Soil samples were collected from 42 boring locations at SWMU 211-A (Figure ES.1). [Note: the RDWP (DOE 2012a) allotted a total of up to 41 planned and contingency soil borings to characterize TCE levels in soil at SWMU 211-A. DOE sampled an additional soil boring to better characterize the extent of the VOC contamination.] Between 12 and 13 soil samples were collected and analyzed at each boring. Grain size distribution (GSD) analysis was performed on select soil samples. Soil sample analytical results, which were used to further evaluate the magnitude and extent of VOCs at SWMU 211-A, are summarized below.

- The average soil boring TCE concentration (based upon the 12 to 13 collected soil samples per soil boring location) was 122 micrograms per kilogram ( $\mu$ g/kg), exceeding the TCE soil remediation goal of 75  $\mu$ g/kg as identified in the RDWP (DOE 2012a). The maximum individual soil sample TCE concentration detected was 4,800  $\mu$ g/kg. The areal extent of TCE is defined to the east, west, north, and south.
- Average TCE levels in soil exceeded the remediation goal (75 µg/kg) in 12 of the 42 soil borings (29%). The average TCE level among all samples in these 12 soil borings was 380 µg/kg.<sup>1</sup>

Using the three-dimensional analysis software Environmental Visualization Systems Expert System (EVS-ES) and a 90% maximum source volume confidence level statistical evaluation, the estimated total TCE volume is approximately 2.2 gal over an areal extent of approximately 34,000 square feet ( $ft^2$ ) area. The area of 90% confidence level that TCE levels exceed 75 µg/kg in part of the soil column extends a maximum of 140 ft in the north-to-south direction (plant coordinate system) and 350 ft in the east-to-west direction (plant coordinate system).

<sup>&</sup>lt;sup>1</sup> The average TCE level among all samples excludes the lower analysis for depth intervals where duplicate analyses are available and uses one-half of the laboratory reporting limit for "U" qualified analyses.

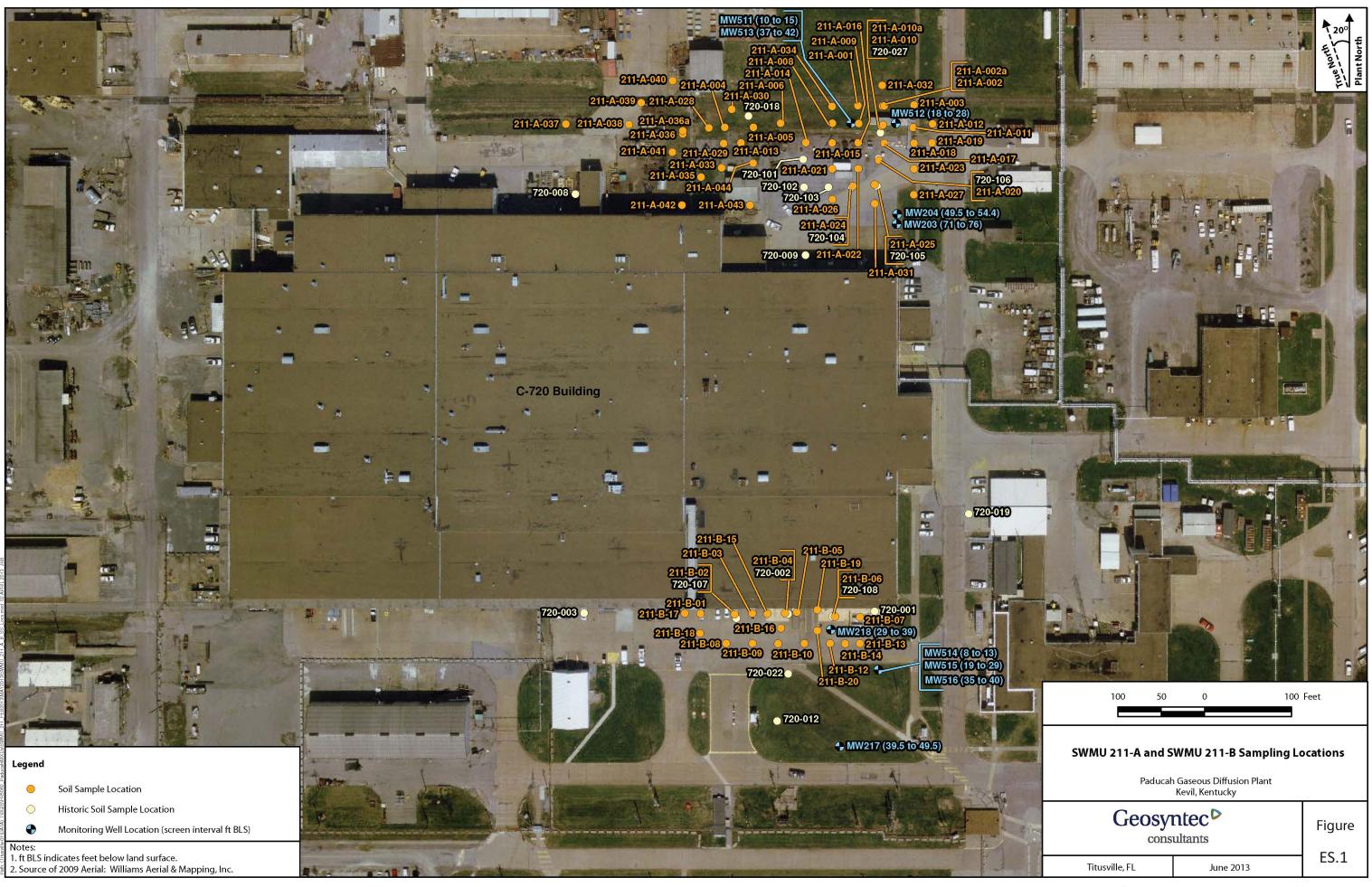


Figure ES.1. SWMU 211-A and SWMU 211-B Sampling Locations

- 1,1-dichloroethene (1,1-DCE) was the only other VOC to exceed its groundwater protection remediation goal as identified in the RDWP (DOE 2012a). Average 1,1-DCE levels in soil exceeded the remediation goal (137  $\mu$ g/kg) in 6 of the 42 soil borings (14%).
- The average soil boring 1,1-DCE concentration (based upon the 12 to 13 collected soil samples per soil boring location) among all SWMU 211-A RDSI soil borings was 94  $\mu$ g/kg. The maximum individual soil sample 1,1-DCE concentration detected was 4,400  $\mu$ g/kg. 1,1-DCE was primarily detected in the western portion of the 211-A area and may be attributable to a separate historic release of 1,1,1-trichloroethane (1,1,1-TCA) since 1,1-DCE is an abiotic degradation product of 1,1,1-TCA.
- The area of 1,1-DCE levels that exceed 137  $\mu$ g/kg in part of the soil column is approximately 18,000 ft<sup>2</sup>, a subset of the area of TCE contamination as defined above and wholly contained within the area of TCE contamination.
- The average soil boring *cis*-1,2-DCE, *trans*-1,2-DCE, and vinyl chloride (VC) concentrations did not exceed their respective soil remediation goals.
- The VOC levels in soil define two discrete areas of greater contaminant levels: an east area of TCE contamination, within and south of the previously identified SWMU 211-A boundary, and a west area of both TCE and 1,1-DCE, outside of the previously identified SWMU 211-A boundary.

Groundwater samples were collected from five monitoring wells (MWs) at SWMU 211-A. Groundwater sample results are summarized in Table ES-1. (Preexisting MWs were sampled three times and RDSI-installed wells were sampled once.) To estimate the total TCE mass in soil and the extent of TCE soil impacts at SWMU 211-A, the RDSI soil TCE data and all historical soil TCE data for the SWMU 211-A investigation area in the Oak Ridge Environmental Information System (OREIS) were interpolated using the software Environmental Visualization Systems Expert System (EVS-ES) and a 90% maximum source volume confidence level statistical evaluation.

LATA Environmental Services of Kentucky (LATA Kentucky) completed an RDSI HU hydrologic analysis to aid in the understanding of injection capacity in the event *in situ* bioremediation is selected as the final remedy for SWMU 211-A. Soil conditions at SWMU 211-A appear to be consistent with the requirements associated with an injection-dependent technology. Flexible wall permeameter tests (ASTM D5084-10) and GSD analyses (ASTM D422) were performed at nine locations. The calculated average hydraulic conductivity values ranged from 5.5E-10 cm/s to 3.8E-7 cm/s. RDSI nested-well injection testing also was performed to assess the hydraulic conductivity of the HU1, HU2, and HU3 formations. The injection testing average hydraulic conductivities were 4.4E-5 cm/s, 1.5E-5 cm/s, and 7.9E-6 cm/s for the HU1, HU2, and HU3 formations, respectively.

## SWMU 211-B RDSI SUMMARY

Soil samples were collected at 19 boring locations at SWMU 211-B (Figure ES.1). [For reference, the RDWP (DOE 2012a) allotted a total of up to 23 planned and contingency soil borings to characterize TCE levels in soil at SWMU 211-B.] Thirteen soil samples were collected and analyzed at each boring. GSD analysis was performed on select soil samples. Soil sample analytical results that were used to further evaluate the magnitude and extent of VOCs at SWMU 211-B are summarized below.

Analyte	Maximum Detected Groundwater Concentration*		Project Action Limit	MCL	Secondary Standard			
Total and Dissolved Metals								
Aluminum (mg/L)	1.77	Ν	1	NIA	0.05 to 0.2			
Aluminum, dissolved (mg/L)	0.2	U	1	NA	0.05 to 0.2			
Chromium (mg/L)	0.284		1	0.1	NLA			
Chromium, dissolved (mg/L)	0.01	U	1	0.1	NA			
Iron (mg/L)	4.99			NA	0.2			
Iron, dissolved (mg/L)	0.404		10		0.3			
Lead (mg/L)	0.00308		1	7	NT A			
Lead, dissolved (mg/L)	0.0013	U	1	Zero	NA			
Manganese (mg/L)	0.282	Ν	1	NA	0.05			
Manganese, dissolved (mg/L)	0.248	Х	1		0.05			
Volatile Organic Compounds								
Trichloroethene (µg/L)	220	D	5	5	NA			
1,1-Dichloroethene (µg/L)	810	D	7	7	NA			
<i>cis</i> -1,2-Dichloroethene (µg/L)	29		70	7	NA			
<i>trans</i> -1,2-Dichloroethene (µg/L)	1 to 10	U	100	100	NA			
Vinyl chloride (µg/L)	2 to 20	U	2	2	NA			
<b>Biological (method Quantitative Polymer</b>	ase Chain React	ion)			•			
Dehalococcoides ethenogenes (cells/mL)	43	U	NA		NA			
Dissolved Gases (method Modified R. S. I	Kerr SOP-175)							
Ethane ( $\mu$ g/L): MDL = 0.10 $\mu$ g/L	0.41		NA	NA				
Ethene ( $\mu$ g/L): MDL = 0.025 $\mu$ g/L	0.49		NA	NA				
Methane ( $\mu$ g/L): MDL = 0.025 $\mu$ g/L	6.8		NA	NA				
Inorganic Anions								
Chloride (mg/L)	120		NA	NA	250			
Nitrate (mg/L)	5.4		NA	20	NA			
Sulfate (mg/L)	66		NA	NA	250			

### Table ES.1. RDSI Groundwater Results (September and October 2012) for all MWs at SWMU 211-A

\*Where all analyses are "U" qualified, Table ES.1 reports the laboratory reporting limits. A range is specified where the laboratory reporting limits varied. Laboratory reporting limits for trans-1,2-dichloroethene and vinyl chloride reflect a 2X dilution in a sample from MW204 and a 10X dilution in sample from MW513.

#### Notes:

µg/L—microgram per liter
 mg/L—milligram per liter.
 D—Compounds identified in an analysis at a secondary dilution filter.

4. N—Sample spike recovery not within control limits.

5. U—(inorganics and organics)—Analyte result is less than reporting limit.
6. X—Other specific flags and footnotes may be required to properly define results. For the dissolved manganese analyses, the serial dilution test difference exceeded the quality control limit of 10%.

7. NA-Not available

8. The higher detection limits reported for trans-1,2-dichloroethene and vinyl chloride are due to a 10× dilution in one sample.

- The average soil boring TCE concentration (based upon 13 collected soil samples per soil boring location) was 150 µg/kg, exceeding the soil remediation goal of 75 µg/kg. The maximum soil sample TCE concentration detected was 13,000 µg/kg. The areal extent of TCE contaminated soil, accessible by the selected remedies, is defined to the east, west, and south and encompasses an area of approximately 3,000 ft<sup>2</sup>. Contamination extending under the C-720 footprint (located to the immediate north) is not addressed in this FCR.
- The average TCE concentration exceeded the soil remediation goal of 75  $\mu$ g/kg at 4 of the 19 boring locations (21%). The average TCE level among all samples in these 4 soil borings was 691  $\mu$ g/kg.<sup>2</sup>
- The average soil boring 1,1-DCE, *cis*-1,2-DCE, *trans*-1,2-DCE, and VC concentrations did not exceed their respective soil remediation goals.

Groundwater samples were scheduled to be collected from five MWs at SWMU 211-B. MW514 was dry during the field event; therefore, groundwater samples were collected and analyzed from the four remaining MWs. Groundwater sample results are summarized in Table ES.2. [Preexisting MWs were sampled three times and RDSI-installed wells, except for MW514 (which was dry), were sampled once.]

EVS-ES was used to interpolate the RDSI soil TCE concentration data along with historical soil TCE data for the SWMU 211-B investigation area from OREIS and estimate the total TCE mass in soil and the extent of TCE soil impacts at SWMU 211-B, with consideration of a 90% maximum source volume confidence level statistical evaluation. The total estimated TCE volume is 0.8 gal [based upon current areal extent and that the FCR is focusing on contaminated soil accessible by the selected remedies (i.e., no mass interpolated beneath building)]. LATA Kentucky performed an RDSI HU hydrologic analysis to aid the design of remedial injection technologies to be applied at SWMU 211-B. Soil conditions at SWMU 211-B are consistent with the requirements associated with an injection dependent technology. Flexible wall permeameter tests (ASTM D5084-10) and GSD analyses (ASTM D422) were performed at nine locations. The calculated average hydraulic conductivity values ranged from 1.6E-9 cm/s to 3.3E-6 cm/s. RDSI nested-well injection testing also was performed to assess the hydraulic conductivity of HU1, HU2, and HU3 formations. The injection testing average hydraulic conductivities were 6.7E-5 cm/s, 2.0E-5 cm/s, and 2.4E-5 cm/s for HU1, HU2, and HU3 formations, respectively.

## DATA GAPS

The lone Decision Rule from the data quality objectives for the RDSI is as follows:

If soil boring averaged concentration of TCE and TCE degradation products in soil of the UCRS exceed cleanup levels for a given soil boring, then include the location in the treatment area. If the soil boring-averaged soil concentrations do not exceed cleanup levels, then the area need not be included in the treatment area.

The RDSI fulfilled this requirement to the extent possible.

 $<sup>^{2}</sup>$  The average TCE level among all samples excludes the lower analysis for depth intervals where duplicate analyses are available and uses one-half of the laboratory reporting limit for "U" qualified analyses.

Analyte	Maximum Detected Groundwater Concentration*		Project Action Limit	MCL	Secondary Standard			
Total and Dissolved Metals								
Aluminum (mg/L)	8.49	Ν	1	NA	0.05 to 0.2			
Aluminum, dissolved (mg/L)	0.281		1	INA	0.03 10 0.2			
Chromium (mg/L)	0.131		- 1	0.1	NIA			
Chromium, dissolved (mg/L)	0.01	U	1	0.1	NA			
Iron (mg/L)	9.79		10		0.2			
Iron, dissolved (mg/L)	0.139		10	NA	0.3			
Lead (mg/L)	0.0106		1	Zero	NT A			
Lead, dissolved (mg/L)	0.0013	U	1		NA			
Manganese (mg/L)	1.43		1	NA	0.05			
Manganese, dissolved (mg/L)	0.746	Х	1		0.05			
Volatile Organic Compounds					•			
Trichloroethene (µg/L)	120		5	5	NA			
1,1-Dichloroethene (µg/L)	10	U	7	7	NA			
<i>cis</i> -1,2-Dichloroethene (µg/L)	2.2		70	7	NA			
<i>trans</i> -1,2-Dichloroethene (µg/L)	2	U	100	100	NA			
Vinyl chloride (µg/L)	4	U	2	2	NA			
<b>Biological (method Quantitative Polymer</b>	ase Chain React	tion)			•			
Dehalococcoides ethenogenes (cells/mL) 35 U NA NA								
Dissolved Gases (method Modified R. S. I	Kerr SOP-175)							
Ethane ( $\mu$ g/L): MDL = 0.10 $\mu$ g/L	25		NA		NA			
Ethene ( $\mu$ g/L): MDL = 0.025 $\mu$ g/L	7.9		NA	NA				
Methane ( $\mu$ g/L): MDL = 0.025 $\mu$ g/L	35		NA	NA				
Inorganic Anions								
Chloride (mg/L)	340		NA	NA	250			
Nitrate (mg/L)	3		NA	20	NA			
Sulfate (mg/L) *Where all analyses are "II" qualified. Table ES 2 report	40		NA	NA	250			

### Table ES.2. RDSI Groundwater Results (September and October 2012) for all MWs at SWMU 211-B

\*Where all analyses are "U" qualified. Table ES.2 reports the laboratory reporting limits.

#### Notes:

 Notes:

 1. μg/L—microgram per liter

 2. mg/L—milligram per liter.

 3. N—Sample spike recovery not within control limits.

 4. U—(inorganics and organics) -Analyte result is less than reporting limit.

 5. X—Other specific flags and footnotes may be required to properly define results. For the dissolved manganese analyses, the serial dilution test difference exceeded the quality control limit of 10%.

 6. NA
 Not available

6. NA-Not available

- The 42 soil borings of SWMU 211-A that were sampled for VOC analyses as part of the RDSI and data from historical soil borings in the area as contained in OREIS delimit the lateral extent of soil contamination of TCE and its degradation products, as defined by the project remediation goals, in all directions.
- At SWMU 211-B, the 20 soil borings that were sampled for VOC analyses as part of the RDSI and data from historical soil borings in the area as contained in OREIS delimit the east, west, and south extent of soil contamination by TCE and its degradation products, as defined by the project remediation goals. The area of soil contamination abuts the C-720 Building. As recognized in the RDWP (DOE 2012a), plant infrastructure and continuing use of the C-720 Building prevent current sampling of the soils beneath the building such that the north extent of the soil contamination cannot be determined at this time.

The available soil data for SWMUs 211-A and 211-B provide a foundation for selection and design of an appropriate remedial alternative.

## DISCUSSION

This FCR (based on data from the current RDSI as well as the soil sample data from 2004 and other historical data for the investigation areas as available in OREIS) used EVS-ES to contour the 90% confidence limit of 75  $\mu$ g/kg TCE in soil. The EVS-ES software estimates the TCE source mass within the 90% confidence limit of 75  $\mu$ g/kg TCE to be approximately 12 kg (2.2 gal) at 211-A and 5 kg (0.8 gal) at 211-B.

The soil and groundwater data collected at SWMU 211-A and SWMU 211-B indicate that natural biodegradation may be occurring, albeit at a relatively slow rate. The presence of methane, ethene, ethane, and *cis*-1,2-DCE, and the absence of VC or measureable *Dehalococcoides mccartyi* are indicative of an environment that appears to have some natural attenuation capacity.

## **1. PROJECT DESCRIPTION**

The U.S. Department of Energy (DOE) has tasked LATA Environmental Services of Kentucky, LLC, (LATA Kentucky) with performing field activities to (1) better determine the lateral and vertical extent and distribution of volatile organic compounds (VOCs) and source material and (2) determine soil and groundwater parameters, including geochemical parameters to be utilized in the design of *in situ* bioremediation, if this alternative is selected for the Upper Continental Deposits (UCD) at Solid Waste Management Units (SWMUs) 211-A and 211-B at the Paducah Gaseous Diffusion Plant (PGDP), located near Paducah, Kentucky (Figure 1). LATA Kentucky has developed this Final Characterization Report (FCR) to document these field activities that are associated with the Remedial Design Support Investigation (RDSI) (DOE 2012a) for the Southwest Plume (Figure 2).

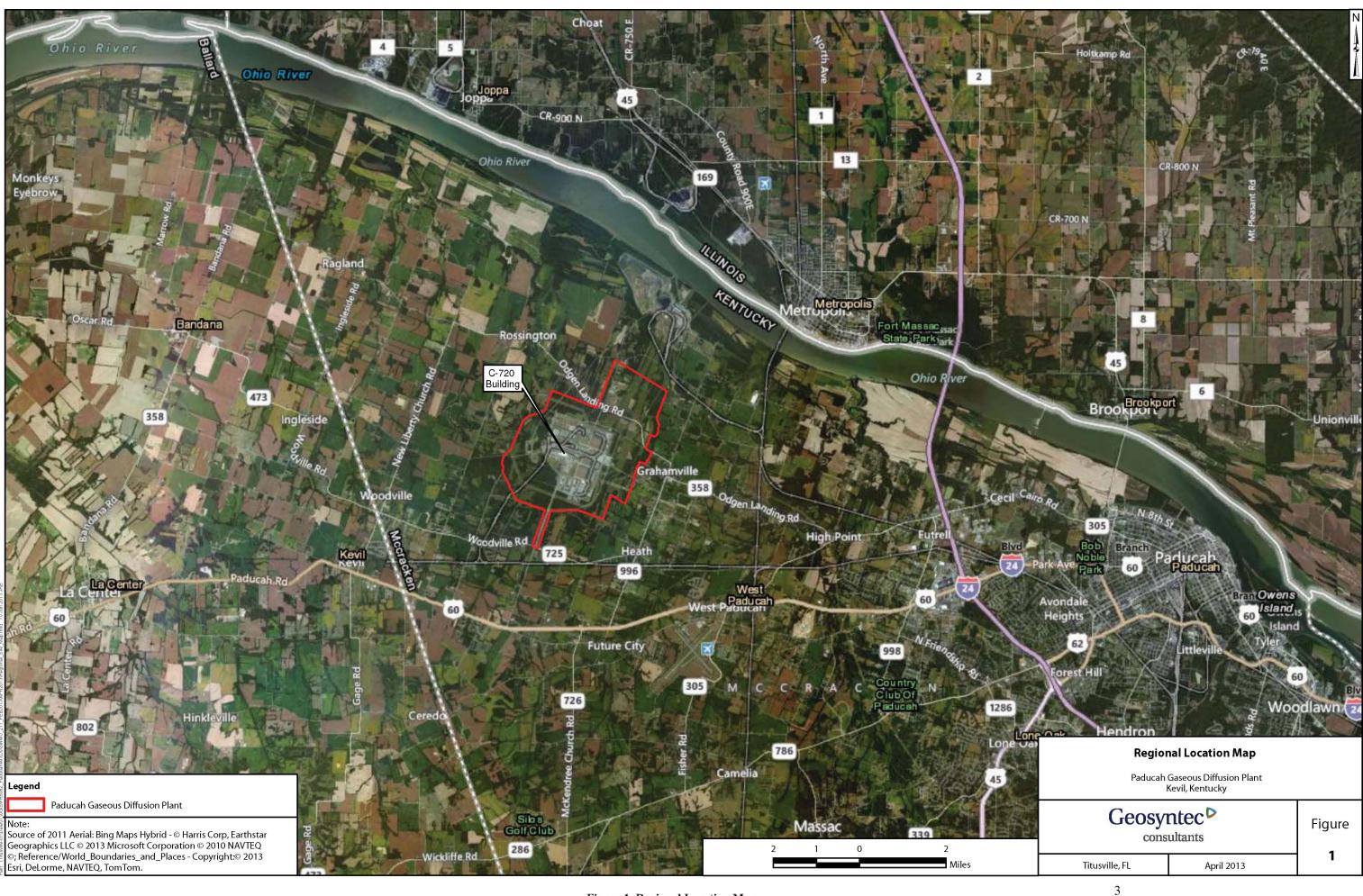
The Southwest Plume refers to an area of groundwater contamination in the Regional Gravel Aquifer (RGA) south of the Northwest Groundwater Plume and west of the C-400 Building. The primary groundwater contaminant of concern for the Southwest Plume is trichloroethene (TCE). Other potential contaminants found in the plume include additional VOCs, metals, and the radionuclide technetium-99.

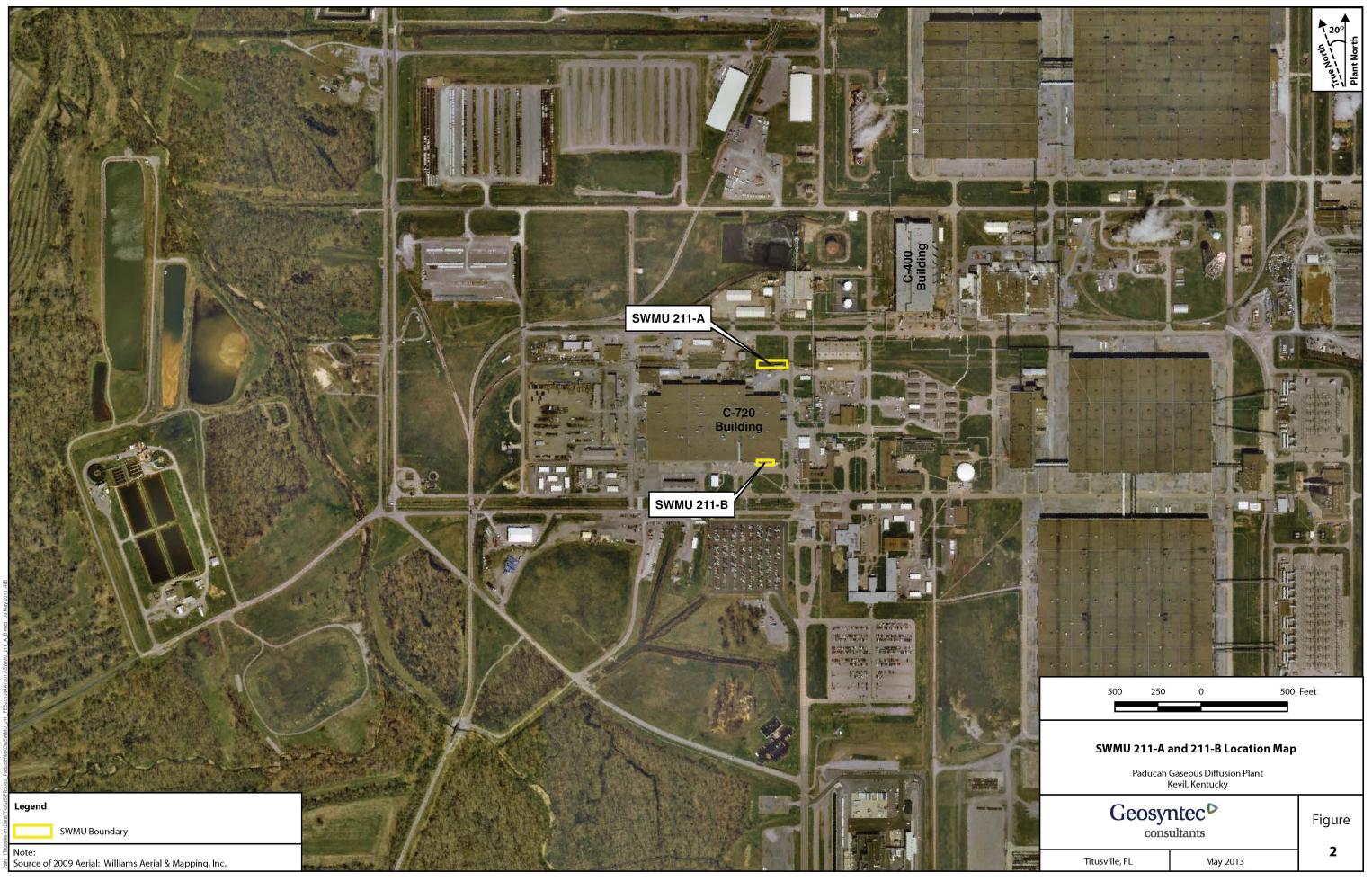
DOE conducted a site investigation (SI) in 2004 to address uncertainties regarding potential source areas to the Southwest Plume that remained after previous investigations. The SI further profiled the concentration and distribution of VOCs in the dissolved-phase plume along the west plant boundary as documented in the SI report (DOE 2007). The potential presence of dense nonaqueous-phase liquid (DNAPL) TCE at the Southwest Plume source areas has been noted based on contaminant trends observed in soil and groundwater samples.

The potential source areas investigated in the SI (DOE 2007) included the C-747-C Oil Landfarm (Oil Landfarm–SWMU 1); the C-720 Building Area near the northeast and southeast corners of the building (C-720 Northeast Site–SWMU 211-A and C-720 Southeast Site–SWMU 211-B); and the storm sewer system between the south side of the C-400 Building and Outfall 008 (storm sewer–SWMU 102). As a result of the SI, the storm sewer was excluded as a potential VOC source to the Southwest Plume.

A revised focused feasibility study (FFS) (DOE 2011) was prepared to evaluate remedial alternatives for potential application at the Southwest Plume source areas. The revised FFS defined the following remedial action objectives:

- 1. Treat and/or remove the principal threat waste consistent with the National Contingency Plan.
- 2a. Prevent exposure to VOC contamination in the source areas that will cause an unacceptable risk to excavation workers (< 10 ft).
- 2b. Prevent exposure to non-VOC contamination and residual VOC contamination through interim land use controls (LUCs) within the Southwest Plume source areas (i.e., SWMU 1, SWMU 211-A, and SWMU 211-B) pending remedy selection as part of the Soils Operable Unit (OU) and the Groundwater OU.
- 3. Reduce VOC migration from contaminated subsurface soils in the treatment areas at the Oil Landfarm and C-720 Northeast and Southeast Sites so that contaminants migrating from the treatment areas do not result in the exceedance of maximum contaminant levels (MCLs) in underlying RGA groundwater.





The following remediation goals for the Upper Continental Recharge System (UCRS) soils at SWMUs 211-A and 211-B are presented in the record of decision (ROD) (DOE 2012b):

- TCE: 75 µg/kg,
- 1,1-dichloroethene (DCE): 137 µg/kg,
- *cis*-1,2-DCE: 619 µg/kg,
- *trans*-1,2-DCE: 5,290 µg/kg, and
- vinyl chloride (VC): 570 µg/kg.

The selected remedies for SWMUs 211-A and 211-B are identified in the ROD (DOE 2012b), which are *in-situ* source treatment using enhanced *in situ* bioremediation with interim LUCs (Alternative 8) or long-term monitoring with interim LUCs (Alternative 2).

This FCR for SWMU 211-A and 211-B is intended to resolve data needs in support of the treatment system design. Based on the information presented in this a report a recommendation for final remedy selection for SWMUs 211-A and 211-B will be presented to the Federal Facility Agreement parties by a letter notification.

## 2. SITE BACKGROUND

## 2.1 SITE DESCRIPTION

PGDP is located approximately 10 miles west of Paducah, Kentucky, (population approximately 26,000) and 3.5 miles south of the Ohio River in the western part of McCracken County (Figure 1). The plant is located on a DOE-owned site, approximately 650 acres of which are within a fenced security area, approximately 800 acres are located outside the security fence, and the remaining 1,986 acres are licensed to Kentucky as part of the West Kentucky Wildlife Management Area. Bordering the PGDP reservation to the northeast, between the plant and the Ohio River, is a Tennessee Valley Authority reservation on which the Shawnee Fossil Plant is located. All plant and process water at PGDP is drawn from the Ohio River.

Before the PGDP was built, a munitions-production facility, the Kentucky Ordnance Works (KOW), was operated at the current PGDP location and at an adjoining area southwest of the site. Munitions, including trinitrotoluene, were manufactured and stored at the KOW between 1942 and 1945. Construction of PGDP was initiated in 1951 and the plant began operations in 1952. Construction was completed in 1955 and PGDP became fully operational in that year, supplying enriched uranium for commercial reactors and military defense reactors.

## 2.2 REGIONAL GEOLOGY AND HYDROGEOLOGY

**Regional Geology.** PGDP is located in the Jackson Purchase Region of Western Kentucky, which represents the northern tip of the Mississippi Embayment portion of the Coastal Plain. The Jackson Purchase Region is an area of land that includes all of Kentucky west of the Tennessee River. The stratigraphic sequence in the region consists of Cretaceous, Tertiary, and Quaternary sediments unconformably overlying Paleozoic bedrock. Within the Jackson Purchase Region, strata deposited above the Precambrian basement rock attain a maximum thickness of 12,000 ft to 15,000 ft. Exposed strata in the region range in age from Devonian to Holocene. The Devonian stratum crops out along the western shore of Kentucky Lake.

Mississippian carbonates form the nearest outcrop of bedrock and are exposed approximately 9 miles northwest of PGDP in southern Illinois (MMES 1992). The Coastal Plain deposits unconformably overlie Mississippian carbonate bedrock and consist of the following: the Tuscaloosa Formation; the sand and clays of the Clayton/McNairy Formations; the Porters Creek Clay; and the Eocene sand and clay deposits (undivided Jackson, Claiborne, and Wilcox Formations). Continental Deposits unconformably overlie the Coastal Plain deposits, which are, in turn, covered by loess and/or alluvium.

Relative to the shallow groundwater flow system in the vicinity of PGDP, the Continental Deposits and the overlying loess and alluvium are of key importance. The Continental Deposits resemble a large low-gradient alluvial fan that covered much of the region and eventually buried the erosional topography. A principal geologic feature in the PGDP area is the Porters Creek Clay Terrace, a subsurface terrace that trends approximately east to west across the southern portion of the plant. The Porters Creek Clay Terrace represents the southern limit of erosion or scouring of the ancestral Tennessee River. Thicker sequences of Continental Deposits, as found underlying PGDP, represent valley fill deposits and can be informally divided into a lower unit (gravel facies) and an upper unit (clay facies). The Lower Continental Deposits (LCD) are the gravel facies consisting of chert gravel in a matrix of poorly sorted sand and silt that rests on an erosional surface representing the beginning of the valley fill sequence. In total, the gravel units average approximately 30-ft thick, but some thicker deposits (as much as 50 ft) exist in deeper scour

channels. The UCD is primarily a sequence of fine grained, clastic facies varying in thickness from 15 ft to 60 ft that consist of clayey silts with lenses of sand and occasional gravel. The UCRS is comprised of alluvial deposits, which vary considerably in grain size and porosity. Based on geologic logs, the lithology reflects facies changes that range from silt to sand to clay. Some logs indicate clay is present from land surface to the top of the RGA, which confines the aquifer. Other logs indicate there are areas where only silt and sand are present from land surface to the top of the RGA, so the RGA is unconfined in these areas. The RGA receives recharge most readily in the unconfined areas. These areas may serve as pathways for contaminant migration from the UCRS to the RGA.

The area of the Southwest Plume lies within the buried valley of the ancestral Tennessee River in which Pleistocene Continental Deposits (the fill deposits of the ancestral Tennessee River Basin) rest unconformably on Cretaceous marine sediments. Pliocene through Paleocene formations in the area of the Southwest Plume have been removed by erosion from the ancestral Tennessee River Basin. In the area of the Southwest Plume and its sources, the upper McNairy Formation consists of 60 to 70 ft of interbedded units of silt and fine sand and underlies the Continental Deposits. Total thickness of the McNairy Formation is approximately 225 ft.

The surface deposits found in the vicinity of PGDP consist of loess and alluvium. Both units are composed of clayey silt or silty clay and range in color from yellowish-brown to brownish-gray or tan, making field differentiation difficult.

**Regional Hydrogeology.** The local groundwater flow system at the PGDP site occurs within the sands of the Cretaceous McNairy Formation, Pliocene terrace gravels, Plio-Pleistocene lower continental gravel deposits and upper continental deposits, and Holocene alluvium (Jacobs EM Team 1997; MMES 1992). Four specific components have been identified for the groundwater flow system and are defined as follows from lowest to uppermost.

- <u>McNairy Flow System</u>. Formerly called the deep groundwater system, this component consists of interbedded sand, silt, and clay of the Cretaceous McNairy Formation. Sand facies account for 40% to 50% of the total formation's thickness of approximately 225 ft. Groundwater flow is predominantly north.
- <u>Terrace Gravel</u>. This component consists of gravel deposits and later reworked sand and gravel deposits found at elevations higher than 320 ft above mean sea level (amsl) in the southern portion of the plant site; they overlie the Paleocene Porters Creek Clay and Eocene sands and are thought to be Pliocene in age. These deposits usually lack sufficient thickness and saturation to constitute an aquifer. Terrace Gravel is not present in the area of the Southwest Plume sources.
- <u>RGA</u>. This component consists of the Quaternary sand and gravel facies of the LCD and Holocene alluvium found adjacent to the Ohio River and is of sufficient thickness and saturation to constitute an aquifer. These deposits are commonly thicker than the Pliocene(?) gravel deposits, having an average thickness of 30 ft, and range up to 50 ft in thickness along an axis that trends east-west through the plant site. Prior to 1994, the RGA was the primary aquifer used as a drinking water source by nearby residents. The RGA has not been formally classified, but likely would be considered a Class II groundwater under U.S. Environmental Protection Agency (EPA) Groundwater Classification guidance (EPA 1986). Groundwater flow is predominantly north toward the Ohio River.
- <u>UCRS</u>. Formerly called the shallow groundwater system, the UCRS consists of the surficial alluvium and UCD. Sand and gravel lithofacies appear relatively discontinuous in cross-section, but portions may be interconnected. The most prevalent sand and gravel deposits occur at an elevation of approximately 345 to 351 ft amsl; less prevalent deposits occur at elevations of 337 to 341 ft amsl.

Groundwater flow is predominantly downward into the RGA from the UCRS, which has a limited horizontal component in the vicinity of PGDP.

The groundwater flow systems associated with the Southwest Plume and its sources are the UCRS and the RGA. In the area of the Southwest Plume, groundwater flow and contaminant migration through the upper 45 ft to 55 ft of subsurface soil (UCD) is predominantly downward with little lateral spreading. This flow system is termed the UCRS. Locally, the UCRS consists of three hydrogeologic units (HUs), an upper silt interval (HU1), an intermediate horizon of sand and gravel lenses (HU2), and a lower silt and clayey silt interval (HU3). Groundwater flow rates in the UCRS tend to be on the order of 0.1 ft per day (ft/day). The silts and clays of the UCRS readily adsorb some contaminants, such as many metals and radionuclides, retarding the migration of these contaminants in groundwater from the source areas. Moreover, laterally extensive silt and clay horizons in the UCRS may halt the downward migration of DNAPLs, but foster the development of DNAPL pools in the subsurface.

Groundwater occurrence in the UCRS is primarily the result of infiltration from natural and anthropogenic recharge. Flow is predominantly downward. Groundwater in the UCRS provides recharge to the underlying RGA. The water table in the UCRS varies both spatially and seasonally due to lithologic heterogeneity and recharge factors (e.g., infiltration of focused run-off from engineered surfaces, seepage due to variations in cooling water line integrity, rainfall and evapotranspiration), and averages approximately 17 ft in depth with a range of 2 to 50 ft.

Downward vertical hydraulic gradients generally range from 0.5 to 1 ft per ft where measured by monitoring wells (MWs) completed at different depths in the UCRS. MWs in the south-central area of PGDP (south of the C-400 Building and east of the C-720 Building) have lower water level elevations than MWs in other areas of the plant (DOE 1997). Horizontal hydraulic conductivity of the UCRS sand units has been determined from numerous slug tests in a previous investigation (CH2M HILL 1992). The measured hydraulic conductivity of the UCRS sands was 3.5E-05 centimeters per second (cm/s) at SWMU 1 and 3.4E-05 cm/s at the C-720 Building (1.4E-05 and 1.3E-05 inches/second). Measurements of the vertical hydraulic conductivity of the UCRS silt and clay units are not available for either SWMU 1 or the C-720 Building; measurements of the vertical hydraulic conductivity of UCRS silt and clay units are not available for either SWMU 1 or the C-720 Building; measurements of the vertical hydraulic conductivity of UCRS silt and clay units on-site range between 1.7E-08 and 2.1E-05 cm/s (6.7E-09 and 8.2E-06 in/s) (DOE 1997; DOE 1999). (The depth-averaged vertical hydraulic conductivity of the total UCRS interval is approximately 1E-06 cm/s [3.9E-07 in/s].)

A thick interval of late Pleistocene sand and gravel from a depth interval of 60 to 90 ft (LCD) represents the shallow, uppermost aquifer underlying most of PGDP, referred to as the RGA. The RGA consists of a discontinuous upper horizon of fine to medium sand (HU4) and a lower horizon of medium to coarse sand, and gravel (HU5). The RGA is the main pathway for lateral flow and dissolved contaminant migration off-site. Variations in hydraulic conductivity and the location of discrete sources of recharge govern the local direction and rate of groundwater flow; however, overall flow within the RGA trends north-northeast toward the Ohio River, which represents the regional hydraulic base level.

The RGA typically has a high hydraulic conductivity with a range from 1.9E-02 to 2.0E+00 cm/s (7.5E-03 to 7.9E-01 in/s) as determined from aquifer testing. RGA horizontal hydraulic gradients range between 1.84E-04 and 2.98E-03 ft/ft and have average and median values of 7.81E-04 and 4.4E-04 ft/ft, respectively. Groundwater flow rates within the RGA average approximately 1 to 3 ft/day. Contaminant migration tends to be less retarded in the coarse sediments of the RGA due to its high groundwater flow rate and also due to the low fraction of organic carbon (0.02%).

## 2.3 STUDY AREA GEOLOGY AND HYDROGEOLOGY

**Study Area Geology.** The geologic strata found in the C-720 Building Area range from clays to silts to sands. Silt and clay are the predominant subsurface soil texture to a depth of 15 to 20 ft. Interbedded sand and clay units are commonly found below those depths. Clay and sandy clay/clayey sand are present near the bottom of most of the soil borings northeast of C-720 Building (DOE 2007).

Immediately southeast of the C-720 Building silt and clay are present to a depth of 15 ft with interbedded sand and clay layers found at deeper horizons. Medium-to-coarse-grained sand, suggestive of the contact between the UCD and LCD, was encountered near the bottom of borings in the southeast corner.

**Study Area Hydrogeology.** The Southwest Plume SI included soil sampling within the upper 60 ft of SWMU 211-A and 211-B. Soil samples verified the presence of the HU1, HU2, and HU3 members of the UCRS. The UCRS is comprised of alluvial deposits, which vary considerably in grain size and porosity. Based on geologic logs, the lithology reflects facies changes that range from silt to sand to clay. Some logs indicate clay is present from land surface to the top of the RGA, which confines the aquifer. Other logs indicate there are areas where only silt and sand are present from land surface to the top of the RGA, so the RGA is unconfined in these areas. The RGA receives recharge most readily in the unconfined areas. These areas may serve as pathways for contaminant migration from the UCRS to the RGA. HU3 sediments tended to be coarser grained than typical. The RGA was not encountered, although the final interval sampled 55 to 60 ft often revealed a noticeable increase in grain size and a significant increase in moisture content, consistent with trends near the top of the RGA.

## 2.4 CONTAMINANT HISTORY

The Southwest Plume refers to an area of groundwater contamination at PGDP in the RGA that is south of the Northwest Groundwater Plume and west of the C-400 Building. The Southwest Plume was identified during the Waste Area Grouping (WAG) 27 Remedial Investigation (RI) (DOE 1999). Additional work to characterize the plume (SWMU 210) was performed as part of the WAG 3 RI (DOE 2000a) and Data Gaps Investigations (DOE 2000b). The Southwest Plume SI (DOE 2007) evaluated potential source areas of contamination to the Southwest Plume and profiled the level and distribution of VOCs in the plume along the west plant fence line.

The C-720 Building is located in the southwest area of the PGDP, southwest of the C-400 Building (Figure 2). The C-720 Building consists of several repair and machine shops, as well as other support operations. The WAG 27 RI identified areas of TCE contamination at the C-720 Building Area. One area was underneath the parking lot and equipment storage area at the northeast corner of the building. The second area was located underneath the parking lot adjacent to the loading docks at the southeast corner of the building.

**C-720 Northeast Site (SWMU 211-A) Source.** Contamination found to the northeast of the C-720 Building is believed to have been released during routine equipment cleaning and rinsing performed in the area. Solvents were used to clean parts, and the excess solvent may have been discharged on the ground; additionally, spills and leaks from the cleaning process may have contaminated surface soils in the area. Solvents may have migrated as dissolved contamination, as rainfall percolating through the soils and migrating to deeper soils and the shallow groundwater, or as DNAPL migrating to adjacent and underlying soils.

**C-720 Southeast Site (SWMU 211-B) Source.** The source of VOC contamination found southeast of the C-720 Building is not certain. The VOCs found in this area may have originated from spills that occurred

within the building, with subsequent discharge to storm drains leading to the southeast corner of the building or from spills or leaks on the loading dock or parking lot located to the southeast of the building. The area of concern discovered during the WAG 27 RI is near the outlet to one of the storm drains for the east end of the building. A storm sewer inlet for the southeast parking lot also is located in the vicinity. The north edge of the parking lot, where the contamination occurs, is the location of one of the loading docks for the C-720 Building, an area where chemicals, including solvents, may have been loaded or unloaded.

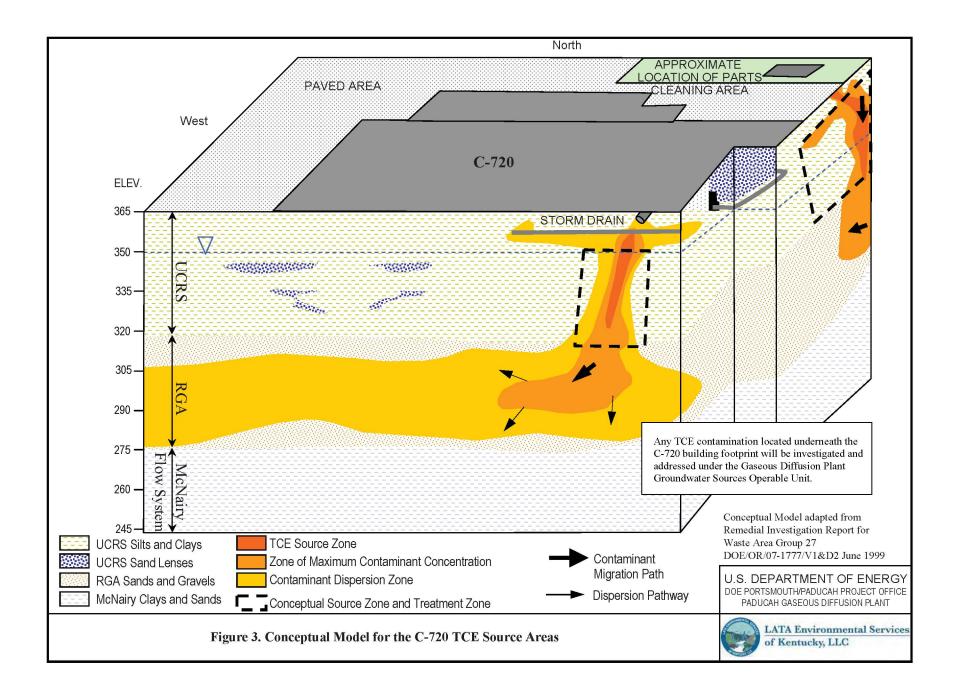
## **2.5 CONCEPTUAL SITE MODELS**

The C-720 Building is a maintenance and machine shop facility that has supported PGDP activities since 1952. It is located in the southwest portion of the plant. The area around the east end of the C-720 Building is covered mostly by concrete or asphalt with intermittent small areas of exposed soil. Both the Northeast and Southeast sites contain multiple utilities that influence the types of subsurface intrusive activities that are feasible in those areas.

For the source zones comprised of high concentration TCE soils and other VOCs at the C-720 sites, the primary pathway of contaminant migration is dissolution of contaminant residual, comprised of TCE and other VOCs, into groundwater in the UCRS and downward migration into the RGA. No lateral migration in the UCRS outside the SWMU area has been identified or is expected since vertical flow is the predominant direction of migration for the TCE contaminant. Dissolved contaminants from these sources subsequently migrate toward the west-northwest in the RGA. The much lower hydraulic conductivity of the McNairy Formation underlying the RGA limits vertical migration of dissolved contamination below approximately 100 ft. Groundwater samples from the RGA in the Southwest Plume support the conclusion that the Southwest Plume has not migrated beyond the DOE property line, which is approximately 4,789 ft northwest of the C-720 Building area. From the point where the groundwater flow path that includes the Southwest Plume crosses the DOE property line, the modeled particle flow path distance to potential points of exposure to RGA groundwater near the Ohio River is approximately 4.0 miles. Currently, there is no uncontrolled exposure to groundwater at PGDP. At this time, exposure to contaminated groundwater off DOE property is hypothetical because the DOE Water Policy controls its use. Figure 3 illustrates the conceptual site model (CSM) for the C-720 Building TCE source area.

C-720 Northeast Site (SWMU 211-A) CSM. The suspected source of contamination for the Northeast site is from a spill(s) of TCE that occurred during routine equipment cleaning and rinsing performed in the area. The suspected spill location(s) is to the north of the adjacent concrete and asphalt parking and maintenance area west of Eighth Street. The maximum TCE concentration detected in soil (8,100  $\mu$ g/kg) in the WAG 27 RI was in a sample 30 ft below ground surface (bgs)/344.39 ft amsl in boring 720-027 (sample ID 720027SA030), located immediately north of the parking lot. The WAG 27 RI and subsequent Southwest Plume SI results show soil TCE levels are variable throughout the UCRS. The source of 1,1-DCE, found co-mingled with TCE in the soils of the west end of the area of SWMU 211-A contamination, is unknown.

C-720 Southeast Site (SWMU 211-B) CSM. The suspected source of contamination for the Southeast site is located below and adjacent to the outlet for the storm drain on the east end, south side of the C-720 Building, and/or a nearby storm sewer inlet for the parking lot. The southeast corner of the building has a parking lot and a material loading and unloading dock adjacent to it. The highest concentration of TCE in soil samples (68,000  $\mu$ g/kg) in the WAG 27 RI and subsequent Southwest Plume SI were found at 20 ft bgs (351.80 ft amsl) in soil boring 720-002 (sample ID 7200002SA020), beneath the concrete and asphalt-covered southeast parking lot and adjacent to the intersection of a buried storm water drain issuing from the facility and a main storm-water sewer line on the south side of the C-720 Building.



These storm water lines eventually discharge through Outfalls 008 and 009 to Bayou Creek. The interval of contaminated soils extends from the base of the storm sewer (5-ft depth) to the base of the UCRS (60-ft depth). The WAG 27 RI and subsequent Southwest Plume SI results show soil TCE levels are variable throughout the UCRS.

# **3. DATA QUALITY OBJECTIVES**

This FCR implemented the seven-step data quality objectives (DQO) process as summarized in the remedial design work plan (RDWP) (DOE 2012a) to ensure that sufficient data of the appropriate type and quality are collected to resolve the data needs identified previously. The DQO process is a series of logical steps that guides managers or staff to a plan for the resource-effective acquisition of environmental data. The DQO process is used to establish performance and acceptance criteria, which serve as the basis for designing a plan for collecting data of sufficient quality and quantity to support the goals of the study.

The DQO process includes systematic planning for environmental data collection. This step is based on the widely accepted "scientific method" and includes concepts such as objectivity of approach and acceptability of results. The DQO process consists of seven iterative steps. Since it is an iterative process, one or more of these steps may be revisited as more information is obtained. The first five steps are focused on identifying qualitative criteria such as the nature of the problem, conceptual model, decisions that need to be made, type of data needed, and the analytic approach or decision rule that describes how the data will be used to draw conclusions. The sixth step establishes acceptable quantitative criteria (acceptance criteria) on the quality and quantity of the data to be collected. The seventh step involves a data collection design to generate data that will meet the quantitative and qualitative criteria specified in step 6. The data collection design specifies the type, number, location, and physical quantity of samples and data and quality assurance/quality control measures.

The DQO process as applied to data collection in support of decision making is summarized here:

- (1) **State the Problem**, wherein the problem to be resolved by the data collection activity is sufficiently defined that the focus of the study will be unambiguous.
- (2) **Identify the Decision**, wherein the principal study question that the study will try to resolve is defined. An output of this step is a decision statement that links the principal study question to possible actions that will solve the problem.
- (3) **Identify Inputs to the Decision**, which identifies informational inputs required to resolve the decision statement and determine which inputs require environmental measurements.
- (4) **Define the Study Boundaries**, which defines the spatial and temporal boundaries of the problem.
- (5) **Develop a Decision Rule**, wherein the environmental measurement parameter of interest, the action level, and inputs from previous steps are formulated in a single statement that describes a logical basis for choosing among alternative actions. An output of this step is an "If...then..." statement that defines conditions that would cause the decision maker to choose among alternative actions.
- (6) **Specify Limits on Decision Errors**, wherein the decision makers' tolerable limits on decision errors are used to establish performance goals for the data collection design.
- (7) **Optimize the Design for Obtaining Data**, wherein an efficient strategy for obtaining data that satisfy the DQOs is identified.

These steps in the DQO process, as they apply to C-720 Northeast and Southeast Sites, are shown in Table 1. The DQO process was conducted for SWMUs 211-A and 211-B and for SWMU 1. Accordingly,

# Table 1. Summary of the DQO Process for the Southwest Plume Source Areas RDSI[Table A.2 of the Remedial Design Work Plan (DOE 2012a)]

1. State the Problem	2. Identify the Decision			3. Identify Inputs to the	5. Develop a	6. Specify Limits	7. Optimize the Design for Obtaining	
	Principal Study Questions	Alternative Actions	Decision Statement	Decision		Decision Rule	on Decision Errors	Data
<ul> <li>Problem Statement:         The PGDP's Southwest Plume consists of groundwater in the RGA contaminated primarily with TCE. The C 747-C Oil Landfarm (SWMU 1) and the C 720 Building Northeast and Southeast Sites (SWMUs 211-A and 211-B, respectively) are sources of contamination to the Southwest Plume A revised FFS (DOE 2011a) was performed for the three Southwest Plume source areas. These are defined in the Southwest Plume FFS:         <ol> <li>Treat and/or remove principal threat waste consistent with CERCLA and the National Contingency Plan.</li> <li>(a) Prevent exposure to VOC contamination in the source areas that will cause an unacceptable risk to excavation workers (&lt; 10 ft depth bgs).</li> <li>(b) Prevent exposure to non-VOC contamination and residual VOC contamination through interim land use controls (LUCs) within the Southwest Plume source areas (i.e., SWMU 1, SWMU 211 A, and SWMU 211 B), pending remedy selection as part of the Soils OU and the Groundwater OU.</li> <li>Reduce VOC migration from contaminated subsurface soils in the treatment areas at the Oil Landfarm and C-720 Northeast and Southeast sites so that contaminants migrating from the treatment areas do not result in an exceedance of MCLs in underlying RGA groundwater.</li> <li>Soil cleanup levels, soil boring-averaged TCE UCRS soil concentrations that would meet RAO #3, calculated in the Southwest Plume Revised FFS Appendix C, are listed below:</li> <li>Oil Landfarm source area 7.3E-02 mg/kg.</li> </ol></li></ul> <li>Previous investigations documented in the WAG 27 RI (DOE 1999) and the SI Report (DOE 2007) did not completely define the areal and vertical extent of soil contaminated above cleanup levels in the source areas. This was identified in the Southwest Plume FFS (DOE 2011a) as a data gap to be resolved in the RDSI.</li> <li>The Southwest Plume Proposed Plan (DOE 2011b) identified <i>In Situ</i> Source Treatment Using Deep Soil Mixing</li>	PSQ-1: What is the areal extent of TCE and TCE degradation products present at soil boring- averaged concentrations higher than cleanup levels at the Southwest Plume source areas? PSQ-2: What are the SWMU-specific ranges of geotechnical and microbial properties that are important to the design of the remedial actions?	AA-1a: Remediation is required where the soil boring-averaged concentrations of TCE and TCE degradation products in soils of the UCRS exceed cleanup levels. AA-1b: Remediation is not required where the soil boring- averaged concentrations of TCE and TCE degradation products in soils of the UCRS do not exceed cleanup levels.	DS-1: Determine the extent of soil boring-averaged concentrations of TCE and TCE degradation products in soils of the UCRS and upper RGA in the Southwest Plume source areas that exceed cleanup levels and require remediation. DS-2: Determine where additional design-type information is required for the preferred alternatives.	<ol> <li>Process knowledge of releases (DOE 2011a).</li> <li>Previous investigation results (DOE 2011a).</li> <li>Description of C 720 source areas in Appendix C of the GWOU FS (DOE 1999).</li> <li>Site conceptual model (DOE 2011a).</li> <li>Southwest Plume FFS Alternatives 2, 3, and 8 descriptions (DOE 2011a).</li> <li>Southwest Plume FFS Alternatives 2, 3, and 8 descriptions (DOE 2011a).</li> <li>Minimum TCE cleanup levels: 7.3E-02 mg/kg for the C-747-C Oil Landfarm and 7.5E-02 mg/kg for the C-720 Northeast and Southeast Sites (DOE 2011a).</li> <li>TCE DLs by USEC = 5E-03 mg/kg (Watson 2010).</li> <li>Current estimates of source area dimensions shown in Southwest Plume FFS (DOE 2011a).</li> <li>Information requirements for design of the preferred alternatives as follows:</li> <li>Soil properties common to both soil mixing and <i>in situ</i> bioremediation—fraction organic carbon, and grain size.</li> <li>Soil properties specific to soil mixing—<i>in situ</i> water content, pH, unconfined compressive strength, compressibility, and index properties.</li> <li>Soil properties specific to <i>soil mixing</i>.</li> <li>Groundwater properties needed to assess <i>in situ</i> bioremediation—permeability</li> <li>Groundwater properties needed to assess <i>in situ</i> bioremediation—permeability</li> </ol>	Spatial boundaries: The vertical boundary of the study is the upper RGA as feasible (to the base of HU4 interval) at all sites. The results of soil TCE analyses will be provided to EPA and KDEP on a timely basis, and the FFA Parties will confer via teleconference regarding the need for further sampling in the RGA. TCE concentrations above cleanup levels are present at the maximum depths sampled in previous investigations. Surface and subsurface infrastructure is present in the C-720 source areas. The C-720 building bounds the north side of the southeast source area. Schedule boundaries: The focused investigation results must be available by the start of development of the 90% remedial design. Fieldwork and lab analysis turnaround is anticipated to require approximately 120 days. Operational boundaries: Field investigations and remedial design are constrained by surface and subsurface infrastructure at the C-720 Building. No significant interferences exist at the Oil Landfarm. None of the areas are posted as radiological contamination areas; however, VOCs, metals, and SVOCs are present in soils. An underground storage tank near northeast corner of C-720 may present problems both as subsurface infrastructure and source of petroleum in soils. Administrative boundaries: The investigation includes subcontracting for a field laboratory to provide near real time analysis of VOCs in soil and groundwater. Establishment of a field laboratory facility will require development of additional work control.	DR-1: If soil boring-averaged concentrations of TCE and TCE degradation products in soil of the UCRS exceed cleanup levels for a given soil boring, then include the location in the treatment area. If the soil boring- averaged soil concentrations do not exceed cleanup levels, then the area need not be included in the treatment area.	Definitive data quality is assumed for fixed-base and field laboratory analysis. Screening level data quality is assumed for field analyses. The soil boring- averaged contaminant concentration will be derived solely from laboratory analyses from each 5-ft depth interval. The derived soil boring-averaged contaminant concentration will be used as a definitive criterion for comparison with the remediation goal, with no consideration for false rejection rate or false acceptance rate. The sampling plan minimizes decision error by intentionally biasing the location of the sample for laboratory analysis to the location of highest field PID measurement in each 5-ft depth interval.	The selected treatment technologies are able to address the range of small discrete areas to broad areas. There effectively is no minimum or maximum decision area. A combination of field screening instruments, field laboratory analysis, and fixed-base laboratory confirmation analysis will be used to define the outer extent of the area contaminated above the remediation goals. The contaminants of interest are TCE and degradation products: 1,1 dichloroethene; <i>cis</i> -1,2-dichloroethene; <i>trans</i> -1,2-dichloroethene; and vinyl chloride. The targeted depth of investigation is 60 ft bgs, which penetrates through the average depth of the base of the HU4 at SWMU 1 and at the C-720 sites. Where one or more soil boring- averaged contaminant concentrations in a soil boring exceed an RG for a site, contingency borings will be sampled, as necessary (up to the contingency allotment for each site), to bound the remediation area. At SWMU 1, successive contingency boring step outs nominally will be 75 ft. (Multiple contingency boring may extend the investigation beyond 75 ft of the SWMU boundary.) At the C-720 sites, contingency boring step outs must be consistent with the sampling grid except where prevented by the presence of utilities or other obstructions. Parameters as established in quality assurance project plan for precision, accuracy, representativeness, completeness, and comparability. A combination of field measurements and fixed-base laboratory analysis will be used to quantify key design criteria for the preferred alternatives.

text in Table 1 contains references to SWMU 1, which are artifacts of the scoping process and not intended to provide information for SWMU 1 as part of this final characterization report. The resulting sampling and analysis plan is described in Section 4. The Quality Assurance Project Plan (QAPP) for the RDSI [Attachment A5 of the RDWP (DOE 2012a)] contains measurement quality objectives and data quality indices derived from the project DQOs that ensured quality data was obtained to adequately assess SWMUs 211-A and 211-B. With the few exceptions noted in Section 4.9, all VOC analyses associated with soil and groundwater samples of the RDSI meet measurement performance and other assessment criteria of the project QAPP and are included in this FCR. In addition to the RDSI data, this FCR incorporates data from the WAG 27 RI and Southwest Plume SI, as required by the project DQOs and QAPP (DOE 2012a).

# 4. FINAL CHARACTERIZATION/RDSI PLANNING

RDSI planning includes evaluating existing data, DQO scoping, and performing a site visit. Additionally, planning is necessary to protect health and safety, develop the environmental sampling protocol, and identify procedures for handling investigation derived waste. Each activity has been completed and is discussed below.

### 4.1 EVALUATION OF EXISTING DATA

The preliminary C-720 northeast and southeast site boundaries shown in the Southwest Plume FFS were based on the fate and transport model grid for the C-720 area used in the WAG 27 RI (DOE 1999) and the Southwest Plume SI (DOE 2007). The Groundwater OU Feasibility Study (DOE 2001) also provided estimates of source area locations and dimensions. These estimates were used in the Southwest Plume FFS to define the SWMU 211-A and 211-B boundaries shown on Figures 4 and 5, respectively.

### 4.2 INITIAL SAMPLING LOCATIONS

By combining data from previous reports as well as information obtained through Oak Ridge Environmental Information System (OREIS), a new general sample boundary area was drawn for the C-720 northeast (i.e., SWMU 211-A) and southeast (i.e., SWMU 211-B) sites (Figures 4 and 5, respectively). The boundaries incorporate historical detections of TCE contamination and extend a short distance outward from these locations. Two sampling locations (720-018 and P4-H7/720-027) in the C-720 northeast site identified during the SI as having at least one TCE detection at a concentration greater than 70  $\mu$ g/kg are included within the sampling area. Sampling grid spacing and sampling location coordinates presented in Appendix A.1 of the RDWP (DOE 2012a) were used as a guide, but site obstructions and/or sample results were used to determine appropriateness of sample locations.

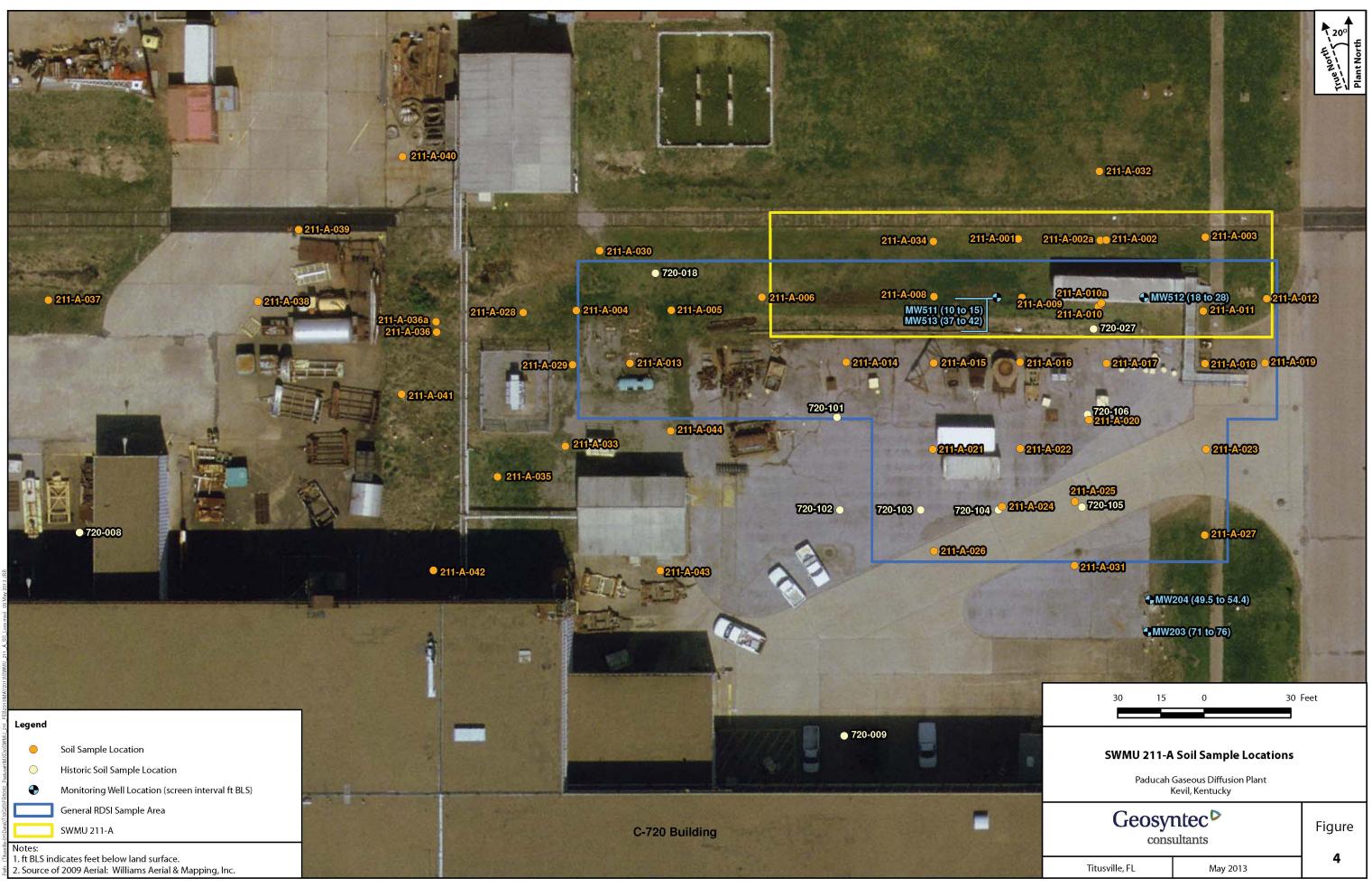
#### 4.3 DQO SCOPING MEETING

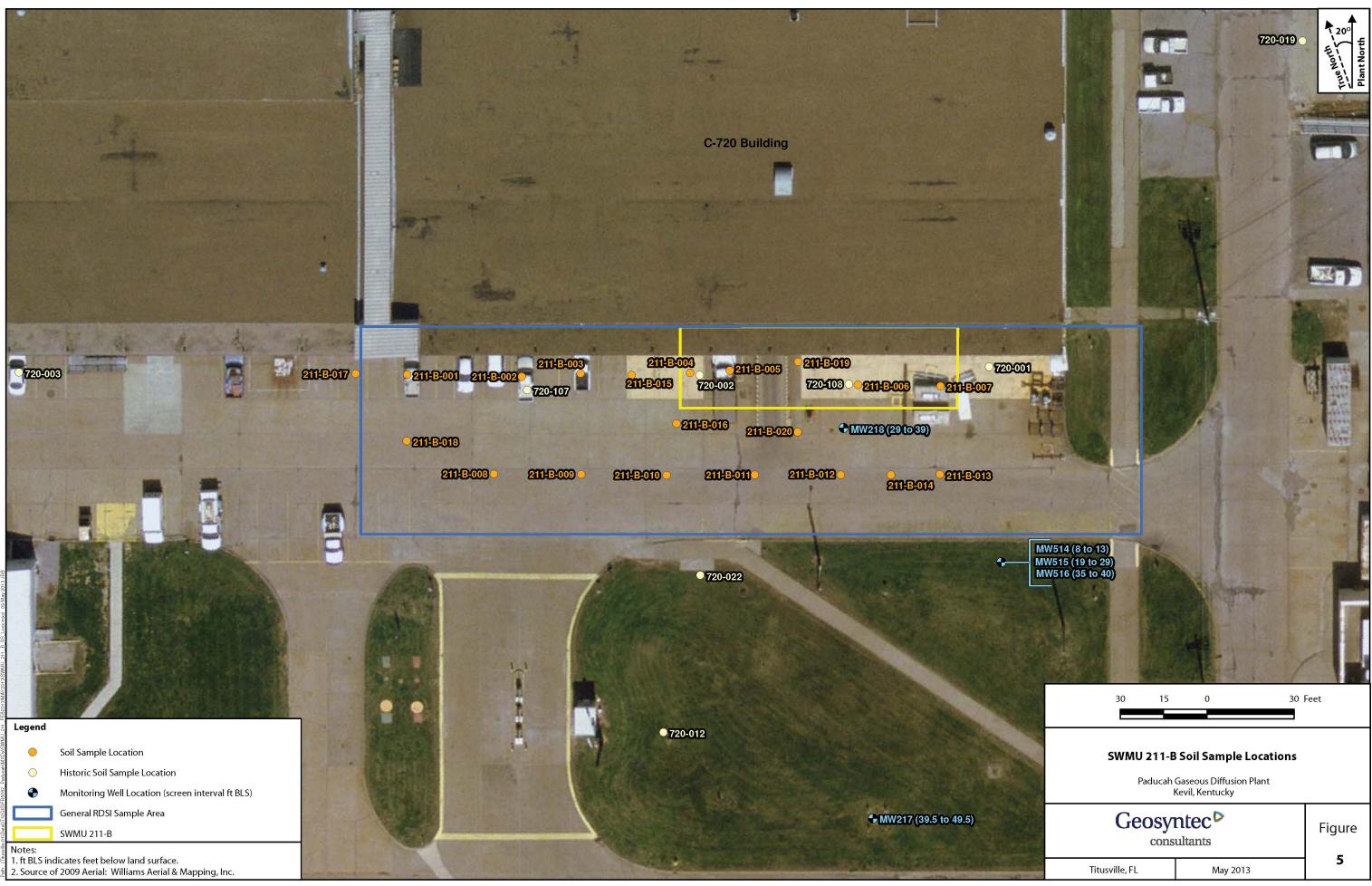
A DQO scoping meeting, attended by subject matter experts, was held February 4, 2010, to gather input to DQO development for the RDSI characterization plan. Subsequently, additional meetings were held, from which data needs specific to the selected remedies were identified. The results from those meetings are presented in the DQOs provided in Section 3.

#### 4.4 SITE WALKDOWNS

The SWMU 211-A and 211-B source areas were visited by the project team prior to commencement of the RDSI characterization plan implementation. The site visits to SWMU 211-A and 211-B were conducted in June and July of 2012. A LATA Kentucky surveyor completed the site walkdown to locate and mark utilities with the aid of plant drawings and coordinates, a handheld Metrotech line locator, and a Geophysical Survey Systems, Inc., ground penetrating radar system, model SIR-3000.

Following the site walkdowns the proposed sample locations at SWMU 211-A required no modifications. The SWMU 211-B proposed locations were shifted toward building C-720 by approximately 5 ft to avoid contact with the sewer drain system.





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#### 4.5 HEALTH AND SAFETY

Environmental sampling to protect the health and safety of the workers is an important part of any related project. During drilling and sampling operations, a photoionization detector (PID) was used to determine if VOCs were present at hazardous levels in the workers' breathing zone. Personal samplers were also used to establish baseline values early in the project. Monitoring for radioactive contamination was conducted according to the radiation work permit. Additional details and requirements for health and safety sampling are contained in the *Health and Safety Plan for the Southwest Plume Remedial Design Support Investigation at the Paducah Gaseous Diffusion Plant, Paducah, Kentucky*, PAD-PROJ-0133/R0 (LATA Kentucky 2012).

#### 4.6 SOIL SAMPLING STRATEGY

The SWMU 211-A and 211-B boundaries shown in the Southwest Plume FFS were based on the fate and transport model grid for the C-720 area used in the WAG 27 RI (DOE 1999) and the Southwest Plume SI (DOE 2007). The Groundwater OU Feasibility Study (DOE 2001) also provided estimates of source area locations and dimensions. These estimates were used in the Southwest Plume FFS to define the SWMU boundaries. The data from these three reports and information obtained through OREIS were combined and a sample boundary area was presented in the RDSI as shown in Figures 4 and 5. The boundaries encompassed historical detections of TCE and extended a short distance outward from the detections and provided a general starting point for this RDSI. Figures 4 and 5 show the actual sampling locations for SWMUs 211-A and 211-B, respectively. Table 2 provides PGDP coordinates for the sampling locations depicted in Figure 4 for SWMU 211-A. Table 3 provides PGDP coordinates for the sampling locations depicted in Figure 5 for SWMU 211-B.

Soil borings 211-A-001 through 211-A-036 and 211-B-001 through 211-B-020 were performed from August 16 through October 19, 2012. Follow-on sampling at SWMU 211-A (soil borings 211-A-037 through 211-A-044) was performed from February 25 through March 6, 2013. Soil borings were completed using an AMS 9500 VTR rig with Geoprobe direct push technology (DPT) DT-22 tooling and polyvinyl chloride sample liners, provided by Chase Environmental Group, Inc. (Kevil, Kentucky).

# 4.7 MONITORING WELL INSTALLATION

MWs were installed at SWMU 211-A (MW511, MW512, and MW513) and SWMU 211-B (MW514, MW515, and MW516) in August 2012 using hollow stem auger drilling methods. Tables 4 and 5 provide well construction details for the MWs installed at SWMU 211-A and SWMU 211-B, respectively. The locations of the newly installed MWs are presented on Figure 4 (SWMU 211-A) and Figure 5 (SWMU 211-B).

At SWMU 211-A, MW511 and MW513 were installed as a cluster within a common borehole using a 6.25-inch inside diameter (ID) auger, and MW512 was installed using a 4.25-inch ID auger. The MWs were constructed of 2-inch diameter stainless screen and riser, with screen intervals of 10 to 15 ft bgs, 359.03 to 364.03 ft amsl (MW511), 18 to 28 ft bgs, 346.68 to 356.68 ft amsl (MW512), and 37 to 42 ft bgs, 332.02 to 337.02 ft amsl (MW513). MW construction logs are included in Appendix A.

At SWMU 211-B, MW514, MW515, and MW516 were installed as a cluster within a common borehole using a 8.25-inch ID auger. The MWs were constructed of 2-inch diameter stainless screen and riser, with screen intervals of 8 to 13 ft bgs, 359.73 to 364.73 ft amsl (MW514), 19 to 29 ft bgs, 343.75 to

353.75 ft amsl (MW515), and 35 to 40 ft bgs, 332.77 to 337.77 ft amsl (MW516). MW construction logs are included in Appendix A.

Station.	Plant Coor	Elevation	
Station	Northing [ft]	Easting [ft]	[ft amsl]
211-A-001	-2023.2110	-5059.5510	374.598
211-A-002	-2023.6120	-5029.1430	374.504
211-A-002a	-2023.7790	-5031.2360	374.476
211-A-003	-2022.6390	-4994.8430	374.913
211-A-004	-2048.0820	-5212.8110	373.283
211-A-005	-2047.9830	-5179.8330	373.701
211-A-006	-2043.4640	-5148.4270	374.090
211-A-008	-2043.2190	-5088.8040	374.092
211-A-009	-2043.5870	-5058.3150	374.263
211-A-010	-2046.7240	-5031.9270	374.330
211-A-010a	-2045.4290	-5030.7210	374.359
211-A-011	-2048.2000	-4995.4900	375.221
211-A-012	-2043.9840	-4973.5470	375.458
211-A-013	-2066.2640	-5194.1350	374.351
211-A-014	-2065.9010	-5119.3050	374.469
211-A-015	-2066.2010	-5088.9670	374.601
211-A-016	-2065.9450	-5059.0230	374.653
211-A-017	-2066.3420	-5029.0030	374.894
211-A-018	-2066.3810	-4994.8990	374.865
211-A-019	-2066.1750	-4974.1430	374.771
211-A-020	-2085.9880	-5035.1640	374.833
211-A-021	-2096.0950	-5089.2170	374.593
211-A-022	-2095.8230	-5058.8970	374.620
211-A-023	-2096.1320	-4994.5060	374.620
211-A-024	-2115.8920	-5065.2080	374.350
211-A-025	-2114.2460	-5040.0200	374.210
211-A-026	-2131.2640	-5088.8230	374.296
211-A-027	-2125.7710	-4995.0460	374.622
211-A-028	-2048.7590	-5231.1660	373.633
211-A-029	-2066.7480	-5214.0940	374.274
211-A-030	-2027.3620	-5204.6280	373.823
211-A-031	-2136.2860	-5040.0740	373.999
211-A-032	-1999.9050	-5031.5160	373.362
211-A-033	-2094.9760	-5216.5300	374.359

Table 2. PGDP Plant Coordinates for SWMU 211-A Source AreaSampling Locations

Station	Plant Coo	rdinates	Elevation
Station	Northing [ft]	Easting [ft]	[ft amsl]
211-A-034	-2024.1310	-5089.0630	374.423
211-A-035	-2105.5170	-5240.0280	373.994
211-A-036	-2055.4830	-5261.2480	374.472
211-A-036a	-2051.9460	-5261.3630	374.415
211-A-037	-2044.5470	-5395.8070	373.516
211-A-038	-2045.0350	-5323.1710	374.499
211-A-039	-2020.1390	-5309.1090	374.571
211-A-040	-1994.8890	-5272.9960	374.583
211-A-041	-2077.0010	-5273.3620	373.935
211-A-042	-2137.9710	-5262.2770	373.996
211-A-043	-2138.0230	-5183.7380	374.863
211-A-044	-2089.7250	-5180.1200	374.396

# Table 2. PGDP Plant Coordinates for SWMU 211-A Source Area Sampling Locations (Continued)

# Table 3. PGDP Plant Coordinates for SWMU 211-B Source AreaSampling Locations

Station	Plant Coo	Elevation	
Station	Northing [ft]	Easting [ft]	[ft amsl]
211-B-001	-2607.6980	-5240.8990	371.916
211-B-002	-2608.4570	-5201.4670	371.965
211-B-003	-2607.3650	-5181.1500	372.000
211-B-004	-2607.1870	-5143.3300	371.941
211-B-005	-2606.3070	-5129.5960	371.940
211-B-006	-2611.2800	-5085.4310	371.960
211-B-007	-2611.7170	-5056.8590	372.028
211-B-008	-2642.0290	-5211.0330	371.474
211-B-009	-2642.0580	-5180.9140	371.359
211-B-010	-2642.3830	-5151.4210	371.331
211-B-011	-2642.3070	-5120.9840	371.318
211-B-012	-2642.2870	-5091.2570	371.587
211-B-013	-2642.1370	-5057.0470	371.850
211-B-014	-2642.3210	-5074.0080	371.668
211-B-015	-2607.9310	-5163.5150	371.996
211-B-016	-2624.6240	-5148.0390	371.569
211-B-017	-2607.4590	-5258.7540	371.976
211-B-018	-2630.5500	-5241.1330	371.646
211-B-019	-2603.3600	-5105.9730	371.996
211-B-020	-2627.5870	-5106.1450	371.664

#### Table 4. PGDP SWMU 211-A Well Construction Details

		Riser	Riser			Top of	Bottom	Concern	<b>C</b>	Datum		Plant Coord	linates
Well Number	Date Installed	Casing Materia l	Casing Diameter [in]	Screened Zone	HU	Top of Screen [ft bgs]	of Screen [ft bgs]	Screen Materia l	Screen Diameter [in]	Datum Elevation [ft NAVD88]	Datum Reference	Northing [ft]	Easting [ft]
	Preexisting Wells												
MW203	4/3/1991	SLS	2	RGA	HU5	71	76	SLS	2	377.91	TOC	-2,159.20	-5014.80
MW204	4/5/1991	SLS	2	UCRS	HU3	49.5	54.4	SLS	2	378.06	TOC	-2148.10	-5014.10
							RDSI-ins	stalled Wells	5				
MW511	8/27/2012	SLS	2	UCRS	HU1	10	15	SLS	2	376.82	TOC	-2042.42	-5176.15
MW512	8/24/2012	SLS	2	UCRS	HU2	17.8	27.8	SLS	2	377.59	TOC	-2044.32	-5043.47
MW513	8/27/2012	SLS	2	UCRS	HU3	37	42	SLS	2	376.82	TOC	-2042.42	-5176.15

Notes:

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1. SLS-stainless steel

PVC—polyvinyl chloride
 NAVD88—North American Vertical Datum of 1988

4. TOC—top of casing5. TIC—top of internal casing

#### Table 5. PGDP SWMU 211-B Well Construction Details

	Date r Installed	Riser	Riser		HU	Top of Screen [ft bgs]	Bottom		Screen	Datum		Plant Coordinates	
Well Number		Casing Dia	Casing Diameter [in]				of Screen [ft bgs]	Screen Material	Diameter [in]	Elevation [ft NAVD88]	Datum Reference	Northing [ft]	Easting [ft]
	Preexisting Wells												
MW217	12/18/91	PVC	2	UCRS	HU3	39.5	49.5	PVC	2	378.56	TIC	-2760.66	-5080.28
MW218	1/30/1992	PVC	2	UCRS	HU2/3	29.0	39.0	PVC	2	371.63	TIC	-2626.16	-5090.38
						RDS	I-installed W	/ells					
MW514	8/27/2012	SLS	2	UCRS	HU1	7.8	12.8	SLS	2	375.67	TOC	-2673.93	-5036.81
MW515	8/27/2012	SLS	2	UCRS	HU2	18.8	28.8	SLS	2	375.67	TOC	-2673.93	-5036.81
MW516	8/27/2012	SLS	2	UCRS	HU3	34.8	39.8	SLS	2	375.67	TOC	-2673.93	-5036.81

Notes:

1. SLS-stainless steel

2. NAVD88—North American Vertical Datum of 1988

3. TOC—top of casing

#### 4.8 INVESTIGATION-DERIVED WASTE

Investigation-derived waste generated during the performance of fieldwork associated with this FCR is considered part of the Southwest Plume RDSI. As such, only a portion of the following inventory of the Southwest Plume RDSI-generated waste is directly associated with SWMUs 211-A and 211-B.

- Nine ST-90 boxes and two 55-gal drums of soil/personal protective equipment and debris (approximately 825 ft<sup>3</sup>).
  - All but one of the ST-90 boxes and the two 55-gal drums have been disposed of at the C-746-U Contained Landfill [permitted for operation by the Kentucky Division of Waste Management (Solid Waste Landfill Permit Number 073-00045)].
  - Sample results for the remaining ST-90 box have been received from the laboratory. The results are being processed in documentation for disposal at the C-746-U Contained Landfill.
- One 55-gal drum of personal protective equipment from decontamination activities (approximately 7.4 ft<sup>3</sup>).
  - The 55-gal drum has been disposed of at the C-746-U Landfill.
- Five 1,200-gal poly tanks of decontamination water (approximately 802 ft<sup>3</sup>).
  - The decontamination water has been treated for suspended solids and staged in two tanks.
  - Of the two tanks, one has been characterized and approved for discharge at C-612. Characterization data for the second tank have been received and are being processed for approval for discharge through C-612.

#### **4.9 DATA EVALUATION**

Data verification, validation, and assessment were performed for the project data in accordance with PAD-ENM-5003, *Quality Assured Data* (LATA Kentucky 2010). The data evaluation results are stored in Paducah Project Environmental Measurements System and are transferred with the data to Paducah OREIS.

The data evaluation for the RDSI identified the following variances. At SWMU 211-A, a total of 31 planned borings and 10 contingency borings were allotted. The investigation sampled 30 of the planned borings and 12 contingency borings. DOE sampled the 2 additional contingency borings to better characterize the extent of the VOC contamination. (For SWMU 211-B, a total of 17 planned borings and 12 contingency borings were available. Only the original 17 planned borings and 2 contingency borings were required to characterize the extent of contamination.)

The investigation soil analyses include a single exceedance of the laboratory reporting limits required by the RDWP (DOE 2012a). The analysis for 1,1-DCE in the sample from 211-A-036 at 22 ft depth (352.47 ft amsl) reports a result of 31 "U"  $\mu$ g/kg; the reporting limit for 1,1-DCE is required to be 10  $\mu$ g/kg. This variance is anticipated to have minimal impact to the project. Analyses of 1,1-DCE for deeper samples in this soil boring significantly exceed the 1,1-DCE remediation goal (137  $\mu$ g/kg) while analyses for shallower samples report nondetect levels.

Groundwater analyses include exceedances of the required laboratory reporting limit only for *trans*-1,2-DCE and vinyl chloride in 1 of 3 samples from MW204 and the lone sample from MW513 (both SWMU 211-A MWs). In MW204, the highest reporting limits (2  $\mu$ g/L *trans*-1,2-DCE and 4  $\mu$ g/L VC) are twice the required reporting limits. Because all three results for these analytes in MW204 are "U" qualified, this variance has little impact to the groundwater assessment.

In the lone MW513 groundwater sample, the reporting limits (10  $\mu$ g/L *trans*-1,2-DCE and 20  $\mu$ g/L VC) are 10 times the required reporting limits (due to a 10 × dilution of the sample); however, analyses for collocated wells MW511 and MW512 (nondetect levels of 1  $\mu$ g/L *trans*-1,2-DCE and 2  $\mu$ g/L VC in both wells) provide good characterization of UCRS groundwater quality at SWMU 211-A. The RDWP (DOE 2012a) identified method ASTM D4360-96 or equivalent for constant head injection tests of the RDSI. The correct method reference is ASTM D4630-96.

Level IV data validation for SWMUs 211-A and 211-B was performed at a rate of 10%, as required by the RDSI characterization plan. Samples from areas with higher TCE concentrations were targeted for data validation. No data was rejected during data validation. During validation, the soils and groundwater data were found to meet the project acceptance criteria except as noted below.

#### • SWMU 211-A soil samples (VOCs)

- Analyses from the validated samples showed compliance with the quality control requirements set forth by the analytical methods. The data was considered valid and acceptable. Chains of custody were reviewed and found to be compliant. All samples were analyzed within the acceptable holding times. The instrument performance check was performed within the required time period and met all acceptance criteria. All initial calibrations were performed at the proper frequency. All continuing calibrations were performed at the proper frequency. Method blanks were analyzed at the proper frequency. Results for VOC analyses for 12 samples were qualified "J" (indicating estimated values) due to surrogate recovery results as follows:
  - 211-A-028 at 48.0 ft depth/325.63 ft amsl
  - 211-A-028 at 50.5 ft depth/323.13 ft amsl
  - 211-A-029 at 28.5 ft depth/345.77 ft amsl
  - 211-A-029 at 32.0 ft depth/342.27 ft amsl
  - 211-A-029 at 48.5 ft depth/325.77 ft amsl
  - 211-A-030 at 32.5 ft depth/341.32 ft amsl
  - 211-A-036 at 22.0 ft depth/352.47 ft amsl
  - 211-A-036 at 26.5 ft depth/347.97 ft amsl
  - 211-A-036 at 31.5 ft depth/342.97 ft amsl
  - 211-A-036 at 35.5 ft depth/338.97 ft amsl
  - 211-A-036 at 44.5 ft depth/329.97 ft amsl
  - 211-A-036 at 47.5 ft depth/326.97 ft amsl

All internal standards were analyzed at the appropriate frequency and met acceptance criteria. Results for VOC analyses for five samples were qualified "J" due to MS/MSD (matrix spike/matrix spike duplicate) recoveries as follows:

- 211-A-004 at 24.9 ft depth/348.38 ft amsl
- 211-A-028 at 38.5 ft depth/335.13 ft amsl
- 211-A-028 at 55.1 ft depth/318.53 ft amsl
- 211-A-029 at 28.5 ft depth/345.77 ft amsl
- 211-A-036 at 44.5 ft depth/329.97 ft amsl

The calculated RPD (relative percent difference) was exceeded for the parent sample and its duplicate for 1,1-DCE and TCE. The results for these two analytes were "J" qualified in the parent and duplicate samples.

- 211-A-029 at 32 ft depth/342.27 ft amsl

LCS (laboratory control sample) and LCSD (laboratory control sample duplicate) samples were analyzed at the proper frequency. Review of calculations met acceptance criteria.

#### • SWMU 211-B soil samples (VOCs)

— Analyses from the validated samples showed compliance with the quality control requirements set forth by the analytical methods. The data was considered valid and acceptable. Chains of custody were reviewed and found to be compliant. All samples were analyzed within the acceptable holding times. The instrument performance check was performed within the required time period and met all acceptance criteria. All initial calibrations were performed at the proper frequency. All continuing calibrations were performed at the proper frequency. Method blanks were analyzed at the proper frequency. The proper surrogate standards were analyzed at the appropriate frequency. No data was qualified due to surrogate recovery limits. All internal standards were analyzed at the appropriate frequency and met acceptance criteria. Results for VOC analyses for two samples were qualified "J" due to MS/MSD recoveries:

- 211-B-005 at 4.9 ft depth/367.04 ft amsl

- 211-B-19 at 32.0 ft depth/340.00 ft amsl

The calculated RPD was exceeded for the parent sample and duplicate samples for TCE. TCE results were "J" qualified in the parent and duplicate samples:

- 211-B-005 at 29.5 ft depth/342.44 ft amsl

LCS and LCSD samples were analyzed at the proper frequency. Review of calculations met acceptance criteria.

#### • SWMU 211-A and 211-B water samples (VOCs, metals, chloride, nitrate, sulfate)

- Analyses from the validated samples showed compliance with the quality control requirements set forth by the analytical methods. The data was considered valid and acceptable. Chains of custody were reviewed and found to be compliant. All samples were analyzed within the acceptable holding times.
  - VOCs—VOCs results for two samples were qualified as either "J" or "UJ" (indicating not detected at or below the lowest concentration reported but estimated) due to the presence of headspace in the samples (MW162 and MW218). The instrument performance check was performed within the required time period and met all acceptance criteria. All initial calibrations were performed at the proper frequency. All continuing calibrations were performed at the proper frequency. No qualification of the data was required based on the evaluation of the continuing calibration. Method blanks were analyzed at the proper frequency. Results for two samples were qualified due to surrogate recoveries (MW161 and MW203). All internal standards were analyzed at the appropriate frequency and met acceptance criteria. Some results were qualified "J" or "UJ" based on low recovery observed in both the MS/MSD and the LCS. The RPD for the duplicate sample analyses were within

acceptance criteria. Some results were "J" or "UJ" qualified due to LCS and LCSD acceptance criteria (MW161, MW162, MW203, MW204, MW217, and MW218). Review of calculations met acceptance criteria.

- Metals—All initial and continuing calibrations were within the acceptance criteria. All method and continuing calibration blanks were analyzed at the proper frequency. There was no qualification of data based on recoveries of the method blanks. The MS/MSD samples were analyzed at the proper frequency. Manganese in one sample was qualified "J" based on the recovery in the MS/MSD (MW516). The percent recoveries for the post digestion spike were all within the acceptance criteria. Chromium and iron in a sample and duplicate were qualified "J" based on exceeding the RPD (MW203). Iron and total and dissolved manganese were qualified "J" in a sample and duplicate based on exceeding the RPD (MW509). LCS samples were analyzed at the proper frequency. All LCS recoveries were within acceptance criteria. Dissolved manganese for one sample results were all within the acceptance criteria. All internal check standards were within the acceptance criteria. Review of calculations met acceptance criteria.
- Chloride, Nitrate, and Sulfate—All calibrations were within the acceptance criteria. All method blanks were run at the proper frequency. All method blanks were confirmed nondetect. LCS samples were analyzed at the proper frequency and were within acceptance criteria. MS/MSD samples were analyzed at the proper frequency and were within acceptable limits. Review of calculations met acceptance criteria.
- Methane, Ethane, and Ethene—All initial and continuing calibrations were performed at the proper frequency and within acceptance criteria. A review of raw data, including chromatograms of standards used were found to be acceptable. Method blanks were analyzed at the proper frequency. Raw data were reviewed and confirmed no detections present in the method blank. All percent recoveries for the MS and MSD were within acceptance criteria. The LCS and LCSD samples were analyzed at the proper frequency and were all within the acceptance criteria. Calculations were reviewed and confirmed.

All soil samples were reported on a dry weight basis. All holding times for soil and water samples were met. Field blanks and equipment blanks were collected at a rate of 5%. All results were acceptable. Trip blanks were collected one per cooler. All results were acceptable.

#### 4.10 DATA ASSESSMENT AND VERIFICATION

Data assessment and verification were performed on 100% of the data. Data verification includes checking methods, units, reporting limits, holding times, and analytical completeness. Exceptions to the data verification were noted in the data assessment package and were considered during data assessment.

Data assessment considered results of the Level IV data validation, data verification, laboratory data qualifiers, laboratory comments, and sampler's comments. All data were found to be of known quality, and it was determined that decisions could be made from the data based on the review.

The RDSI field investigation achieved a high degree of completeness as summarized below. For the SWMU 211-A soils VOC characterization, sampling and analysis accomplished the following:

#### • Number of soil borings

- Twenty-six of 27 initially located soil borings were sampled.<sup>3</sup>
- Four of four additional borings were sampled in the vicinity of the planned soil boring with highest average VOC levels (211-A-038 through 211-A-041).
- Twelve contingency borings were sampled (211-A-029 through 211-A-037 and 211-A-042 through 211-A-044), of 10 originally planned contingency borings.

### • Number of VOC analyses

- Five hundred forty-one of a potential 548 sample depths (98.7%) were characterized in the soil borings.
- Five thousand eight hundred eighty-two of a potential of 5,954 field PID readings (98.8%) were measured in the soil borings.

For SWMU 211-B soils VOC characterization, sampling analysis accomplished the following:

### • Number of soil borings

- Thirteen of 13 initially located soil borings were sampled.
- Four of four borings were sampled in the vicinity of the planned soil boring with highest average VOC levels (211-B-015, 211-B-016, 211-B-019, and 211-B-020).
- Two of the allotted six contingency borings were sampled (211-B-017 and 211-B-018).

# • Number of VOC analyses

- Two hundred forty-six of a potential of 249 sample depths (98.8%) were characterized in the soil borings.
- Two thousand six hundred fifty-one of a potential of 2,693 field PID readings (98.4%) were measured in the soil borings.

# 4.11 UNCERTAINTY EVALUATION

Factors that may affect uncertainty in site characterization data sets may include the following:

- Results and frequencies of quality control samples, quality control exceedances, and qualifiers;
- Biases and trends in the data; and
- Project completeness.

<sup>&</sup>lt;sup>3</sup> The FFA parties concurred to not sample soil boring 211-A-007.

As documented in Section 4.9, quality control exceedances and the occurrence of data qualifiers are sparse. Consequently, these factors are not envisioned to affect substantially the utility of the data in regard to estimation of the extent and mass/volume of VOCs in the UCRS and upper RGA at SWMUs 211-A and 211-B and associated decisions with regard to selection of a final remedy for these sites.

Sampling and analysis protocols identified in the RDSI characterization plan were selected to minimize the loss of VOCs, thereby reducing the potential or uncertainty associated with underestimating the presence of VOCs. The field investigation followed the characterization plan for sample technique and laboratory methods. A fixed-based laboratory, offering same day courier service with overnight analyses, was used for the VOC analyses and provided a degree of quality control that was superior to that which would have been provided if VOC analyses were conducted using the field laboratory option contained in the characterization plan.

The objective of the RDSI was to characterize the extent and mass/volume of VOC soil contamination in the UCRS and upper RGA at SWMUs 211-A and 211-B. The RDSI characterization plan (provided in DOE 2012a) was designed specifically to reduce the potential for decision error through an underestimation of mass through the identification and selection of the highest VOC concentration samples. Each 60-ft deep borehole core was divided into 5 ft segments over which field screening using a PID was conducted to identify intervals for sample collection and shipment for off-site VOC analysis. This approach was intended to ensure that the resulting VOC mass/volume calculations did not underrepresent the VOC mass/volume present in the subsurface. This approach essentially imposed a bias on the resulting VOC mass/volume calculations for each interval and correspondingly served to reduce the potential for underestimating VOC mass/volume.

Field PID measurements were a primary basis for selection of the sample interval within each 5-ft core from the soil borings. <sup>4</sup> These PID responses were reviewed to assess the potential for trends and biases to be present in the data set. The distribution of maximum PID readings in each 5-ft core is as follows:

	SWMU 21	1-A	<b>SWMU 211-B</b>		
# Cores	408		228		
# Measurements	4,488		2,508		
PID	Number of	% of	Number of	% of	
Measurement	Detections of	Detections of	Detections of	Detections of	
Location in Core	Maximum	Maximum	Maximum	Maximum	
0.1 ft	27	14.8	26	14.4	
0.5 ft	28	15.4	23	12.8	
1.0 ft	16	8.8	18	10.0	
1.5 ft	18	9.9	10	5.6	
2.0 ft	8	4.4	12	6.7	
2.5 ft	11	6.0	9	5.0	
3.0 ft	12	6.6	17	9.4	
3.5 ft	12	6.6	22	12.2	
4.0 ft	14	7.7	15	8.3	
4.5 ft	19	10.4	19	10.6	
4.9 ft	17	9.3	9	5.0	

<sup>&</sup>lt;sup>4</sup> In many soil cores with low contamination by VOCs, the PID readings were constant across the core. In those cases, the texture of the soil core was used to define the sample location. Sandy intervals were sampled preferentially.

The percentage of detection of the maximum PID response was notably higher in the upper 0.5 ft of the cores. Follow-up with the manufacturer of the PID used in the field investigation identified moisture interference on the PID lamp as a possible cause for bias. Accordingly, the distribution may indicate a potential bias in PID responses associated with moisture interference.

The effect of moisture-impacted PID response is a potential underestimation of the VOCs mass/volume for those intervals where the maximum PID measurement was in the upper 0.5 ft of the soil core. At SWMU 211-A, 86.5% of the sample locations were not impacted by moisture; at SWMU 211-B, 78.5% of the sample locations were not impacted by moisture. In general, the distribution of maximum PID response and experience of the field crew both indicate that the field PID scan correctly identified the sample interval where high VOC intervals were present deeper in the core. Moreover, the areas of soils with high VOC levels, as identified for the RDSI by the PID and verified with laboratory analysis, are consistent with historical soil analyses, as summarized in the conceptual site model of the RDSI characterization plan (in DOE 2012a).

The RDSI method of using the maximum PID response to select the sample interval intentionally biases the results high compared to random sampling or multi incremental sampling. The moisture-impacted PID response would have led to oversampling of the upper 0.5-ft interval only in those cores with little VOC content. Thus, moisture-impacted PID response would not affect significantly the standard deviation of the data set and would have little influence on the estimation of the mass/volume of VOCs at either SWMU.

In regard to determination of the extent of VOC source material, the field investigation design employed a near uniform sampling grid of both SWMUs 211-A and 211-B. Contingency borings were utilized, as provided in the RDSI characterization plan, to further delineate the extent of the area of VOC contamination based on observed results for samples collected and analyzed based on 24-hour turnaround (quick-turn). Quick-turn analytical results and corresponding plans for contingency locations were reviewed with EPA and Kentucky Division of Waste Management project personnel to obtain concurrence on planned locations and attain project objectives (i.e., determination of the extent of source based VOC mass). This approach also reduced the potential for bias related to delays associated with extended turnaround times for receipt of analytical results and less timely interaction among the FFA parties on contingency sample placement.

Observed trends and potential impacts on uncertainty and decision making were observed as follows. Results for TCE in soil at SWMU 211-A define two discrete areas where average borehole soil TCE concentrations exceed the soil cleanup goal of 75  $\mu$ g/kg. Each area has unique spatial attributes. In the eastern portion of SWMU 211-A, the distribution of borings where the average borehole TCE concentration exceeds 75  $\mu$ g/kg defines a north/south feature (95-ft long by 15-ft wide), whereas TCE concentrations in the western portion of the investigation area are distributed equidimensionally (70 ft in the north/south direction by 65 ft in the east/west direction). In both areas at SWMU 211-A, the RDSI data adequately define the extent of VOC concentrations in the UCRS and upper RGA that exceed the identified cleanup goal.

The soil VOC data for SWMU 211-B conforms to the anticipated distribution based on the site conceptual model. The distribution of average borehole TCE concentration that exceed the cleanup goal of 75  $\mu$ g/kg forms a discrete area on the south side of the C-720 Building (50-ft long by 15-ft wide). The presence of the building precluded delineation of the extent of contamination to the north. The delineation of extent is sufficient to support a decision for SWMU 211-B based on the assumption of a release at the surface on the south side of C-720.

Historical VOC results in the database were used to supplement the RDSI results and assist in the estimation of VOC mass/volume for both SWMUs 211-A and 211-B. The distribution of VOC mass/volume based on the RDSI for 211-B generally conformed to the VOC mass/volume distribution, as defined by historical VOC concentrations. The distribution of VOC mass/volume for SWMU 211-A was significantly enhanced by the inclusion of information gathered during the RDSI. The inclusion of historical VOC data reduces the potential for underestimating VOC mass/volume based on the use of RDSI results only.

The RDSI analysis of extent and mass/volume of TCE contamination, developed with input from the FFA parties, was based on kriging all sample points compared to an interpolation of the borehole-average TCE analyses (the statistical metric used to develop the remediation goals for SWMUs 211-A and 211-B). Kriging techniques can be used to describe and model spatial patterns, predict values at unmeasured locations, and assess the uncertainty associated with a predicted value at the unmeasured locations. The technique provides a "standard error" that may be used to quantify confidence levels. The RDSI data were evaluated using 50% and 90% confidence intervals, where the confidence interval indicates the probability that the predicted mass of VOC contamination in the subsurface at the SWMU, given the distribution of samples, either exceeds or is less than the estimate. The resulting mass/volume estimate for TCE, based on the 90% confidence interval, provided a more robust approach than initially envisioned and presented in the RDSI characterization plan (DOE 2012a). The method used reduces the potential for underestimating VOC mass through the use of the 90% confidence interval in combination with interpolation using individual sample results and inclusion of historical data.

The primary conclusions of the soils VOC data are (1) definition of the location and extent of contaminated soils that exceed the remediation goals identified in the ROD (DOE 2012b) for SWMUs 211-A and 211-B (e.g., 0.075 mg/kg TCE) and (2) estimation of the mass and volume of the TCE contamination. The soil VOC data generated, in combination with historical data, are sufficient and appropriate to define an upper bound for the estimate of the VOC mass and volume to support the selection of a final remedial action for VOCs at each SWMU.

# 4.12 THREE-DIMENSIONAL ANALYSIS

Results of the UCD soil samples from the RDSI and historical data from OREIS are inputs to three-dimensional contamination models for SWMU 211-A and SWMU 211-B using the EVS-ES software. The area historical data in OREIS come from the WAG 27 RI (DOE 1999) and the Southwest Plume SI (DOE 2007). These models estimate the extent of TCE soil impacts and the total TCE mass in soil at each SWMU.

EVS is similar to other environmental decision support software (DSS), such as SitePro and Spatial Analysis and Decision Assistance, and was evaluated by EPA and DOE in 1998 alongside five other DSS packages. EVS underwent an environmental technology verification report in March 2000 that concluded that "the main strengths of EVS-PRO are its outstanding 3-D visualization capabilities and its capability to rapidly process, analyze and visualize data" and "the demonstration showed the EVS-PRO software can be used to generate reliable and useful analyses for evaluating environmental contamination problems."

Several interpolation techniques, including inverse distance weighting, nearest neighbor, and kriging, were evaluated, with kriging ultimately being selected as the primary interpolation technique. Kriging is a stochastic technique similar to inverse distance weighted averaging in that it uses a linear combination of weights at known points to estimate the value at the grid nodes. Kriging is named after D. L. Krige, who used kriging's underlying theory to estimate ore content. Kriging uses a variogram (a.k.a.

semivariogram), which is a representation of the spatial and data differences between some or all possible "pairs" of points in the measured data set. The variogram then describes the weighting factors that will be applied for the interpolation.

It is acknowledged that there are significant uncertainties associated with providing a mass estimate of DNAPL using kriging. Using kriging, however, is still a useful and valid approach to estimate the extent of the source area at various isoconcentration levels below the threshold of residual saturation. Kriging also provides insight about the mass distribution at differing isoconcentration levels. Uncertainty has been considered by estimating mass at different levels of statistical confidence. By kriging data at every node of the model, an average value along with a standard deviation is calculated, thus providing a range of estimated TCE concentrations and ultimately mass. A level of significance of 0.1 (i.e., 90% confidence interval) was used in modeling the geometry and mass of TCE above 75  $\mu$ g/kg in order to address uncertainty in the estimates.

Each SWMU contaminant model was based on a five-layer geologic model. Analytical results were log processed in the model. The Horizontal/Vertical Anisotropy Ratio parameter, which allows the model to take into consideration expected differences in fluid flow through the soil matrix, was set to a value of 1.5. The Octant Search method was used to determine which sample points are selected for inclusion in the kriging matrix. This method sets a maximum number of points for each octant, which helps offset bias effects of sampling distribution irregularities. The model used a soil density of 1.4 gram per cubic centimeter (g/cc) and a chemical density of 1.46 g/cc.

Model results of TCE soil impacts for SWMU 211-A and SWMU 211-B are illustrated later in this report as the 50% and 90% confidence limits of 75  $\mu$ g/kg soil TCE and the 90% confidence limit of 1,000  $\mu$ g/kg soil TCE. Soil TCE mass estimates for SWMUs 211-A and 211-B are reported as the 90% maximum confidence level for the source volume statistical evaluation.

Appendix B provides a CD containing viewable three-dimensional model EVS-ES files. Appendix C is the sensitivity analysis of the source volume estimate.

# 5. SWMU 211-A RDSI SAMPLE RESULTS

# **5.1 LITHOLOGY**

Soil lithology logs that provide a detailed description of soil type and HU transitions are included in Appendix D. Within the SWMU 211-A investigation area, lithology logs reveal the presence of fill material (gravelly fine sand) to a typical depth of approximately 2 ft, underlain primarily by silt with very fine sand representing the HU1 to a typical depth of approximately 20 ft bgs. HU2 was identified from approximately 20 ft bgs to approximately 35 ft bgs and consisted primarily of fine sand and silt with some gravel. HU3, primarily consisting of silt with fine sand and clay, was identified from approximately 35 ft bgs to 60 ft bgs.

# **5.2 SOIL SAMPLE RESULTS**

Forty-two DPT soil boring locations (25 original, 18 contingency), shown in Figure 4, were performed on and extending north of the parking lot off the northeastern portion of the C 720 Building. Collected soil cores were screened approximately every 0.5 ft using a PID to identify intervals of maximum organic vapor response, if present. Soil samples were collected from the 0.5 ft interval of maximum PID reading for each 5-ft soil core and sent by courier to the fixed-base laboratory for overnight VOC analysis. The laboratory preliminary analytical results were available by 8:30 a.m. on Monday for samples collected on the previous Friday and by 8:30 a.m. Tuesday through Friday for samples collected the previous day. The next day laboratory results were used to assess actively whether additional borings were needed by comparison of the average contaminant concentration<sup>5</sup> for the samples from each boring to the remediation goal. If the average exceeded the remediation goal, then one or more contingency borings were required.

A total of 541 soil samples was collected from 42 soil boring locations. Soil sample VOC results are summarized in Table 6 and presented in Appendix E. Soil sample depths ranged from 0.1 ft bgs (374.55 ft asml) to 66.5 ft bgs (307.49 ft amsl). The maximum measured TCE result was 4,800  $\mu$ g/kg from location 211-A-036 at a depth of 47.5 ft bgs (326.97 ft amsl). The observed maximum *cis*-1,2-DCE and VC results of 110  $\mu$ g/kg and 28  $\mu$ g/kg (both results "J" qualified indicating estimated values), respectively, also were collected at soil boring location 211-A-036, at a depth of 44.5 ft bgs (329.97 ft amsl). The maximum measured 1,1-DCE result was 4,400  $\mu$ g/kg from location 211-A-004 at a depth of 40.1 ft bgs (333.18 ft amsl). Soil boring locations 211-A-004 and 211-A-036 are located in the western portion of the investigation area. *Trans*-1,2-DCE was not detected in the collected soil samples above laboratory detection limits. At 12 borings (29%), the borehole average concentration exceeded the remediation goal. A total of 97 soil samples (18%) exceeded the remediation goal. In general, the highest concentrations were noted in the 30 to 50 ft bgs depth range.

Figure 6 illustrates all of the soil TCE analyses for the SWMU 211-A investigation area, overlaid on a map. For reference, soil TCE analyses greater than 75  $\mu$ g/kg (the borehole average project remediation goal) are noted by yellow highlight.

Subsequent to development of the RDWP (DOE 2012a), the approach for determining the distribution of TCE mass within the UCRS that exceeds soil TCE concentrations of 75  $\mu$ g/kg was refined based on discussion among the FFA parties. The revised approached included the use of historical TCE soil data for the UCRS contained in OREIS, analytical results from the RDSI, and the use of the spatial

<sup>&</sup>lt;sup>5</sup> The average contaminant concentration for a borehole was calculated using one half of the laboratory reporting limit for nondetect analyses and using the greater concentration where analyses of duplicate samples were available.

Station	Date Collected	TCE [µg/kg]	1,1-DCE [µg/kg]	<i>cis-</i> 1,2- DCE [µg/kg]	trans-1,2- DCE [μg/kg]	VC [µg/kg]
	Groundwater Protection Remediation Goal		137	619	5290	570
211-A-001	8/29/2012	3.4	***	***	***	***
211-A-002	8/30/2012 & 8/31/2012	161	2.5	2.0	***	***
211-A-003	9/12/2012	18*	4.1	0.5	***	***
211-A-004	8/31/2012 & 9/4/2012	552	763	9.1	***	***
211-A-005	9/4/2012	175	163	5.2	***	5.9
211-A-006	9/26/2012	8.3	7.4	0.6	***	***
211-A-008	9/20/2012	12*	6.8	0.6	***	***
211-A-009	9/20/2012	40*	4.8	0.8	***	***
211-A-010	8/16/2012, 9/13/2012 & 9/17/2012	135	3.4	2.3	***	***
211-A-011	8/17/2012	12*	6.7	0.3	***	***
211-A-012	9/17/2012	4.9	11	0.6	***	***
211-A-013	9/4/2012 & 9/5/2012	34*	45	4.4	***	2.4
211-A-014	9/5/2012	12	24*	0.8	***	***
211-A-015	9/6/2012	36*	19	0.8	***	***
211-A-016	9/27/2012	58*	14	1.7	***	***
211-A-017	9/21/2012	276	***	5.6	***	4.3
211-A-018	9/11/2012 & 9/12/2012	46*	5.8	***	***	***
211-A-019	9/12/2012	1.3	10	0.5	***	***
211-A-020	9/24/2012	297	6.7	3.7	***	***
211-A-021	9/6/2012	19	32	1.8	***	0.2
211-A-022	9/27/2012	12*	4.1	0.6	***	***
211-A-023	9/11/2012	19*	4.4	0.5	***	***
211-A-024	9/10/2012	9*	***	0.4	***	***
211-A-025	9/10/2012	213	***	13	***	***
211-A-026	9/7/2012	4.8	4.8	1.2	***	0.3
211-A-027	9/11/2012 & 9/18/2012	55*	1.6	0.7	***	***
211-A-028	9/24/2012	804	904	12	***	***
211-A-029	9/25/2012	351	348	7.0	***	***
211-A-030	9/25/2012	12*	14	1.5	***	***
211-A-031	9/26/2012	32*	***	1.1	***	***
211-A-032	9/28/2012	6.6	***	0.6	***	***

Table 6. Soils VOC Data (Average Borehole Concentration) for SWMU 211-A

Station	Date Collected	TCE [µg/kg]	1,1-DCE [µg/kg]	<i>cis</i> -1,2- DCE [µg/kg]	<i>trans</i> -1,2- DCE [μg/kg]	VC [µg/kg]
Groundwate Remediation		75	137	619	5290	570
211-A-033	10/1/2012	166	140	7.1	***	***
211-A-035	10/2/2012	170	131*	4	***	***
211-A-036	10/3/2012	1,171	1,043	20	***	9
211-A-037	2/25/2013	0.5	***	***	***	***
211-A-038	2/25/2013	14	3.3	3.9	***	2.9
211-A-039	2/26/2013	0.6	7.3	0.57	***	***
211-A-040	2/26/2013	***	2.5	***	***	***
211-A-041	2/27/2013	21*	36*	4.3	***	1.2
211-A-042	2/27/2013	28*	20	4.2	***	0.6
211-A-043	3/4/2013	11	2.5	15	***	***
211-A-044	3/6/2013	14*	3.4	131*	***	14

 Table 6. Soils VOC Data (Average Borehole Concentration) for SWMU 211-A (Continued)

Notes:

1. Groundwater Protection Remediation Goals from *Remedial Design Work Plan for Solid Waste Management Units 1,* 211-A, and 211-B Volatile Organic Compound Sources for the Southwest Groundwater Plume at the Paducah Gaseous Diffusion Plant, Paducah, Kentucky, (DOE 2012a).

2. \*—Indicates average concentrations that are below the Groundwater Protection Remediation Goal, but at least one sample exceeded the remediation goal.

3. \*\*\*-Indicates average concentration not calculated as all boring analyses were "U" qualified (compound analyzed for but not detected at or below the lowest concentration reported) for specific VOC.

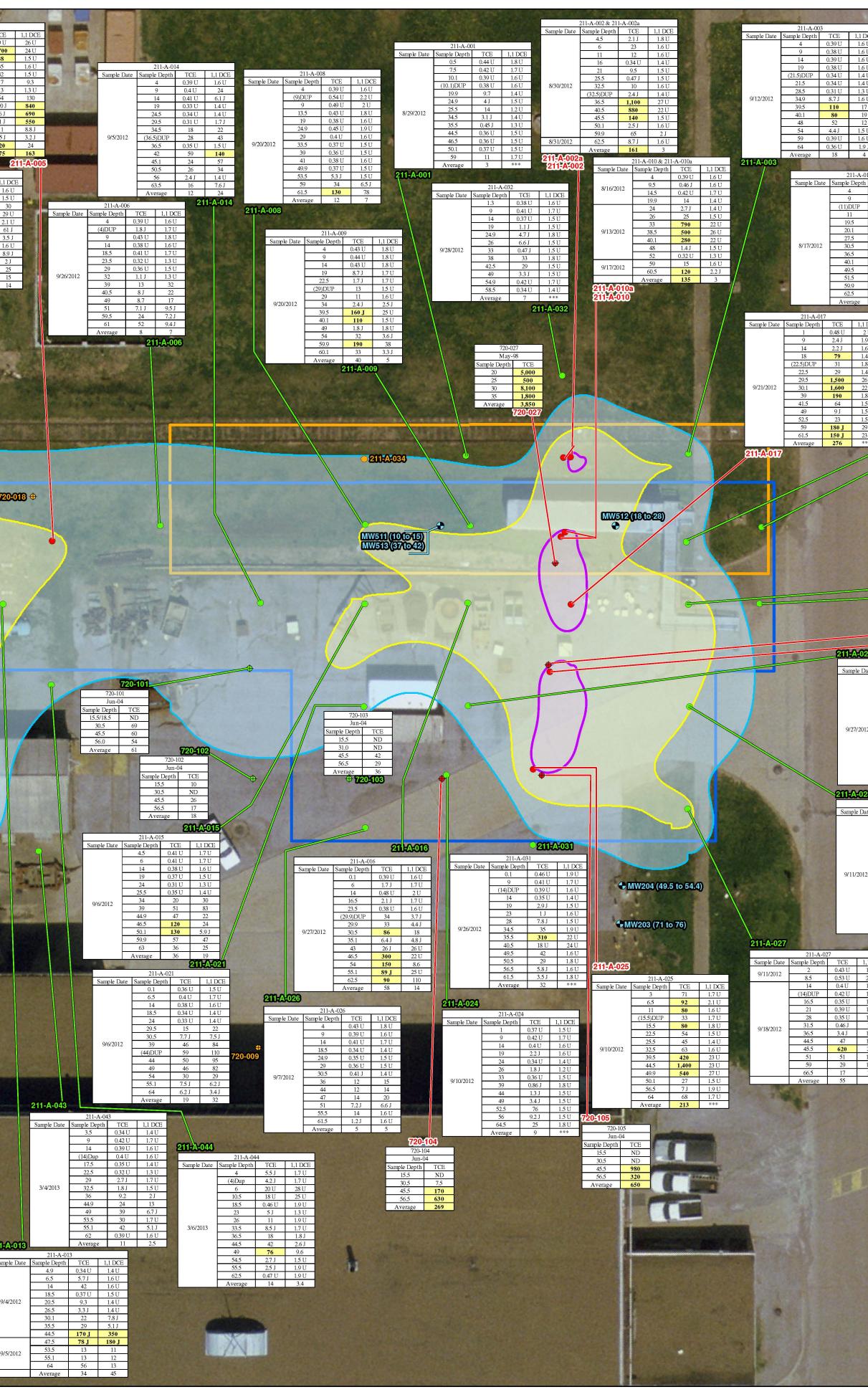
4. For "U" qualified analyses, a value of one half the concentration reported was used in calculating the average borehole concentration.

5. Yellow shading and bold text indicate an exceedance of Groundwater Protection Remediation Goals.

6. Soil boring 211-A-007 was not collected.

7. Soil boring 211-A-034 was collected and archived. Boring was not logged or screened for VOC impacts.

	In C. W.	in the		Sample Date	211-A-004           Sample Depth         TCE         1,1 DCE           4         0.39 U         1.6 U           9         0.38 U         1.6 U	211-A-005           Sample Date         Sample Depth         TCE           4         19 U         6         1,700           14         88         88
	1000			8/31/2012	14         0.36 U         1.6 J           16.5         0.33 U         18           24.9 <b>1,700 1,600</b> 27 <b>960 970</b> 30.1 <b>620 900</b> 35.1 <b>1,200 1,400</b> 40.1 <b>2,400 4,400</b>	15.1         35           (15.1)DUP         42           23.5         17           26         13           34.9         54           35.5         190 J           43.5         96 J
				9/4/2012	48.1         2,400         4,400           48.5         17 U         480           53.5         33 J         110 J           59.9         97         12           61         160         23           Average         552         763           211-A-004         21	45.5         571 J           53         11           55.5         65 J           60.5         120           Average         175
				Sample Date Sa	211-A-028 mple Depth TCE 1,1 DCE	211-A-030           mple Date         Sample Depth         TCE         1,11           9         0.39 U         1.6           14         0.36 U         1.5           19         0.36 U         3           23.5         21 U         29
	15	Sample E	211-A-039         Sample Date         Sample Depth           Date         Sample Depth         TCE         1,1 DCE         3           9         0,41 U         1.7 U         9         14           14         0,44 U         1.8 U         14         14           (14)Dup         0,46 U         1.9 U         16.5         12           19         0,36 U         1.5 U         22         2		4         0.38 U         1.6 U         9         9         0.43 U         1.8 U         1.8 U         1.4 U         1.7 U         9         0.76 J         55         22.5         0.44 U         1.8 J         1.8 J         26         210         290         34         220 J         55 J         55         5	29.9         0.51 U         2.1           32.5         97 J         6.           39         0.38 U         3.           40.1         0.38 U         3.           40.5         4.8 U         3.9           54.5         4.8 J         2           58         20         2
		2/26/20	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.34 U 1.4 U 0.34 U 1.4 U 0.41 U 1.7 U 0.35 U 1.5 U 0.4 U 1.7 U 0.37 U 2.4 J	38.5         3,700         4,200           42.5         2,800         3,800           48         1,600         1,800           50.5         1,700         1,400           55.1         42         79           61         180         66           Average         804         904	61 12 1 Average 12 1
			51.5         0.39 U         57           56         1 J         1.5 U           64         4.5 J         2.3 U           Average         0.6         7.3 <b>211-A-039</b>	0.37 U 1.5 U 0.36 U 21 0.38 U 3.2 J *** 2.5 211FA-040	Average 804 904 211-A-028	
		Sample Date	211-A-036 & 211-A-036a           Sample Depth         TCE         1,1 DCE           0.1         0.41 U         1.7 U           9         0.47 U         1.9 U           14.7         0.42 U         1.7 U           19         0.67 J         2.1 J           22         280 J         31 U	1.22		
		10/3/2012	26.5         810         340           31.5         1,400         1,600           35.5         2,800         3,700           44.5         3,800         3,900           47.5         4,800         3,300           50.1         1,300         690			
		211-A-037 •	55.5         3 J         1.5 U           61         33         12           Average         1,171         1,043           211-A-036a         211-A-036			72
	Sample Date	211-A-037           Sample Depth         TCE         1,1 DCE           4         0.4 U         1.6 U           9         0.39 U         1.6 U           14         0.42 U         1.7 U           12         22	CE         1,1 DCE           37U         1.5 U           0U         27 U           3U         32 U           41 U         1.7 U			
	2/25/2013	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	41 U 1.7 U 26 1.6 U 36 U 1.5 U 37 U 1.5 U 30 1.6 U 51 2.1 98 J 1.6 U		A	·/ ſ
	0000	54.5         2.2 J         1.7 U         56         2           56.5         1.4 J         2.5 U         62         52	.6J     1.5 U       20     3.6 J       11     1.8 J       14     3.3			
	T	211-A-0 Sample Date Sample Depth 4 9 14.5 18.5 (18.5)Dup				17
		$ \begin{array}{c}     24 \\     27 \\     34.5 \\     39 \\     41 \\     49 \end{array} $	0.53 U         2.2 U           0.34 U         1.4 U           1.7 J         1.6 J           71         120           76         140           33         170			
			18         26           27         2.2 J           68         21           21         36 <b>211-A-042</b> 211-A-042           211-A-042           211-A-042           211-A-042           211-A-042           211-A-042           1.1 - CE			
			9         0.41 U         1.7 U           14.5         0.39 U         1.6 U           17         0.37 U         1.5 U           22.5         0.33 U         1.4 U           27.5         0.34 U         1.4 U           31         0.38 U         1.6 U			ATA
		2/	227/2013         39         61         68           42         120         94           48         82         40           54.9         40         21           57         0.38 U         1.6 U           62.5         27         6.4 J           Average         28         20		211-A-035	1000
	Legend		Avelage 20 20	Sample Date         Sample Depth         TCE           1.9         0.4 U         8.6         0.39 U           13.4         0.38 U         13.4         0.38 U           18.5         1.6 J         24         7.6 J	1.7 U 1.6 U	u*
	•	Soil Boring Location with Average Soil Concentration Exceeding One Soil Boring Location with Average Soil Concentration Less than Both F Archive Core Soil Boring Location - Not Sampled		$   \begin{array}{r}       \frac{24}{27} & 7.03 \\       \frac{27}{2.1 \text{ J}} \\       30.5 & 35 \\       37 & 580 \\       (41.5)\text{DUP} & 420 \\       41.5 & 400 \\       49 & 210 \\       49 & 210 \\       49 & 210 \\       49 & 210 \\       40 & 210 \\  $	30       1.7J       27       590       350       400       26 J	
	<ul><li>♦</li><li>♦</li></ul>	Historic Soil Boring Location with Average Soil Concentration Exceedi Historic Soil Boring Location with Average Soil Concentration Less tha		51.5         680           55.5         17           66.5         25           Average         170	360 1.7 U 9.3 J 131 211-A-033 021 - D - D	<b>211:A-029</b> 211-A-029
13 JRB	•	Historic Archive Core Soil Boring Location - Not Sampled Monitoring Well Location (screen interval ft BLS) Area defined by 90% Confidence Level TCE Concentrations greater the	an 1,000 µg/kg	211-A Sample Date Sample Dep 4 9 14 14 19 21.5		ample Depth         TCE         1,1 DCE           4         0.4 U         1.7 U           9         0.51 U         2.1 U           14         0.4 U         1.7 U           18         0.31 U         1.3 U           24.9         23         18           28.5         440         240
'OC Results.mxd 19 Sep 20		Area defined by Nominal (50%) Confidence Level TCE Concentrations Area defined by 90% Confidence Level TCE Concentrations greater the General RDSI Sample Area		29.9 (34)DUP 10/1/2012 34 36 44.5 49.5	3.6 J         2.4 J           12         1.9 J           60         16           1,100         1,100           700         540           300         240	(32)DUP         110         77           32         480         360           38         2,600         2,900           40.5         870         880           48.5         270         350           50.5         22         27
4Y2013/SWIMU 211 A SS Vi	Parame	SWMU 211-A Groundwater Protection Remediation Goals	Contour (μg/kg)         Total Area (ft <sup>2</sup> )         Area (ft <sup>2</sup> ) Exclusive           90% CL 75         34,000         24,500	50.5 56.5 62 Average	130 J         58 J           0.48 J         1.7 U           14         3.6 J           166         140	55.1         3.8 J         4.4 J           64         100         15           Average         351         348
VDs\SWMU_211_FEB2013\MA	Trichloroe 1,1-Dichloro Notes: 1. Results are	e presented in microgram per kilogram (µg/kg).	Nominal 75         13,200         9,500           90% CL 1000         3,700         3,700			C-720 Building 2114
VOGISVFR5082 PaducahV	3. Only thos 4. DUP indic 5. J indicate 6. U indicate 7. Yellow sh	epth is presented in feet below land surface (ft BLS). e individual volatile organic compounds (VOC) with a result exceeding ates duplicate sample. s an estimated value. is compound analyzed for but not detected at or below the lowest cor aded, bold text indicates an exceedance of the Groundwater Protectio	ncentration reported. on Remediation Goal UCRS Soil Cleanup Target Level for VOC	s.		9/4
ath: (Titusville-01\Data))	9. TCE isople 10. Section 7 confiden	ates average concentration not calculated as all boring samples were <sup>6</sup> oths are based upon individual soil sample results over all depths of sau 7 of the Final Characterization Report includes explanation of the mod ce levels. f 2009 Aerial: Williams Aerial & Mapping, Inc.	mpling.			9/5



$\begin{array}{c} DCE \\ 6 U \\ 4 U \\ 4 U \\ 4 U \\ 3 U \\ 6 U \\ 17 \\ 19 \\ 12 \\ 5 U \\ 6 U \\ 17 \\ 19 \\ 12 \\ 5 U \\ 6 U \\ 17 \\ 19 \\ 12 \\ 5 U \\ 6 U \\ 17 \\ 19 \\ 12 \\ 5 U \\ 6 U \\ 19 \\ 19 \\ 12 \\ 5 U \\ 6 U \\ 10 \\ 19 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10$	720-030 *         * 720-029	True North
3.2 J       1.5 U         8.3 J       19         8.6 J       28         12       7         20       211-A-011         1.4 U       9/17/2012         1.8 U       9/17/2012         1.5 U       211-A-011         1.5 U       9/17/2012         1.5 U       211-A-012         32 U       8         9       9/17/2012         1.5 U       9/17/2012	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
$\begin{array}{r} 9/12/201\\ \hline 211-A-022\\ \hline \\ $	Average 46 6 15.5 30	
Date         Sample Depth         TCE         1,1 DCE           1         0.4 U         1.7 U           7         0.37 U         1.5 U           14.9         0.36 U         1.5 U           18         0.36 U         1.5 U           20.1         0.33 U         1.6 J           (20.1)DUP         0.36 U         7.2 J           25.5         0.33 U         1.6 J           (20.1)DUP         0.36 U         7.2 J           25.5         0.33 U         1.8 U           34.9         0.37 U         1.5 U           36.5         0.43 U         1.8 U           43         0.39 U         7.9 J           49         1.4 J         9.9           53         66         8.6 J           55.1         130         6.9 J           62         73<11		
		30 Feet
	Paducah Gaseous Diffusion Plant Kevil, Kentucky Ceosyntec consultants Titusville, FL May 2013	Figure <b>6</b>

analysis EVS-ES software to contour the 90% confidence limit of 75  $\mu$ g/kg soil TCE for SWMUs 211-A and 211-B. Figure 6 shows the lateral extent of 75  $\mu$ g/kg soil TCE (90% confidence limit).

In addition, Figure 6 shows the smaller areas of 75  $\mu$ g/kg soil TCE (50% confidence limit) and 1,000  $\mu$ g/kg soil TCE (90% confidence limit) for comparison. These depictions define the extent of TCE contamination.

Total organic carbon (TOC) results for SWMU 211-A ranged from 150 milligram/kilogram (mg/kg) to 650 mg/kg with an average concentration of 396 mg/kg. TOC sample results are presented in Table 7.

Station	Date Collected	Sample Top Depth/Elevation [ft bgs/ft amsl]	Sample Bottom Depth/Elevation [ft bgs/ft amsl]	Hydrologic Unit	TOC [mg/kg]
		15.5/358.59	16/358.09	HU1	420
211-A-006	9/26/2012	20.5/353.59	20.5/353.59	HU2	650
		40.5/333.59	40.5/333.59	HU3	340
	8/16/2012	9/365.33	9/365.33	HU1	500
211-A-010		19.5/354.83	19.5/354.83	HU2	370
	9/13/2012	40/334.33	40/334.33	HU3	220
		15/360.46	16359.46	HU1	400
211-A-012	9/17/2012	25/350.46	26/349.46	HU2	490
		37/338.46	38/337.46	HU3	410
	9/18/2012	14/360.62	15/359.62	HU1	530
211-A-027		25/349.62	25.5/349.12	HU2	270
		36.5/338.12	37/337.62	HU3	150

Table 7. Summary of Soils TOC Data for SWMU 211-A

# **5.3 GROUNDWATER SAMPLE RESULTS**

In the area of SWMU 211-A, RGA groundwater flows to the north and northeast. MW203 (RGA) is screened in the RGA from 71 to 76 ft bgs (298.95 to 303.95 ft amsl) and is located 16 ft upgradient of the defined area of VOC contamination at SWMU 211-A. The results of groundwater samples collected from MW203 represent ambient water quality in the area associated with the eastern half of SWMU 211-A. The prevailing hydraulic gradient in the UCRS is vertically downward, and groundwater in the UCRS is a source of recharge to the RGA. UCRS well MW204, screened from 49 to 54 ft bgs (320.44 to 325.34 ft amsl), is similarly located south (upgradient) of the defined VOC contamination in the east half of SWMU 211-A. Thus, results for MW204, similarly, represent ambient water quality for the investigation analytes. (MW204 water quality is influenced by an unidentified technetium-99 source, up to 1,240 pCi/L.) UCRS wells MW511 (screened 10 to 15 ft bgs/359.03 to 364.03 ft amsl), MW512 (screened 18 to 28 ft bgs, 346.68 to 356.68 ft amsl), and MW513 (screened 37 to 42 ft bgs, 332.20 to 337.02 ft amsl) are located within the eastern half of the area impacted by VOC contamination at SWMU 211-A, crossgradient to the areas of highest soil VOC levels. The groundwater from samples obtained from these wells reflects crossgradient impacts from VOC contamination identified with SWMU 211-A. Currently, there are no monitoring wells located in the western portion of SWMU 211-A or downgradient of SWMU 211-A.

Groundwater samples were collected during September and October 2012 from the MWs noted above: MW203 (RGA), MW204 (UCRS), MW511 (UCRS), MW512 (UCRS), and MW513 (UCRS). The groundwater samples were analyzed for VOCs, alkalinity, total and dissolved metals, ferrous iron, major anions, and dissolved gasses. Additionally, samples from MW511 and MW513 were analyzed for *Dehalococcoides mccartyi* (*Dhc*). Groundwater sample results are presented and are summarized in Table 8. Comparisons of the highest levels detected in the wells installed during the RDSI and the preexisting wells MW203 and MW204 follow.

**VOCs.** In the east half of SWMU 211-A, in the UCRS wells installed during the RDSI, contaminant levels were significantly higher in the deepest well, MW513.

	East Half of SWMU 211-A	Southeast of SWMU 211-A (Upgradient)				
	MW513 (deep UCRS well)	MW204 max value (UCRS well)	MW203 max value (RGA well)			
Trichloroethene (µg/L)	220 ("D" qualified)	76	110			
1,1-DCE (µg/L)	810 ("D" qualified)	17	6.7			
<i>cis</i> -1,2-DCE (µg/L)	12	18	29			

*Trans*-1,2-DCE and VC were not detected above individual laboratory detection limits in any of the SWMU 211-A groundwater samples. The presence of *cis*-1,2-DCE suggests that biologically mediated reductive dechlorination is occurring in the groundwater at SWMU 211-A. Groundwater VOC sample results are displayed in Figure 7.

**Dissolved Gases.** Among the UCRS wells installed for the RDSI at SWMU 211-A, all three dissolved gasses—ethane, ethene, and methane—are highest in the shallow well.

	East Half of SWMU 211-A	Southeast of SWMU 211-A (Upgradient)			
	MW511	MW204 max value	MW203 max value		
	(shallow UCRS well)	(UCRS well)	(RGA well)		
Ethane (µg/L)	0.41	0.039	0.097		
Ethene ( $\mu g/L$ )	0.32	0.1	0.49		
Methane (µg/L)	0.86	2.6	6.8		

Methane is produced by methanogenic bacteria conversion of acetate or reduction of carbon dioxide under anaerobic conditions. Methanogens and dechlorinating organisms thrive under similar conditions; therefore, the production of methane in groundwater is an indicator that conditions exist that are suitable for reductive dechlorination. Ethene is the final dechlorination product of TCE, while ethane is the product of ethene reduction. The presence of ethene/ethane provides a direct line of evidence that reductive dechlorination is proceeding to completion.

**Inorganic Anions.** Among the wells installed during the RDSI within the area impacted by VOC contamination in the east half of SWMU 211-A, chloride was measured at highest concentration in the deepest UCRS well, MW513, and the highest measured sulfate concentration was measured in the shallowest UCRS well, MW511. Nitrate was undetectable in both wells.

	East Half of SV	VMU 211-A	Southeast of SWMU	U 211-A (Upgradient)
	MW511 MW513		MW204 max value	MW203 max value
	(shallow UCRS well)	(deep UCRS well)	(UCRS well)	(RGA well)
Chloride (mg/L)	3.9	92	90	120
Nitrate (mg/L)	< 3	< 3	5.4	3.6
Sulfate (mg/L)	66	22	49	17

The nitrate and sulfate (electron acceptors) concentrations present are not at levels that would be anticipated to hinder the reductive dechlorination pathway. Additionally, sulfate is not present at an elevated concentration that has the potential to result in sulfide concentrations that are toxic to dechlorinating microorganisms.

**Metals.** Among the UCRS wells installed during the RDSI in the east half of SWMU 211-A, the highest measured levels of aluminum, iron, and lead were found in samples from the shallowest well, MW511; the highest levels of chromium and manganese were found in samples from the deepest well, MW513.

	East Half of S	WMU 211-A	Southeast of SWMU 211-A (Upgradient)		
	MW511	MW513	MW204 max value	MW203 max value	
	(shallow UCRS well)	(deep UCRS well)	(UCRS well)	(RGA well)	
Aluminum (mg/L)	1.77 ("N" qualified)	< 0.2 ("N" qualified)	0.736 ("N" qualified)	< 0.2	
Chromium (mg/L)	< 0.01	0.0409	0.284	0.202	
Iron (mg/L)	2.35	0.77	1.96	4.99	
Lead (mg/L)	0.00275	< 0.0013	0.00308	< 0.0013	
Manganese	0.204 ("N" qualified)	0.282 ("N" qualified)	0.0357	0.209 ("N" qualified)	

**Biological.** *Dhc* was not measured at a concentration greater than the reporting limits of 43 cells/milliliter (cells/mL) in MW511 and 17 cells/mL in MW513. The absence of detectable *Dhc* suggests that reductive dechlorination is not occurring at a high rate under current conditions.

Analyte	Date Collected	MW2	203	MW2	04	<b>MW51</b> 1	1	MW512	MW5	513
Total and Dissolved	l Metals									
	9/5/2012	0.2	U	0.64						
Aluminum (mg/L)	9/12/2012	0.2	U	0.659						
	10/22/2012	0.2	UN	0.736	Ν	1.77	Ν		0.2	UN
A.1	9/5/2012	0.2	U	0.2	U					
Aluminum, Dissolved (mg/L)	9/12/2012	0.2	U	0.2	U					
Dissolved (ilig/L)	10/22/2012	0.2	U	0.2	U	0.2	U		0.2	U
	9/5/2012	0.117		0.261						
Chromium (mg/L)	9/12/2012	0.114		0.284						
	10/22/2012	0.202		0.229		0.01	U		0.0409	
Classic	9/5/2012	0.01	U	0.01	U					
Chromium, Dissolved (mg/L)	9/12/2012	0.01	U	0.01	U					
Dissolved (ilig/L)	10/22/2012	0.01	U	0.01	U	0.01	U		0.01	U
	9/5/2012	4.99		1.38						
Iron (mg/L)	9/12/2012	4.67		1.62						
	10/22/2012	4.73		1.96		2.35			0.77	
Iron, Dissolved	9/5/2012	0.275		0.326						
	9/12/2012	0.186		0.177						
(mg/L)	10/22/2012	0.404		0.325		0.115			0.1	U

Table 8. Summary of Groundwater Metals, VOCs, and Dissolved Gases Data for SWMU 211-A

Analyte	Date Collected	MW2	03	MW2	04	<b>MW51</b> 1	L	MW512	MW5	13
Lead (mg/L)	9/5/2012	0.0013	U	0.0013	U					
	9/12/2012	0.0013	U	0.00162						
	10/22/2012	0.0013	U	0.00308		0.00275			0.0013	U
	9/5/2012	0.0013	UB	0.0013	UB					
Lead, Dissolved (mg/L)	9/12/2012	0.0013	UB	0.0013	UB					
(IIIg/L)	10/22/2012	0.0013	U	0.0013	U	0.0013	U		0.0013	U
	9/5/2012	0.168		0.0221						
Manganese (mg/L)	9/12/2012	0.151		0.0357						
	10/22/2012	0.209	Ν	0.0341	Ν	0.204	Ν		0.282	Ν
	9/5/2012	0.162		0.0228						
Manganese, Dissolved (mg/L)	9/12/2012	0.11		0.0175						
Dissolved (IIIg/L)	10/22/2012	0.181	Х	0.0249	Х	0.203	Х		0.248	Х
Volatile Organic Co	ompounds									
	9/5/2012	72	JY	56	DJY					
Trichloroethene	9/12/2012	83		61						
(µg/L)	10/22/2012	110		76		10			220	D
	10/23/2012							34		
	9/5/2012	6.1		15	D					
1,1-Dichloroethene	9/12/2012	6.5		17						
(µg/L)	10/22/2012	6.7		16		5	U		810	D
	10/23/2012							5 U		
	9/5/2012	28		17	D					
<i>cis</i> -1,2-	9/12/2012	29		17						
Dichloroethene (µg/L)	10/22/2012	27		18		2.6			12	D
(µg/L)	10/23/2012							1.2		
	9/5/2012	1	U	2	U					
trans-1,2-	9/12/2012	1	U	1	U					
Dichloroethene (µg/L)	10/22/2012	1	U	1	U	1	U		10	U
(µg/L)	10/23/2012							1 U		
	9/5/2012	2	U	4	U					
Vinyl chloride	9/12/2012	2	U	2	U					
(µg/L)	10/22/2012	2	U	2	U	2	U		20	U
	10/23/2012							2 U		
Biological	I									
Dehaloccoides ethenogenes (cells/mL)	10/22/2012					43	U		17	U
Dissolved Gases										
	9/5/2012	0.097		0.039						
	9/18/2012	0.02	J	0.022	J					
Ethane (µg/L)	10/22/2012	0.0076	J	0.012	J	0.41			0.33	
	10/23/2012							0.03		

# Table 8. Summary of Groundwater Metals, VOCs, and Dissolved Gases Data for SWMU 211-A (Continued)

#### Table 8. Summary of Groundwater Metals, VOCs, and Dissolved Gases Data for SWMU 211-A (Continued)

Analyte	Date Collected	MW203	MW204	MW511	MW512	MW513
	9/5/2012	0.49	0.1			
Ethana (ua/L)	9/18/2012	0.034	0.031			
Ethene (µg/L)	10/22/2012	0.026	0.02 J	0.32		0.12
	10/23/2012				0.01 J	
	9/5/2012	6.8	2.6			
Mathana (ua/L)	9/18/2012	0.31	0.47			
Methane ( $\mu$ g/L)	10/22/2012	0.23	0.16	0.86		1.3
	10/23/2012				0.48	
Inorganic Anions						
	9/5/2012	120	88			
Chloride (mg/L)	9/12/2012	120	87			
	10/22/2012	110	90	3.9		92
	9/5/2012	3.6	5.4			
Nitrate (mg/L)	9/12/2012	3.4	5.1			
	10/22/2012	3.1	5.4	3 U		3 U
	9/5/2012	15	49			
Sulfate (mg/L)	9/12/2012	15	47			
	10/22/2012	17	48	66		22

Notes:

1. B—Applies when the analyte is found in the associated blank.

2. D—Compounds identified in an analysis at a secondary dilution filter.

3. J—Indicates an estimated value.

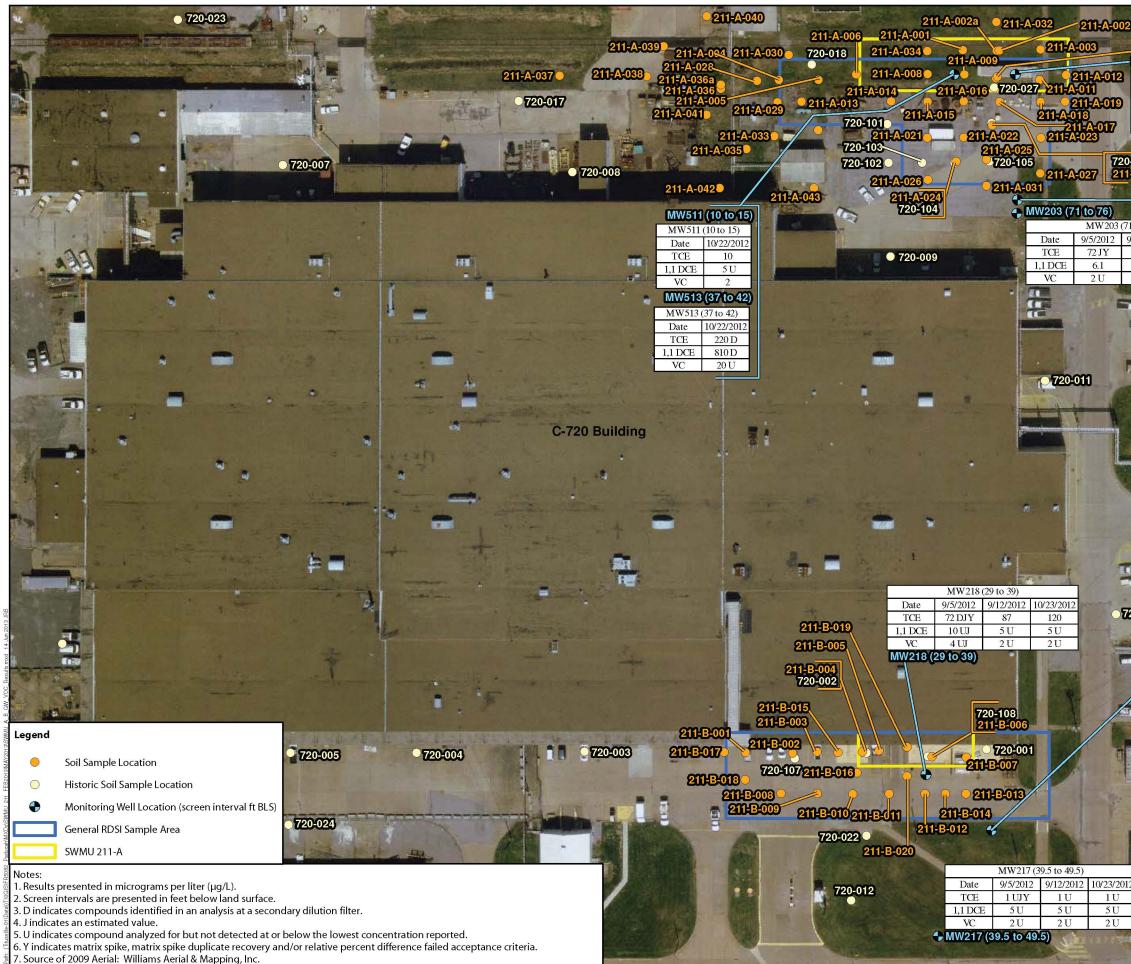
N—Sample spike recovery not within control limits.
 U (inorganics and organics)—Analyte result is less than the reporting limit.

6. X-Other specific flags and footnotes may be required to properly define results. For the dissolved manganese analyses, the serial dilution test difference exceeded the quality control limit of 10%.

7. Y-Matrix spike, matrix spike duplicate and/or relative percent difference failed acceptance criteria.

"---"—signifies sample was not collected. 8.

9. The high reporting limits for MW513 for trans-1,2- DCE and VC are due to a 10× dilution of the sample.



2 211-A-0 211-A-0 211-A-0 - MW512 (18 to 2 MW512 (18 to 2 Date 10/23/ TCE 34 1,1 DCE 51 VC 2 T	28) 2012 U			True North
D-106 1-A-020 71 to 76) 9/12/2012 10/22/20 83 110 6.5 6.7 2 U 2 U	Date         9/5/?           12         TCE         561           1,1 DCE         15           VC         4	204 (49.5 to 54.4) 2012 9/12/2012 10/2 DJY 61 D 17	22/2012 76 16 2 U	
720-010				
	MW514 (8 to 13) MW515 (19 to 29 MW515 (19 to 29)			
20-019	Date         10/23/20           TCE         2 U           1,1 DCE         10 U           VC         4 U           MW516 (35 to 40)           Date         10/22/20           TCE         8.9           1,1 DCE         5 U           VC         2 U			
	Ground	0 0 1-A and SWMU dwater VOC Res h Gaseous Diffusion Kevil, Kentucky	sults	feet
	Geosy com	/ntec isultants May 2013	3	Figure <b>7</b>

## 5.4 SWMU 211-A HU HYDROLOGIC ANALYSIS

Both field and laboratory evaluations were performed to assess the ability of the HU1, HU2, and HU3 formations to accept injectate (Appendix F) and to predict the likely injection pressures and flow rates that may be encountered during field implementation of an injection remedy. Table 9 presents the results of the flexible wall permeameter tests and injection tests. One of the geotechnical laboratory tests estimated hydraulic conductivity by use of a flexible wall permeameter test (ASTM D5084-10) performed at nine locations:

- 211-A-012 (10-12 ft bgs/363.46 to 365.46 ft amsl), 211-A-012 (23-25 ft bgs/350.46 to 352.46 ft amsl), 211-A-012 (38-40 ft bgs/335.46 to 337.46 ft amsl)
- 211-A-027 (10-12 ft bgs/362.62 to 364.62 ft amsl), 211-A-027 (22.5-24.5 ft bgs/350.12 to 352.12 ft amsl), 211-A-027 (38-40 ft bgs/334.62 to 336.62 ft amsl)
- MW513 (10-12 ft bgs/362.02 to 364.02 ft amsl), MW513 (20-21 ft bgs/353.02 to 354.02 ft amsl), MW513 (40-42 ft bgs/332.02 to 334.02 ft amsl)

The calculated average hydraulic conductivity values ranged from 5.5E-10 cm/s to 3.8E-7 cm/s.

Injection test results provided estimates of the likely injection pressures and flow rates during performance of an injection-based remedy. MW511, MW512, and MW513 were tested at pressures of 25, 50, 75, and 100 pounds per square inch (psi) while the flow rate was recorded. The injection flow rates and pressures were used as inputs to calculate hydraulic conductivity by the Jacob-Lohman Method, as provided by the U.S. Geological Survey (USGS 2002). The Jacob-Lohman method calculated hydraulic conductivity values ranged from 4.2E-6 cm/s to 8.8E-5 cm/s. Based upon field observations injection pressures in excess of 50 psi and a flow rate greater than 2 gallons per minute (gpm) are not advisable. Pressures greater than 50 psi tended to raise the immediate groundwater level to the ground surface, signifying that the aquifer is over pressurized and will not provide optimum horizontal distribution within the target HU.

	Permeameter Test Result Summary							
Boring Location	Hydrologic Unit	Sample Depth/Elevation Interval (ft bgs/ft/amsl)	Average Vertical Hydraulic Conductivity (cm/s)					
211-A-012	HU1	10-12/363.46-365.46	1.2E-08					
211-A-012	HU2	23-25/350.46-352.46	3.5E-09					
211-A-012	HU3	38-40/335.46-337.46	3.8E-09					
211-A-027	HU1	10-12/362.62-364.62	2.0E-08					
211-A-027	HU2	22.5-24.5/350.12-352.12	3.9E-09					
211-A-027	HU3	38-40/334.62-336.62	4.8E-09					
MW513	HU1	10-12/362.02-364.02	3.8E-07					
MW513	HU2	20-21/353.02-354,02	5.5E-10					
MW513	HU3	40-42/332,02-334,02	1.8E-07					

Table 9. Summary of Hydrologic	Unit Hydraulic Conductivities for SWMU 211-A
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	Injection Test Result Summary								
Monitoring Well	Hydrologic Unit	Injection Pressure (psi)	Average Flow Rate (gpm)	Calculated Horizontal Hydraulic Conductivity (cm/s)					
MW511	HU1	25	2.3	8.8E-05					
MW511	HU1	50	3.1	4.2E-05					
MW511	HU1	75	3.9	2.6E-05					
MW511	HU1	100	4.8	1.9E-05					
MW512	HU2	25	2.0	2.9E-05					
MW512	HU2	50	3.3	1.5E-05					
MW512	HU2	75	4.1	9.9E-06					
MW512	HU2	100	4.7	7.4E-06					
MW513	HU3	25	0.9	1.3E-05					
MW513	HU3	50	2.0	6.4E-06					
MW513	HU3	75	3.0	4.2E-06					

Table 9. Summary of Hydrologic Unit Hydraulic Conductivities for SWMU 211-A (Continued)

A laboratory evaluation of soil samples was performed to obtain soil grain size distribution (GSD) information (see Appendix F). GSD analyses (ASTM D422) were performed at the following locations:

- 211-A-006 (12-15.5 ft bgs/358.59-362.09 ft amsl), 211-A-006 (21.3-25 ft bgs/349.09-352.79 ft amsl), 211-A-006 (40-42.5 ft bgs/331.59-334.09 ft amsl)
- 211-A-002 (9-13 ft bgs/361.50-365.50 ft amsl), 211-A-002 (23-26 ft bgs/348.50-351.50 ft amsl)), 211-A-002 (37.4-39 ft bgs/335.50-337.10 ft amsl)
- 211-A-012 (12-15 ft bgs/360.46-363.46 ft amsl), 211-A-012 (20-23 ft bgs/352.46-355.46 ft amsl), 211-A-012 (40-42 ft bgs/333,46-335,46 ft amsl)
- 211-A-027 (12-15 ft bgs/359.62-362.62 ft amsl), 211-A-027 (22-25 ft bgs/349.62-352.62 ft amsl), 211-A-027 (35.5-37 ft bgs/337.62-339.12 ft amsl)

Overall, the GSD results indicate that injection technologies would be expected to be successful (though limited in rate/pressure due to grain size) at SWMU 211-A.

## 6. SWMU 211-B RDSI SAMPLE RESULTS

## **6.1 LITHOLOGY**

Soil lithology logs that provide a detailed description of soil type and HU transitions are included in Appendix D. Within the SWMU 211-B investigation area, lithology logs reveal the presence of fill material (gravelly fine sand) to a typical depth of approximately 2 ft, underlain primarily by silt with very fine sand representing HU1 to a typical depth of approximately 20 ft bgs. HU2 was identified from approximately 35 ft bgs and consisted primarily of fine sand and silt with some gravel. HU3 was identified from approximately 35 ft bgs to 60 ft bgs and consisted primarily of silt with fine sand and clay.

#### 6.2 SOIL SAMPLING RESULTS

Nineteen DPT soil boring locations (17 original and 2 contingency) (Figure 5) were performed on the parking lot south of the southeastern portion of the C-720 Building. Collected soil samples were screened approximately every 0.5 ft using a PID to identify intervals of maximum organic vapor response, if present. Soil samples were collected from the 0.5 ft interval of maximum PID reading for each 5-ft soil core and sent by courier to the fixed-base laboratory for overnight VOC analysis. The laboratory preliminary analytical results were available by 8:30 a.m. on Monday for samples collected on the previous Friday and by 8:30 a.m. Tuesday through Friday for samples collected the previous day. The next day laboratory results were used to actively assess whether additional borings were needed based upon a comparison to the RDWP (DOE 2012a) remediation goals. As a result, two contingency borings were completed.

A total of 256 soil samples were collected from 19 soil boring locations. The soil sample VOC results are summarized in Table 10 and presented in Appendix G. Soil sample depths ranged from 0.5 ft bgs (370.07 ft amsl) to 64.9 ft bgs (306.42 ft amsl). The maximum measured TCE result was 13,000  $\mu$ g/kg from location 211-B-019 at a depth of 25.1 ft bgs (346.90 ft amsl). The observed maximum *cis*-1,2-DCE result was 66  $\mu$ g/kg ("J" qualified) collected at soil boring location 211-B-004, at a depth of 14.5 ft bgs (357.44 ft amsl). Soil boring locations 211-B-019 and 211-B-004 are located centrally in the investigation area and within 35 ft of historical location 720-002 (location with greatest TCE concentrations from the Southwest Plume SI). 1,1-DCE, *trans*-1,2-DCE, and VC were not detected in the collected soil samples above laboratory detection limits. At four borings (21%), the borehole average concentration<sup>6</sup> exceeded the remediation goal. A total of 40 soil samples (16%) exceeded the remediation goal. In general, the highest concentrations were noted in the 15 to 30 ft bgs depth range. The area with remediation goal exceedances is immediately adjacent to the southern limit of the eastern portion of the C-720 Building.

Figure 8 illustrates all of the soil TCE analyses for the SWMU 211-B investigation area, overlaid on a map. For reference, soil TCE analyses greater than 75  $\mu$ g/kg (the borehole average project remediation goal) are noted by yellow highlight. As discussed in Section 5.2, Figure 8 shows the lateral extent of 75  $\mu$ g/kg soil TCE (90% confidence limit) and the smaller areas of 75  $\mu$ g/kg soil TCE (50% confidence limit) and 1,000  $\mu$ g/kg soil TCE (90% confidence limit) for comparison.

<sup>&</sup>lt;sup>6</sup> The average contaminant concentration for a borehole was calculated using one half of the laboratory reporting limit for nondetect analyses and using the greater concentration where analyses of duplicate samples were available.

Station	Date Collected	TCE [µg/kg]	1,1-DCE [µg/kg]	<i>cis-</i> 1,2- DCE [µg/kg]	trans-1,2- DCE [μg/kg]	VC [µg/kg]
Groundwater Protection Remediation Goal		75	137	619	5290	570
211-B-001	10/9/2012	197	***	1	***	***
211-B-002	10/10/2012	43*	***	***	***	***
211-B-003	10/10/2012	10	***	***	***	***
211-B-004	10/11/2012	418	***	10	***	***
211-B-005	10/15/2012	863	***	6	***	***
211-B-006	10/15/2012	15*	***	***	***	***
211-B-007	10/16/2012	4	***	***	***	***
211-B-008	10/9/2012	0.6	***	***	***	***
211-B-009	10/8/2012	2	***	0.3	***	***
211-B-010	10/5/2012	3	***	0.3	***	***
211-B-011	10/8/2012	5	***	***	***	***
211-B-012	10/4/2012	1.0	***	***	***	***
211-B-013	10/4/2012	0.3	***	***	***	***
211-B-015	10/16/2012	39*	***	2	***	***
211-B-016	10/17/2012	15	***	0.4	***	***
211-B-017	10/17/2012	25*	***	0.6	***	***
211-B-018	10/18/2012	4	***	***	***	***
211-B-019	10/18/2012	1,178	***	4	***	***
211-B-020	10/19/2012	11	***	***	***	***

Table 10. Soils VOC Data (Average Borehole Concentration) for SWMU 211-B

Notes:

4. For "U" qualified analyses, a value of one half the concentration reported was used in calculating the average borehole concentration.

5. Yellow shading and bold text indicate an exceedance of Groundwater Protection Remediation Goals.

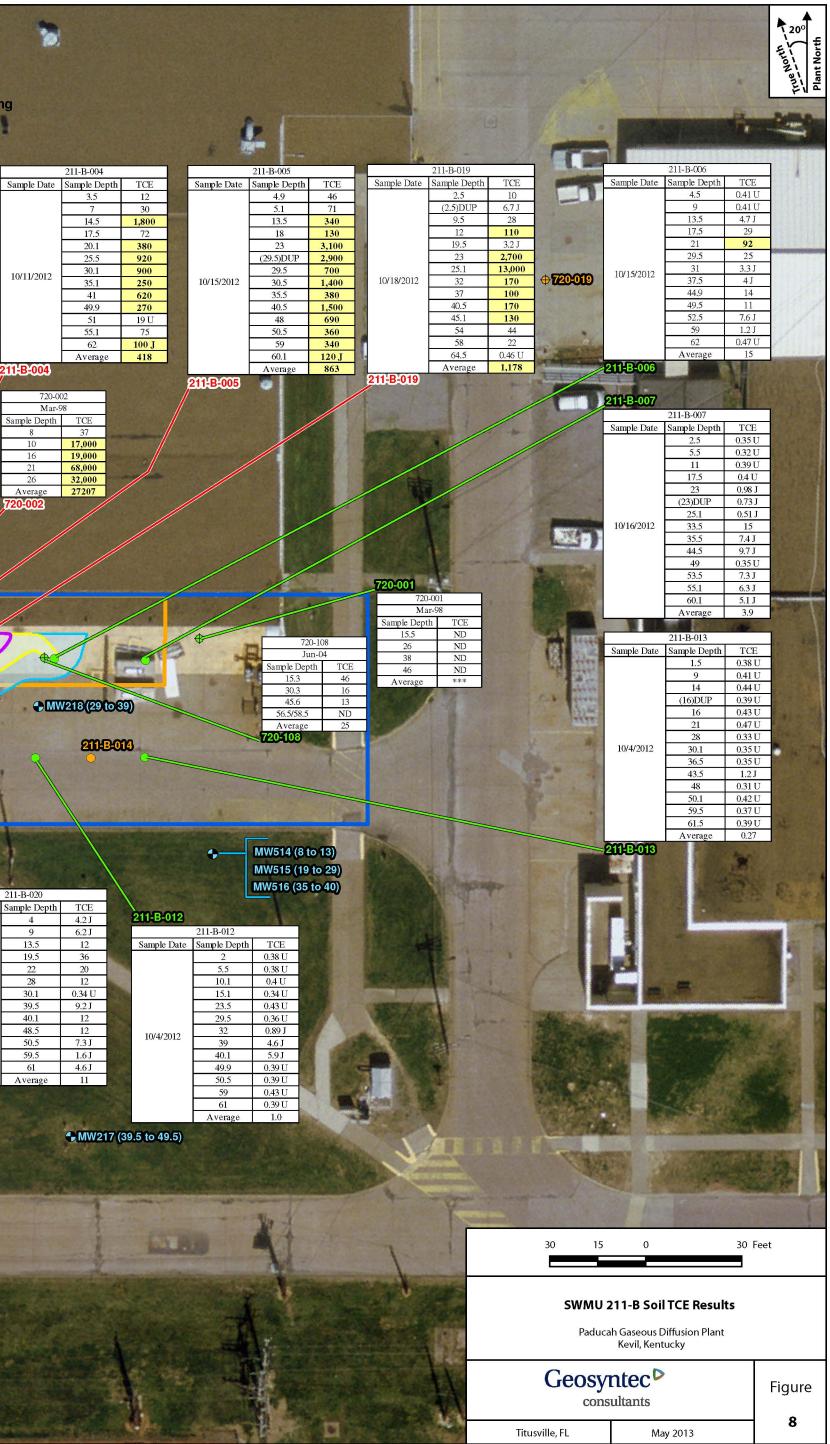
6. Soil boring 211-B-014 was collected and archived. Boring was not logged or screened for VOC impacts.

<sup>1.</sup> Groundwater Protection Remediation Goals from *Remedial Design Work Plan for Solid Waste Management Units 1, 211-A, and 211-B Volatile Organic Compound Sources for the Southwest Groundwater Plume at the Paducah Gaseous Diffusion Plant, Paducah, Kentucky* (DOE 2012a).

<sup>2. \*—</sup>Indicates average concentrations that are below the Groundwater Protection Remediation Goal, but at least one sample exceeded the remediation goal.

<sup>3. \*\*\*-</sup>Indicates average concentration not calculated as all boring analyses were "U" qualified (compound analyzed for but not detected at or below the lowest concentration reported) for specific VOC.

11-B-02       11-B-02	211-B-003           Sample Date         Sample Depth         TCE           4         0.41 U         9         0.41 U           9         0.41 U         14.5         1 J           19.5         0.46 J         (19.5)DUP         0.5 J           23         0.35 U         23         0.35 U           10/10/2012         34         0.87 J         39         17	211-B-015         Sample Date       Sample Depth       TCE         3       1.6 J         5.1       2.2 J         13.5       4.9 J         19.9       1 J         21.5       170         29.5       120         30.5       5.4 J         37       5.5 J         41.5       37         48.5       17         52       39         56       42         60.5       67         Average       39	C-720 Building         11-B-016         Sample Date       Sample Depth       TCE         1       043 U         14       7.7 J         (16)DUP       033 U         10/17/2012       33.5       16         36.5       18         43.5       23         36.5       18         43.5       23         50.1       42         50.1       43.3         20.5       16         36.5       18         43.5       23         48.5       31         50.1       42         50.1       43.3         20.5       16         36.5       18         43.5       21         50.1       43.3         20.1       43.3         30.1       42         50.1       23.5         50.1       43.3         48.5       31         50.1       43.3         50.1       43.3         50.1       43.3         51.5       20         51.1       51.5         52.1       51.5         53.1
Sample Date	CE 2 U 7 U 9 U 8 U 5 U 2 J 6 U 1 U 9 U 8 U 5 Sample Date 8 Sample Det 1 4 4 1 U 3 U 3 U 3 U 3 U 3 U 3 U 3 U 3	3J           3.5J           10           8.4J           0.38 U	720-022 •       211-B:020         1       211         1       3mple Date       3mple
Legend         ● Soil Boring Location with Average Soil Concentration Exceeding TCE Remediation Goal         ● Soil boring location with Average Soil Concentration Less than TCE Remediation Goal         ● Archive Core Soil Boring Location - Not Sampled         ● Historic Soil Boring Location with Average Soil Concentration Exceeding TCE Remediation Goal         ● Historic Soil Boring Location with Average Soil Concentration Exceeding TCE Remediation Goal         ● Historic Soil Boring Location with Average Soil Concentration Less than TCE Remediation Goal         ● Historic Soil Boring Location with Average Soil Concentration Less than TCE Remediation Goal         ● Historic Soil Boring Location with Average Soil Concentration Less than TCE Remediation Goal         ● Historic Archive Core Soil Boring Location - Not Sampled         ● Monitoring Well Location (screen interval ft BLS)         ▲ Area defined by 90% Confidence Level TCE Concentrations greater than 1,000 µg/kg         ▲ Area defined by 90% Confidence Level TCE Concentrations greater than 75 µg/kg         ● Groundwater Protection Remediation Goals         ● WUU 211-8         Notes:         1. Results are presented in microgram per kilogram (µg/kg).         2. Sample depth is presented in feet below land surface (ft BLS).         3. DUP indicates an estimated value.         4. J indicates an estimated value.         5. Undicates compound analyzed for but not detected at or below the lowest concentration reporte		0.4 U 0.35 U 0.41 U 0.41 U 0.39 U 0.41 U 0.41 U 0.41 U 77	20-012 <b>*</b> 211-B-011 Sample Date Sample Depth TCE 4 0.41 U 9 4.3 J 14.5 15 19.5 12 20.5 15 (20.5)DUP 5.8 J 29.5 1.6 J 39 0.84 J 44 1.5 J 45.1 2.4 J 51 2.2 J 39 0.84 J 44 1.5 J 45.1 2.4 J 51 2.3 J 59 0.39 U 64.9 2.3 J A verage 4.5



TOC results for SWMU 211-B ranged from lower than the reporting limit of 33 mg/kg to 670 mg/kg with an average concentration of 500 mg/kg. TOC sample results are presented in Table 11.

Station	Date Collected	Sample Top Depth/Elevation [ft bgs/ft amsl]	Sample Bottom Depth/Elevation [ft bgs/ft amsl]	Hydrogeologic Unit	TOC [mg/kg]
		9.5/362.42	9.5/362.42	HU1	430
211-B-001	10/9/2012	18.5/353.42	18.5/353.42	HU2	460
		39/332.92	39/332.92	HU3	380
		5.5/366.44	5.5/366.44	HU1	620
211-B-004	10/11/2012	22.3/349.64	22.3/349.64	HU2	33 U
		38/333.94	38/333.94	HU3	450
		9/363.03	9/363.03	HU1	670
211-B-007	10/16/2012	27.5/344.53	27.5/344.53	HU2	240
		43/329.03	43/329.03	HU3	750

Table 11. Summary of Soils TOC Data for SWMU 211-B

#### 6.3 GROUNDWATER SAMPLE RESULTS

As at SWMU 211-A, RGA groundwater flows to the north and northeast in the area of SWMU 211-B. Because of the proximity of the Porters Creek Clay Terrace, there are no RGA MWs present in the vicinity of SWMU 211-B to characterize groundwater quality. The prevailing hydraulic gradient in the UCRS is vertically downward and groundwater flows downward to recharge the RGA. UCRS wells MW217 (distal), screened from 40 to 50 ft bgs/325.96 to 335.96 ft amsl, and MW218 (proximal), with screen at 29 to 39 ft bgs/333.30 to 343.30 ft amsl, are located 130 ft and 8 ft south (upgradient) of SWMU 211-B, respectively, and provide ambient groundwater quality characterization for the investigation. UCRS wells MW514 (screened 8 to 13 ft bgs/359.73 to 364.73 ft amsl), MW515 (screened 19 to 29 ft bgs/343.75 to 353.75 ft amsl), and MW516 (screened 35 to 40 ft bgs/332.77 to 337.77 ft amsl) were installed southeast (upgradient) of the area of VOC contamination as part of the RDSI to provide further characterization for SWMU 211-B. (Continued use of the SWMU 211-B area precluded installation of MWs in the VOC contaminated area.) There are no UCRS or RGA downgradient monitoring wells for SWMU 211-B.

Groundwater samples were collected during September and October 2012 from UCRS MWs MW217, MW218, MW515, and MW516. MW514 (shallowest UCRS well) had insufficient water to support groundwater sampling. The groundwater samples were collected and analyzed for VOCs, alkalinity, total and dissolved metals, ferrous iron, major anions, and dissolved gasses. Additionally, samples from MW515 and MW516 were analyzed for *Dhc*. Groundwater sample results are presented in Table 12. Comparisons of the highest levels detected in the wells installed during the RDSI and the levels observed in pre-existing wells MW217 and MW218 follow.

**VOCs.** In the RDSI wells installed for SWMU 211-B, the only detection of a VOC was in the deepest well, MW516.

	SWMU 211-B RDSI Well	South of SWMU 211-B		
	MW516 (deep UCRS well)	MW217 max value (distal UCRS well)	MW218 max value (proximal UCRS well)	
Trichloroethene (µg/L)	8.9	< 1	120	
cis-1,2-DCE (µg/L)	< 1	< 1	2.2	

1,1-DCE; *trans*-1,2-DCE; and VC were not detected above individual laboratory detection limits in any of the SWMU 211-B groundwater samples. The presence of *cis*-1,2-DCE suggests that biologically mediated reductive dechlorination is occurring in the groundwater at SWMU 211-B. Groundwater VOC sample results are displayed in Figure 7.

**Dissolved Gases.** Among the wells installed during the RDSI at SWMU 211-B, all three dissolved gasses—ethane, ethene, and methane—are highest in the shallower well with water.

	SWMU 211-B RDSI Well	-B RDSI Well South of SWMU 211-B		
	MW515	MW217 max value	MW218 max value	
	(shallower UCRS well)	(distal UCRS well)	(proximal UCRS well)	
Ethane (µg/L)	25	0.11	0.18	
Ethene ( $\mu g/L$ )	7.9	0.14	0.24	
Methane ( $\mu$ g/L)	35	6.5	2.4	

Methane is produced by methanogenic bacteria conversion of acetate or reduction of carbon dioxide under anaerobic conditions. Methanogens and dechlorinating organisms thrive under similar conditions; therefore, the production of methane in groundwater is an indicator that conditions exist that are suitable for reductive dechlorination. Ethene is the final dechlorination product of TCE, while ethane is the product of ethene reduction. The presence of ethene/ethane provides a direct line of evidence that reductive dechlorination is proceeding to completion.

**Inorganic Anions.** Within the SWMU 211-B RDSI UCRS wells, chloride and nitrate levels were measured at highest concentration in the deepest well, MW516, and the highest sulfate concentration was measured in the shallower well, MW515.

	SWMU 211-B	<b>RDSI Wells</b>	South of SWMU 211-B		
	MW515 MW516		MW217 max value	MW218 max value	
	(shallower UCRS well)	(deepest UCRS well)	(distal UCRS well)	(proximal UCRS well)	
Chloride (mg/L)	160	300	160	340	
Nitrate (mg/L)	< 3	3	< 3	< 3	
Sulfate (mg/L)	22	6.4	39	40	

The nitrate and sulfate (electron acceptors) concentrations present are not at levels that would be anticipated to hinder the reductive dechlorination pathway. Additionally, sulfate is not present at an elevated concentration that has the potential to result in sulfide concentrations that are toxic to dechlorinating microorganisms.

**Metals.** Among the UCRS SWMU 211-B RDSI wells, the highest measured levels of metals, with the exception of chromium, were found in samples from the shallower UCRS well, MW515.

	SWMU 211-B	<b>RDSI</b> Wells	South of SWMU 211-B		
	MW515 MW516		MW217 max value	MW218 max value	
	(shallower UCRS well)	(deepest UCRS well)	(distal UCRS well)	(proximal UCRS well)	
Aluminum (mg/I)	8.49	0.202	0.647	4.61	
Aluminum (mg/L)	("N" qualified)	("N" qualified)	0.047	("N" qualified)	
Chromium (mg/L)	0.0137	0.131	< 0.01	< 0.01	
Iron (mg/L)	9.79	0.605	0.354	0.515	
Lead (mg/L)	0.0106	< 0.0013	0.00262	0.00241	
Manganasa	0.32	0.108	1.43	0.0356	
Manganese	("N" qualified)	("N" qualified)	1.45	("N" qualified)	

**Biological.** *Dhc* was not measured at a concentration greater than the reporting limits of 35 cells/mL for MW515 and 25 cells/mL in MW516. The absence of detectable *Dhc* suggests that reductive dechlorination is not occurring at a high rate under current conditions.

Analyte	Date Collected	MW2	17	MW2	18	MW515	i	MW516	•
Total and Dissolve	ed Metals			•					
	9/5/2012	0.647		4.48					
Aluminum	9/12/2012	0.2	U	2.46					
(mg/L)	10/22/2012							0.202	Ν
	10/23/2012	0.237	Ν	4.61	Ν	8.49	Ν		
	9/5/2012	0.2	U	0.2	U				
Aluminum,	9/12/2012	0.2	U	0.2	U				
Dissolved (mg/L)	10/22/2012							0.2	U
	10/23/2012	0.2	U	0.2	U	0.281			
	9/5/2012	0.01	U	0.01	U				
Chromium	9/12/2012	0.01	U	0.01	U				
(mg/L)	10/22/2012							0.131	
	10/23/2012	0.01	U	0.01	U	0.0137			
	9/5/2012	0.01	U	0.01	U				
Chromium,	9/12/2012	0.01	U	0.01	U				
Dissolved (mg/L)	10/22/2012							0.01	U
	10/23/2012	0.01	U	0.01	U	0.01	U		
	9/5/2012	0.354		0.437					
	9/12/2012	0.1	U	0.462					
Iron (mg/L)	10/22/2012							0.605	
	10/23/2012	0.153		0.515		9.79			
	9/5/2012	0.1	U	0.1	U				
Iron, Dissolved	9/12/2012	0.1	U	0.1	U				
(mg/L)	10/22/2012							0.1	U
	10/23/2012	0.1	U	0.1	U	0.139			
	9/5/2012	0.00262		0.00241					
Land (ma/L)	9/12/2012	0.0013	U	0.00213					
Lead (mg/L)	10/22/2012							0.0013	U
	10/23/2012	0.0013	U	0.00233		0.0106			
	9/5/2012	0.0013	UB	0.0013	UB				
Lead, Dissolved	9/12/2012	0.0013	UB	0.0013	UB				
(mg/L)	10/22/2012							0.0013	U
	10/23/2012	0.0013	U	0.0013	U	0.0013	U		

 Table 12. Summary of Groundwater Metals, VOCs, and Dissolved Gases Data for SWMU 211-B

Analyte	Date Collected	MW2	17	MW2	218	MW515		MW516	
Volatile Organic	Compounds								
	9/5/2012	1.43		0.0204					
Manganese	9/12/2012	0.806		0.0167					
(mg/L)	10/22/2012							0.108	Ν
	10/23/2012	0.826	Ν	0.0356	Ν	0.32	Ν		
	9/5/2012	0.404		0.005	U				
Manganese,	9/12/2012	0.605		0.005	U				
Dissolved (mg/L)	10/22/2012							0.127	Х
_	10/23/2012	0.746	Х	0.00664	Х	0.17	Х		
	9/5/2012	1	UJY	72	DJY				
Trichloroethene	9/12/2012	1	U	87					
(µg/L)	10/22/2012							8.9	
	10/23/2012	1	U	120		2	U		
	9/5/2012	5	U	10	UJ				
1,1-	9/12/2012	5	U	5	U				
Dichloroethene	10/22/2012							5	U
(µg/L)	10/23/2012	5	U	5	U	10	U		_
	9/5/2012	1	U	2.1	DJ		-		
<i>cis</i> -1,2-	9/12/2012	1	U	2.2					
Dichloroethene	10/22/2012		-					1	U
(µg/L)	10/23/2012	1	U	2.1		2	U		-
	9/5/2012	1	U	2	UJ		-		
trans-1,2-	9/12/2012	1	U	1	U				
Dichloroethene	10/22/2012		-		-			1	U
(µg/L)	10/23/2012	1	U	1	U	2	U		-
	9/5/2012	2	U	4	UJ		-		
Vinyl chloride	9/12/2012	2	U	2	U				
(µg/L)	10/22/2012		-		-			2	U
	10/23/2012	2	U	2	U	4	U		0
Biological	10/20/2012					•	0		
Dehaloccoides	10/22/2012							25	U
enthenogenes									-
(cells/mL)	10/23/2012					35	U		
Dissolved Gases				1					
	9/5/2012	0.11		0.18					
	9/18/2012	0.024	J	0.013	J				
Ethane ( $\mu g/L$ )	10/22/2012							0.013	J
	10/23/2012	0.015	J	0.025	U	25			
	9/5/2012	0.14		0.24					
	9/18/2012	0.039		0.021	J				
Ethene (µg/L)	10/22/2012							0.023	J
	10/23/2012	0.0093	J	0.027		7.9			-
	10/20/2012	0.0075		0.027					

# Table 12. Summary of Groundwater Metals, VOCs, and Dissolved Gases Data for SWMU 211-B (Continued)

Analyte	Date Collected	MW217	7	MW2	18	MW515		MW516
<b>Inorganic Anions</b>								
	9/5/2012	6.5		2.4				
Methane (µg/L)	9/18/2012	0.75		0.18				
Methane (µg/L)	10/22/2012							0.52
	10/23/2012	0.52		0.056	J	35		
	9/5/2012	160		340				
Chloride (mg/L)	9/12/2012	160		330				
Chioride (hig/L)	10/22/2012							300
	10/23/2012	150		340		160		
	9/5/2012	3	U	3	U			
Nitrate (mg/L)	9/12/2012	3	U	3	U			
Nitrate (IIIg/L)	10/22/2012							3
	10/23/2012	3	U	3	U	3	U	
Sulfate (mg/L)	9/5/2012	5.6		39				
	9/12/2012	4.8		39				
	10/22/2012							6.4
	10/23/2012	39		40		22		

Table 12. Summary of Groundwater Metals, VOCs, and Dissolved Gases Data for SWMU 211-B (Continued)

Notes:

1. B—Applies when the analyte is found in the associated blank.

2. D-Compounds identified in an analysis at a secondary dilution filter.

J—Indicates an estimated value.
 N—Sample spike recovery not within control limits.

5. U (inorganics and organics)—Analyte result is less than the reporting limit.

6. X—Other specific flags and footnotes may be required to properly define results. For the dissolved manganese analyses, the serial dilution test difference exceeded the quality control limit of 10%.

7. Y-Matrix spike, matrix spike duplicate and/or relative percent difference failed acceptance criteria.

8. "---"—signifies sample was not collected.

## 6.4 SWMU 211-B HU HYDROLOGIC ANALYSIS

Both field and laboratory evaluations were performed to assess the ability of the HU1, HU2, and HU3 formations to accept injectate (Appendix F) and to predict the likely injection pressures and flow rates that may be encountered during field implementation of an injection remedy. Table 13 presents the results of the flexible wall permeameter tests and injection tests. One of the geotechnical laboratory tests estimated hydraulic conductivity by use of a flexible wall permeameter test (ASTM D5084) performed at nine locations:

- 211-B-001 (5-7 ft bgs/364.92-366.92 ft amsl), 211-B-001 (15-17 ft bgs/354.92-356.92 ft amsl), 211-B-001 (32-37 ft bgs/334.92-339.92 ft amsl)
- 211-B-004 (8-10 ft bgs/361.94-363.94 ft amsl), 211-B-004 (18-20 ft bgs/351.94-353.94 ft amsl), 211-B-004 (38-40 ft bgs/331.94-333.,94 ft amsl)
- MW516 (10-12 ft bgs/360.77-362.77 ft amsl), MW516 (25-26 ft bgs/346.77-347.77 ft amsl), MW516 • (40-42 ft bgs/330.77-332.77 ft amsl)

The calculated average hydraulic conductivity values ranged from 1.6E-9 cm/s to 3.3E-6 cm/s.

Injection test results provided estimates of the likely injection pressures and flow rates during performance of an injection-based remedy. MWs MW514, MW515, and MW516 were tested at pressures

of 25, 50, 75, and 100 psi and the flow rate was recorded. The injection flow rates and pressures were used as inputs for hydraulic conductivity calculation by the Jacob-Lohman Method, provided by the U.S. Geological Survey (USGS 2002). The Jacob-Lohman method calculated hydraulic conductivity values ranged from 8.8E-6 cm/s to 1.3E-4 cm/s. A viable injection pressure was not determined conclusively based on the tests conducted at these locations. The groundwater elevation increased on multiple instances during injection testing; however, the water level elevation decreased significantly after completion of the test and prior to the start of the next test. Based on this observation, it is suspected that the bentonite seal between the nested well screens did not provide an effective seal resulting in a preferential path for pressure stress, artificially increasing groundwater levels during testing. If required, future injection by DPT tends to create a better seal with the borehole, decreasing the chance of injection fluid making its way to the ground surface. Using the direct push injection method and the injection test data, a flow rate of approximately 2.4 gpm at a pressure of 50 psi should provide effective distribution of injectate among the HU1, HU2, and HU3 formations at SWMU 211-B.

A laboratory evaluation of soil samples was performed to obtain soil GSD information (see Appendix F). GSD analyses (ASTM D422) were performed at the following locations:

- 211-B-007 (8-12 ft bgs/360.03-364.03 ft amsl), 211-B-007 (27.5-31.5 ft bgs/340.53-344.53 ft amsl), 211-B-007 (42.5-44 ft bgs/328.03-329.53 ft amsl)
- 211-B-004 (5-7.5 ft bgs/364.44-366.94 ft amsl), 211-B-004 (21.1-23.5 ft bgs/348.44-350.84 ft amsl), 211-B-004 (36-38 ft bgs/333.94-335.94 ft amsl)
- 211-B-001 (8-10 ft bgs/361.92-363.92 ft amsl), 211-B-001 (18-20 ft bgs/351.92-353.92 ft amsl), 211-B-001 (38-40 ft bgs/331.92-333.92 ft amsl)

Overall, the GSD results indicate that injection technologies would be expected to be successful (though rate/pressure limited due to grain size) at SWMU 211-B.

Permeameter Test Result Summary									
Boring Location	Hydrologic Unit	Sample Depth/Elevation Interval (ft bgs/ft amsl)	Average Vertical Hydraulic Conductivity (cm/s)						
211-B-001	HU1	5-7/364.92-366.92	3.8E-08						
211-B-001	HU2	15-17/354.92-356.92	3.3E-06						
211-B-001	HU3	32-37/334.92-339.92	1.9E-09						
211-B-004	HU1	8-10/361.94-363.94	4.8E-07						
211-B-004	HU2	18-20/351.94-353.94	1.6E-09						
211-B-004	HU3	38-40331.94-333.94	2.5E-09						
MW516	HU1	10-12/360.77-362.77	9.2E-07						
MW516	HU2	25-26/346,77-347.77	4.6E-08						
MW516	HU3	40-42/330.77-332,77	1.1E-07						

Table 13. Summary of Hydrologic Unit Hydraulic Conductivities for SWMU 211-B

Injection Test Result Summary									
Monitoring Well	Hydrologic Unit	Injection Pressure (psi)	Average Flow Rate (gpm)	Calculated Horizontal Hydraulic Conductivity (cm/s)					
MW514	HU1	25	2.3	1.3E-04					
MW514	HU1	50	2.4	6.7E-05					
MW514	HU1	75	3.1	4.2E-05					
MW514	HU1	100	3.4	3.3E-05					
MW515	HU2	25	1.9	3.9E-05					
MW515	HU2	50	2.8	1.8E-05					
MW515	HU2	75	3.7	1.2E-05					
MW515	HU2	100	4.5	8.8E-06					
MW516	HU3	25	1.9	4.6E-05					
MW516	HU3	50	3.1	2.4E-05					
MW516	HU3	75	3.3	1.6E-05					
MW516	HU3	100	4.2	1.2E-05					

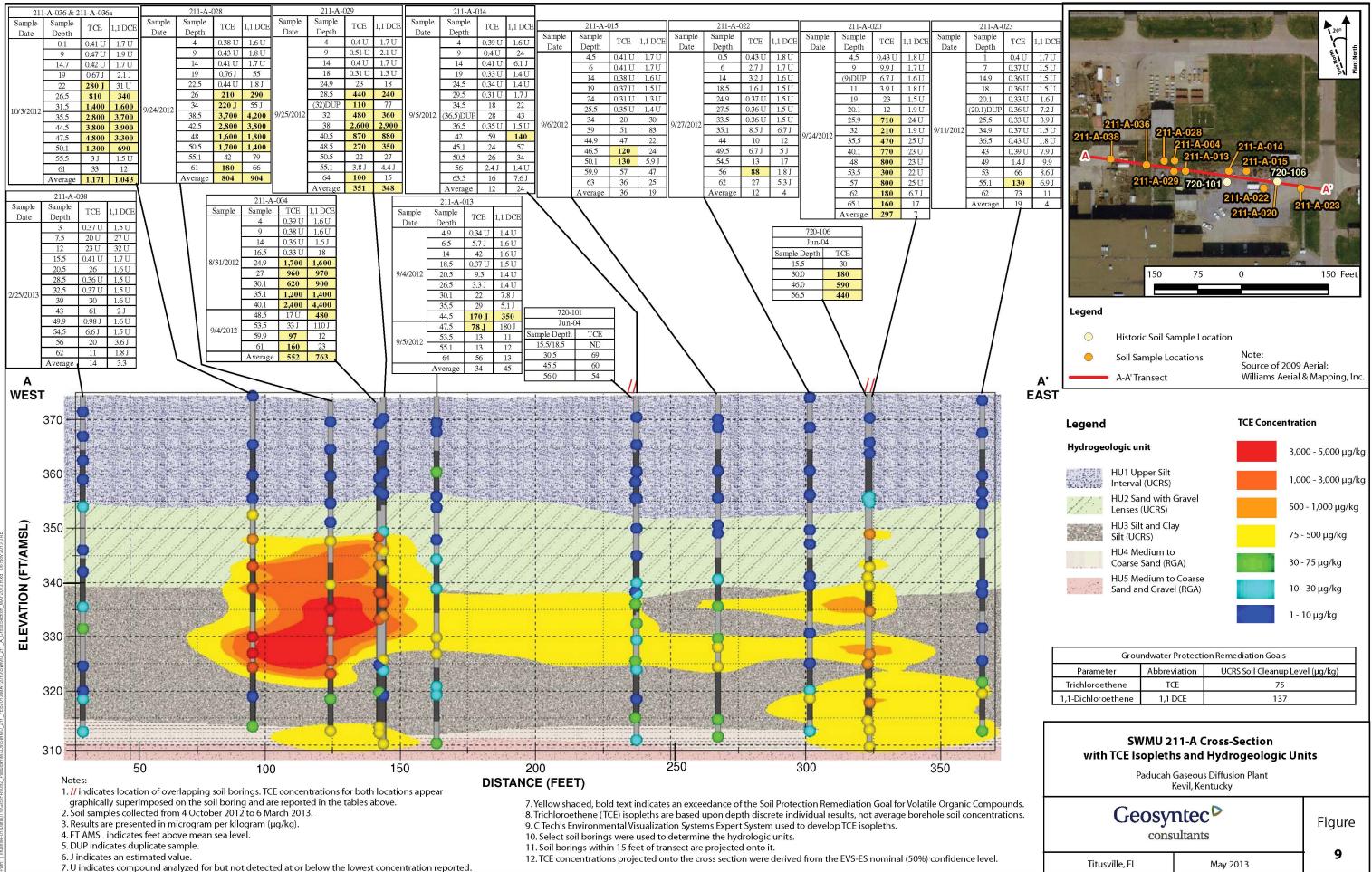
# 7. SWMU 211-A DATA EVALUATION AND ASSESSMENT

Data collected during the RDSI further delineated the magnitude and areal and vertical extents of TCE and other VOC contamination in SWMU 211-A within the Southwest Plume source areas. The results of the RDSI and previous investigations of the SWMU 211-A area indicate that soils containing VOC contamination are located within the subsurface north of the northeast corner of the C-720 Building Area. The highest level of TCE (4,800 µg/kg) detected during the RDSI was at a depth of 47.5 ft bgs/326.97 ft amsl (211-A-036), with low-levels of cis-1,2-DCE (77 µg/kg) and 1,1-DCE (3,300 µg/kg) also detected. Sample location 211-A-036 is located approximately 240 ft north by northwest of the previous investigation maximum concentration (8,100 µg/kg TCE at 30 ft depth/344.39 ft amsl elevation in location 720-027 from the WAG 27 RI). RDSI soil locations from this investigation in close proximity to historical soil sample location 720-027 are 211-A-010 and 211-A-017, with 211-A-017 having the greatest TCE concentration of 1,600 µg/kg at 30.1 ft bgs/344.79 ft amsl. Among the Southwest Plume SI borings in the SWMU 211-A area, TCE levels were highest in location 720-105 (980 µg/kg at 46 ft depth/approximately 328.2 ft amsl) (DOE 2007). Overall results from the soil samples indicate that dehalogenation (i.e., degradation of parent VOCs to daughter products such as TCE degrading to cis-1,2-DCE and VC) is occurring. Of the 542 soil samples collected for VOC analysis during the RDSI, 316 samples have a TCE detection, 196 samples have a 1,1-DCE detection, 189 samples have a *cis*-1,2-DCE detection, no samples have a trans-1,2-DCE detection, and 23 samples have a VC detection. Groundwater analysis results also support that TCE degradation is occurring.

Results of the UCD soil samples from the RDSI and historical data were used to create a three-dimensional contamination model using the software Environmental Visualization Systems Expert System (EVS-ES). A five-layer geologic model was used for modeling soil contamination. Analytical results from this investigation and all historical soil TCE data for the SWMU 211-A investigation area in the OREIS, shown in Figure 6, were log processed in the model. The Horizontal/Vertical Anisotropy Ratio parameter, which allows the model to take into consideration expected differences in fluid flow through the soil matrix, was set to a value of 1.5. The Octant Search method was used to determine which sample points are selected for inclusion in the kriging matrix. This method sets a maximum number of points for each octant, which helps offset bias effects of sampling distribution irregularities. The model used a soil density of 1.4 g/cc and a chemical density of 1.46 g/cc. The SWMU 211-A soil impacted greater than 75  $\mu$ g/kg of TCE based upon a 90% confidence level that is estimated to have an areal extent of 34,000 ft<sup>2</sup>. The mass of TCE in the SWMU 211-A soil impacted greater than 75  $\mu$ g/kg is estimated to be 2.2 gal (12 kg). Figure 6 also shows the smaller areas of 75  $\mu$ g/kg soil TCE (50% confidence limit) and 1,000  $\mu$ g/kg soil TCE (90% confidence limit) for comparison. These extents define distinct east and west areas of TCE contamination.

Figure 9<sup>7</sup> shows a cross-section through the locations of the greatest magnitude concentrations. The TCE isopleths depicted in Figure 9 show a predominance of TCE impacts in the western portion of the cross-section in the 25 to 50 ft bgs depth interval. A sensitivity analysis was performed. The sensitivity analysis utilized a range of values to evaluate the area of VOC impacts and volume present. The volume/mass estimates range from 0.2 gal/1 kg to 2.2 gal/12 kg for a range of 10% to 90% confidence level with a volume/mass of 0.7 gal/4 kg for the 50% confidence level. A CD containing viewable three-dimensional model EVS-ES files and supporting calculations and technical details are included in Appendices B and C.

<sup>&</sup>lt;sup>7</sup> Figure 9 is a cross section taken from a three-dimensional model of TCE sample results. Where samples were not collected for laboratory analyses from the bottom depth of a soil boring (samples were collected at discrete intervals targeted by field measurements over each 5-ft interval), the bottom depths depicted on Figure 9 do not represent the total depth of the soil boring.



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There are two areas with soil remediation goal exceedances that are defined by the areal distribution of soil boring locations with depth-average TCE concentration greater than 75  $\mu$ g/kg. Although there are 1,1-DCE exceedances, their location is less extensive and coincides with TCE exceedances. The western area (defined by borings 211-A-004, 211-A-005, 211-A-028, 211-A-029, 211-A-033, 211-A-035, and 211-A-036) covers approximately 15,900 ft<sup>2</sup> (based upon 50% nominal 75  $\mu$ g/kg isocontour) laterally with a depth interval of 6 ft bgs to 64 ft bgs. The eastern area (defined by borings 211-A-002, 211-A-010, 211-A-017, 211-A-020, and 211-A-025) covers approximately 15,000 ft<sup>2</sup> (based upon 50% nominal 75  $\mu$ g/kg isocontour) laterally with a depth interval from 6.5 ft bgs to 65.1 ft bgs.

Overall, FCR findings tend to be consistent with the current CSM regarding the depth and magnitude of VOC soil contamination; however, the horizontal location of the greatest TCE soil impact (potential source area) does not align with previous SI findings. The current CSM assumes the TCE source area is located near soil sample location 720-027 (DOE 1999) (see Figure 4). During performance of the RDSI, the greatest magnitude TCE concentration was located at soil sample location 211-A-036, which indicates that an additional TCE source also is located west of soil sample location 720-027. A number of depth-averaged TCE concentration soil boring locations lower than 75  $\mu$ g/kg were installed between historical location 720-027 and 211-A-036 indicating separate source areas. The information presented in this FCR indicates that the area of TCE source-based mass for the 211-A site is larger than previously assumed.

# 8. SWMU 211-B DATA EVALUATION AND ASSESSMENT

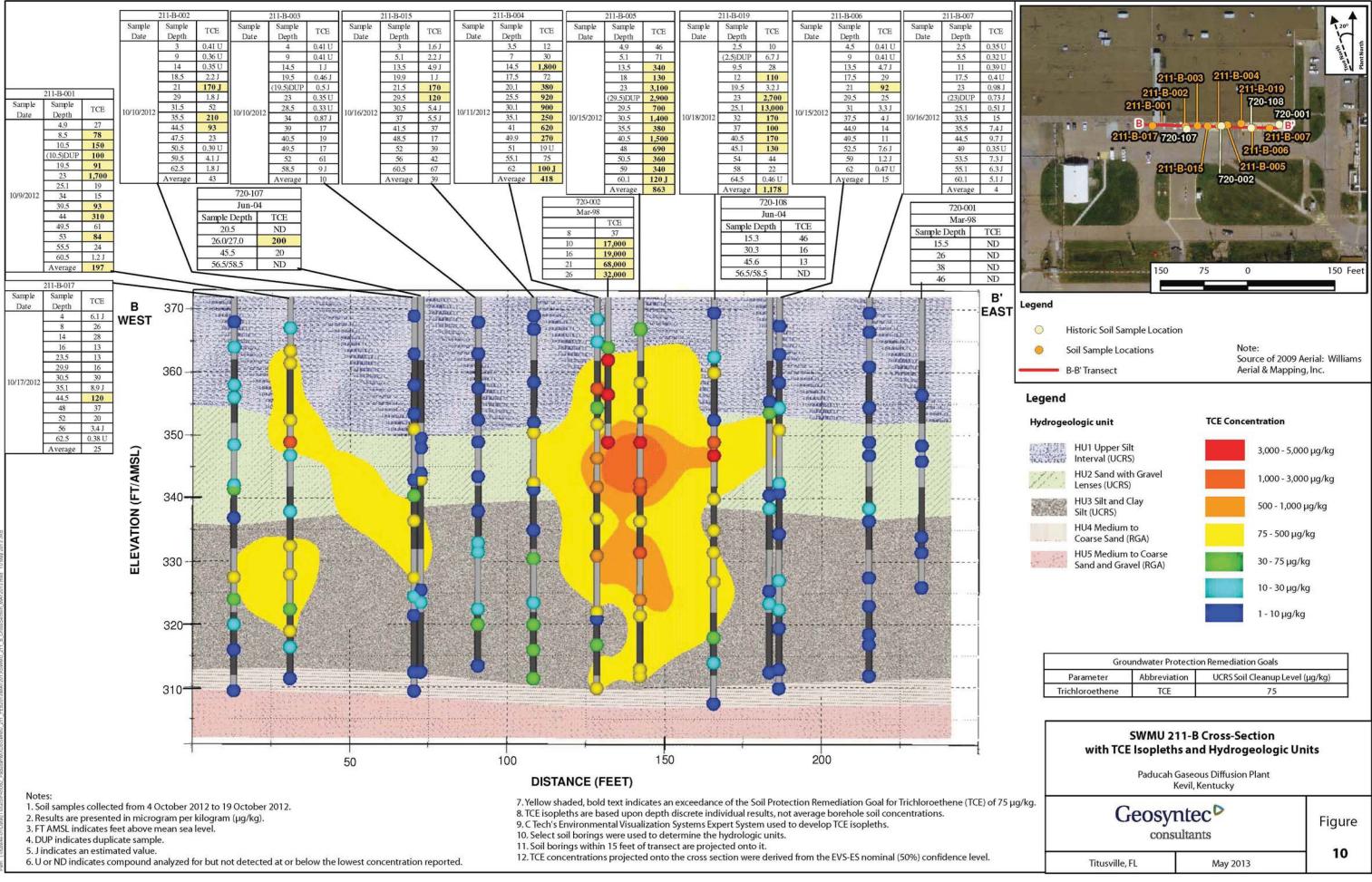
RDSI results and those of previous investigations of the SWMU 211-B area indicate that soils containing low-levels of VOC contamination are present in the subsurface at the southeast corner of the C-720 Building Area (Figure 8). The greatest TCE soil concentration (13,000  $\mu$ g/kg) detected during this investigation was at 25.1 ft bgs/346.90 ft amsl (211-B-019), which is approximately 10 ft west of the previous investigation maximum concentration (68,000  $\mu$ g/kg) location (720-002 at 20 ft depth/351.80 ft amsl). Another soil location from this investigation in close proximity to 720-002 is 211-B-005, with a maximum TCE concentration of 3,100  $\mu$ g/kg at a depth of 23 ft bgs/348.94 ft amsl. Overall results from the soil samples indicate that dehalogenation likely is occurring at SWMU 211-B. Of the 245 soil samples collected for VOC analysis during the RDSI, 171 samples have a TCE detection and 27 samples have a *cis*-1,2-DCE detection. Groundwater analysis results also support this finding. The TCE soil isopleths depicted in Figure 10<sup>8</sup> show that the mass present is predominantly located in HU2, with limited low-level detections below HU3 (near the RGA).

Overall, RDSI VOC results at SWMU 211-B trend to be consistent with the previous CSM. The lateral location, vertical location, and magnitude of the greatest magnitude TCE impacts align with previous SI findings. Data available at SWMU 211-B are sufficient to provide a foundation for selection of an appropriate remedial technology to address VOC-impacted groundwater.

As at SWMU 211-A, results of the UCD soil samples from this investigation and historical data were used to create a three dimensional model (using EVS-ES) to represent SWMU 211-B soil impacts. A fivelayer geologic model was used for modeling soil contamination. Soil analytical results from this investigation, shown in Figure 8, were log-processed in the model. As at SWMU 211-A, the Horizontal/Vertical Anisotropy Ratio parameter was set to 1.5. The Octant Search method was used to determine which sample points are selected for inclusion in the kriging matrix. The model used a soil density of 1.4 g/cc and a chemical density of 1.46 g/cc. The SWMU 211-B soil impacted greater than 75 µg/kg of TCE is estimated to be 3,213 bank cubic yards (bcy). The mass of TCE in the SWMU 211-B soil impacted greater than 75  $\mu$ g/kg is estimated to be 5 kg (0.8 gal) at a 90% confidence level. The mass and volume estimates do not extrapolate the area beneath the C-720 Building. Additional TCE impacts mass may be present beneath the C-720 building, but the purpose of this FCR is to select a remedy for accessible soil contamination. Figure 8 also shows the smaller areas of 75 µg/kg soil TCE (50% confidence limit) and 1,000 µg/kg soil TCE (90% confidence limit) for comparison. A sensitivity analysis was performed. The volume/mass estimates range from 0.1 gal/0.6 kg to 0.8 gal/4 kg for a range of 10% to 90% confidence level with a volume/mass of 0.3 gal/2 kg for the 50% confidence level. A CD containing viewable three-dimensional model EVS-ES files and details regarding the sensitivity analysis are included in Appendices B and C.

The area potentially requiring treatment is defined by the areal distribution of soil boring locations with depth-average TCE concentration greater than 75  $\mu$ g/kg. The area (defined by borings 211-B-001, 211-B-004, 211-B-005, and 211-B-019) covers approximately 3,000 ft<sup>2</sup> (at a 90% source volume confidence level) laterally with a depth interval of 8.5 ft bgs to 64.5 ft bgs (approximate volume of 6,200 bcy).

<sup>&</sup>lt;sup>8</sup> Figure 10 is a cross section taken from a three-dimensional model of TCE sample results. Where samples were not collected for laboratory analyses from the bottom depth of a soil boring (samples were collected at discrete intervals targeted by field measurements over each 5-ft interval), the bottom depths depicted on Figure 10 do not represent the total depth of the soil boring.



As similarly stated in the SWMU 211-A section, RDSI data indicate that soil VOC concentrations are decreasing over time, based on natural processes.

# 9. CONCLUSION

This FCR presents the results of the RDSI for SWMUs 211-A and 211-B, which were outlined in the *Remedial Design Work Plan for Solid Waste Management Units 1, 211-A, 211-B, Volatile Organic Compound Sources for the Southwest Groundwater Plume at the Paducah Gaseous Diffusion Plant, Paducah, Kentucky* (DOE 2012a). The RDSI was performed to better determine the lateral and vertical extent and distribution of VOCs and source material in the Southwest Plume source areas and to determine soil and groundwater parameters, including geochemical parameters, at each of the SWMUs to be used to design *in situ* bioremediation, if this alternative is selected. The results of this RDSI provide the data necessary for identifying the areas to be treated and selecting the remedies at SWMUs 211-A and 211-B.

The selected remedy, as identified in the ROD for SWMUs 211-A and 211-B pending this final characterization of source extent and magnitude, is *in situ* source treatment using enhanced *in situ* bioremediation with LUCs (Alternative 8) or long-term monitoring with interim LUCs (Alternative 2).

**SWMU 211-A.** Data collected during the RDSI further delineated the magnitude and areal and vertical extents of TCE and other VOC contamination at SWMU 211-A. As during previous investigations, RDSI results indicate that soils containing VOC contaminations are located at the northeast corner of the C-720 Building Area. However, the highest level of TCE (4,800  $\mu$ g/kg) detected during the RDSI was at sample location 211-A-036, which is located approximately 240 ft west of the previous investigation maximum concentration (8,100  $\mu$ g/kg TCE) location (720-027 at 30-ft depth/344.39 ft amsl elevation). The SWMU 211-A soil volume impacted greater than the remediation goal of 75  $\mu$ g/kg of TCE is estimated to be 29,000 bcy with an areal extent of 34,000 ft<sup>2</sup> (using both the RDSI data and all historical soil TCE data for the SWMU 211-A investigation area in OREIS). Approximately 2.2 gal (12 kg) of TCE at a 90% confidence level is estimated to be present.

As part of the hydrologic analysis to assess the ability of the HU1, HU2, and HU3 formations to accept injectate at suitable pressures and flow rates, soil conditions at SWMU 211-A appear to be consistent with the requirements associated with an injection-dependent technology.

Overall results from the RDSI indicate that limited dehalogenation (i.e., degradation of parent VOCs to daughter products such as TCE degrading to *cis*-1,2-DCE and VC and 1,1,1-TCA to 1,1-DCE) is occurring at SWMU 211-A.

**SWMU 211-B.** The lateral location, vertical location, and magnitude of the greatest magnitude TCE impacts align with the current CSM. RDSI results at SWMU 211-B indicate that soils containing VOC contamination are present in the subsurface at the southeast corner of the C-720 Building Area. VOC concentrations are decreasing over time. RDSI soil data indicate that dehalogenation likely is occurring, but is inhibited at SWMU 211-B. The SWMU 211-B soil impacted greater than the remediation goal of 75  $\mu$ g/kg of TCE is estimated to be 3,213 bcy (using both RDSI data and all historical soil TCE data for the SWMU 211-B investigation area in OREIS). The mass of TCE in the SWMU 211-B soil impacted at TCE concentrations greater than 75  $\mu$ g/kg and accessible for possible treatment is estimated to be 5 kg (0.8 gal) at a 90% confidence level. Any TCE contamination located underneath the C-720 Building footprint associated with SWMU 211-B will be addressed, as appropriate, under the Soils and Slabs OU, as specified in the Fiscal Year 2013 Site Management Plan (DOE 2013).

The hydrologic analysis to assess the ability of the HU1, HU2, and HU3 formations to accept injectate at suitable pressures and flow rates indicates that soil conditions at SWMU 211-B are consistent with the requirements associated with an injection dependent technology: a flow rate of approximately 2.4 gpm at a pressure of 50 psi, if achievable, should provide effective distribution of injectate among the HU1, HU2,

and HU3 formations at SWMU 211-B. Overall results from the RDSI indicate that limited dehalogenation (i.e., degradation of parent VOCs to daughter products such as TCE degrading to *cis*-1,2-DCE) is occurring at SWMU 211-B.

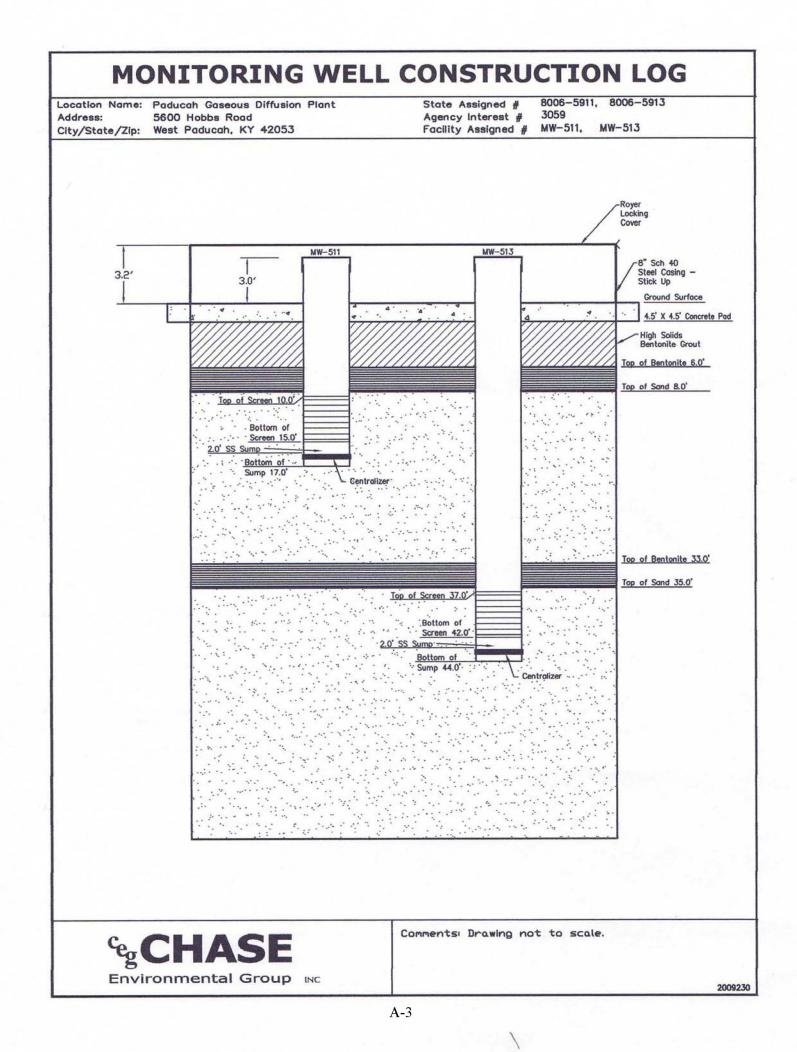
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**APPENDIX A** 

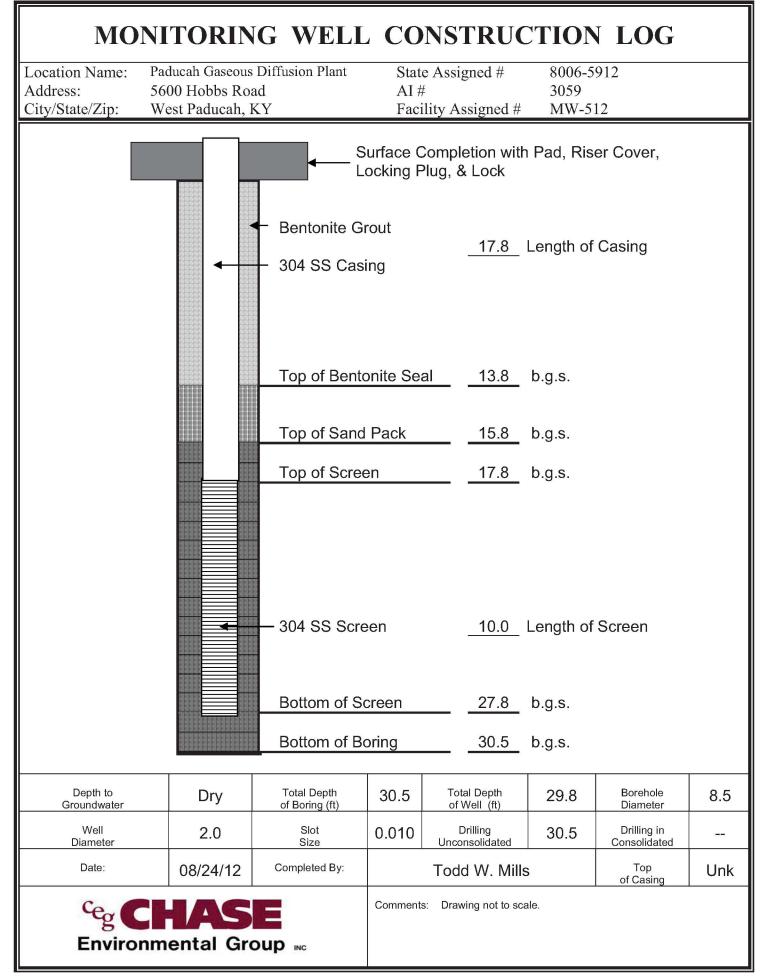
MONITORING WELL CONSTRUCTION LOGS



Ceg CHASE Environmental Group ™						Soil Boring Log								
Project: Southwest Plume RDSI – C-720 Northeast						Northeast Boring Location: MW-511/MW-513								
Date Drilled: 8/24/12 Date Completed: 8/27/12						Sampling Method: Dual Tube Surface Elevation:								
Date Completed: 8/27/12 Drilling Method: 6.25" ID HSAs						Total Depth: 44.5								
Drilling Company: Chase Environmental Group						Group Logged By: Ken Davis, LATA of Kentucky								
DEPTH feet	SAMPLE NUMBER	BLOW COUNT 6"	<b>UIA</b> mdd	REC	FORMATION	GEOLOGIC DESCRIPTION								
0.0						Dark Gray to Light Brown Silty GRAVEL w/organics								
2.5						Light Brown to Dark Gray SILT, Soft, Moist								
15.2						Reddish Yellow to Light Gray Gravely Fine SAND grading to SILT, Soft to Dense, Moist								
21.5						Light Gray to Pale Brown Fine SAND w/GRAVEL, Hard, Moist								
35.2						White to Reddish Yellow Silty Fine SAND, Soft, Moist								
44.5						No Refusal – Boring Terminated @ 44.5 in SAND As Above.								

		UN	IFORM K	ENTUC	KY WELL CC	NSTRUC	FION RI	ECORD							
Use this form to report installation of monitoring or water wells.															
Form must be completed and submitted to the Division of Water within 60 days of well completion.															
					See instructions b	elow.									
			One	copy to ov	vner and one copy	/ to driller'	™s files.								
Owner Name(*)	United	Statas Doportmo	nt of Enorg								1				
	Owner Name(*)         United States Department of Energy           Owner First Name         Owners Let Num/(*)														
(*)	NA		Ow	ner Last	Name(*) NA										
Owner Address(*)	5600 H	obbs Road													
Owner City(*)	West P	aducah St	ate(*) Kei	ntucky	• Owr	ner Zip(*)	42086								
Owner Phone(*)	270-441	1-6800	Owner e	eMail							_				
Site Name(*)	Paduca	h Gaseous Diffu	sion Plant										Kentucky Well ID		
Site Address(*)	5600 H	obbs Road				]							(AKGWA) Number	8006-5911	
Site City(*)	West P	aducah St	ate(*) Ke	ntucky	▼ Site	Zip(*) 420	86						(*) Owner Well ID	MW-511	-
Site Phone	270-441	1-6800	Site eMa	ail									Work Start Date(*)	08/24/2012	
Well Latitude(*)													Work End Date(*)	08/27/2012	
DMS to DD Conv	37.1	14	Well Longi	tude(*)	88.815	Method	l(*) Mar	p Grade (	GPS - Diffe	erentially Co	orrected		Total depth (ft)(*)	17.0	
Agency Interest (AI	) Number	3059	Facility 7	Type & II	CERCLA				-				Depth to bedrock (ft)		
USGS Topo Map(*		ATH		•	County(*)		McCrac	ken	-				Static water level (ft)		<u>_</u>
Surface elevation (ft					Elevation dete					ation - digitiz	zed 💌		SWL method(*) Casing height above	Undetermined -	
Physiographic Regio	on(*) Jac	ckson Purchase	•		Well Use(*)		Monitori	ng well - o	complian	ce	•		surface (in)		
Drilling Method(*)		ger - hollow stem		-	Well Status(*	-	active			-			WATER WELLS ON	LY	
Wellhead(*)		cking Cap 💌			Well Condition	on(*)	Functior	ning prop	erly 💌				Estimated well yield		
Casing / Open Bore		To depth (ft)(*)	Borehole	liameter	(in)(*) Casing di	iameter (in)	(*) Casin	na type(*)	)				Well Yield Method Well service (# of		
Delete 0	, , , , , , , , , , , , , , , , , , ,	10.0	10.5		2			I - stainle					people served)	ļ	
Delete 15.0		17.0	10.5		2		Stee	I - stainle	SS				Disinfectant amount		
Add New													Disinfectant type Pitless adapter		
Screen				Borehold	e diameter (in)	Screen dia	meter (in	)(*)			Screen slo	st	installed		
From depth	(ft)(*)(*)	To depth (ft)	*)(*)	(*)(*)		(*)	ineter (in	Scr	reen Type	(*)(*)	size(*)(*)		Pump installed		<u> </u>
Delete 10.0		15.0		10.5		2		Ste	eel - stain	less	• 0.010		Depth to intake (ft) Apparent quality and	odor:	
New													Appearance	<b>•</b>	
Annulus fill and seal									1				Odor Type	•	
Section(* Delete Grout	*) Fro	om depth (ft)(*)	To de	epth (ft)(*		rial(*) conite		<b>_</b>					Odor-Level		
Delete Seal	6.0	1	8.0		Bent								Coliform Test Coliform test type	-	
Delete Filter Pa			33.0		San			•						· · ·	
Add New														or	
Lithologic log	oth (ft)(*)	To depth (ft)(*)	Description	n(*)									Coliform test results	# colonies per 10	00 ml
Add New	, (ii)( )	1.5 ucpui (ii)( )	Sesenpilo												
Site Map/Sketch M	ap(*)								E	Browse			Date Sampled		
Well Diagram (moni	toring we	11)									Browse		Date Analyzed		
Coliform analysis (if	applicabl	e)									Browse	1	Save For Future F	Retrieval	Submit to DEP
Signed variance (if a											Browse				
Other laboratory and											Browse				
Casing/Screen Supp											Browse				
Comments This is t Affirmation: I certify				ent and al	l attachments w	ere prepare	d under r	ny direct	ion or sur	ervision in	accordance wi	ha			
system designed to a who manage the syst	ssure that	qualified person	nel properl	y gather a	and evaluate the	information	n submitt	ted. Base	d on my i	nquiry of th	e person or per	sons			
belief, true, accurate,	and comp	olete. I am aware	that there a	re signifi	cant penalties fo	r submitting	g false int	formatior	n, includin	g the possib	oility of fine and	1			
imprisonment for kno either by me or by th			nung data,	uns trans	mission constitu	ues my signa	ature and	1 am res	ponsible f	or any and a	an content subr	nued			
Signature of certified driller & PIN(*) Date Signed(*) 03/27/2013															
Driller First Name(*	) Todd					Driller La Name(*)		Mills							
Certification Number (*)	r 0344-0	454-00				Certificat Company	ion	Chase E	nvironme	ntal Group, I	Inc.				

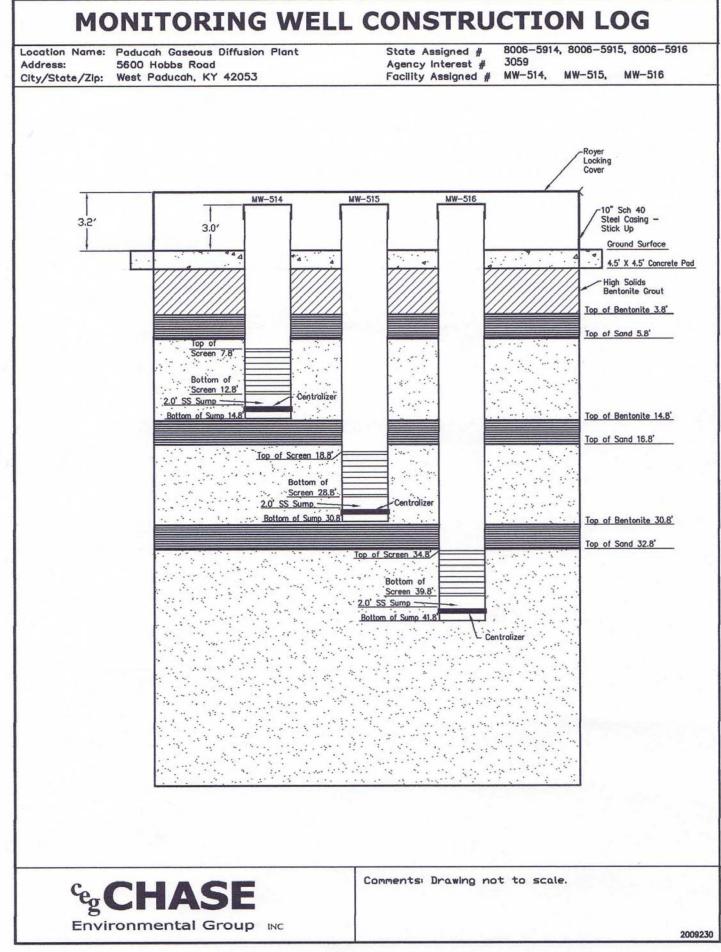
UN							
Form must be c							
[							
Owner Name(*) United States Departmen	nt of Energy						
Owner First Name (*) NA	Owner Last Name(*	*) NA					
Owner Address(*) 5600 Hobbs Road							
Owner City(*) West Paducah Sta	ate(*) Kentucky	• Owner Zip(*) 42086					
Owner Phone(*) 270-441-6800	Owner eMail						
Site Name(*) Paducah Gaseous Diffus	sion Plant						
Site Address(*) 5600 Hobbs Road					Kentucky Well ID (AKGWA) Number	8006-5913	
Site City(*) West Paducah Sta	ate(*) Kentucky	▼ Site Zip(*) 42086			(*)	18000-3913	
Site Phone 270-441-6800	Site eMail					MW-513	
Well Latitude(*)	Well Longitude(*) -88.815	Method(*)	ap Grade GPS - Differentially Co	rrected 💌		08/24/2012	
DMS to DD Converter					Work End Date(*)	08/27/2012	
Agency Interest (AI) Number 3059	Facility Type & ID CER	CLA 👤			1 ( )( )	44.0	
USGS Topo Map(*) HEATH	<ul> <li>Coun</li> </ul>		icken 🔻		Depth to bedrock (ft)		
Surface elevation (ft)			raphic map interpolation - digitize	ed 💌	Static water level (ft)		_
Physiographic Region(*) Jackson Purchase			ring well - compliance	•	SWL method(*)	Undetermined	<u> </u>
Drilling Method(*) Auger - hollow stem		Status(*) active			Casing height above surface (in)		
Wellhead(*) Locking Cap			oning properly		WATER WELLS ON	LY	
					Estimated well yield		
Casing / Open Borehole From depth (ft)(*) To depth (ft)(*)	Porahala diamatar (in)(*)	Casing diamator (in)(*) Cas	ing type(*)		Well Yield Method	<u></u>	
	10.5		el - stainless		Well service (# of	 	
	10.5		el - stainless 🔹		people served)	ļ	
Add New	10.0				Disinfectant amount		
Screen					Disinfectant type		•
	*)(*) Borehole diame	ter (in) Screen diameter (	in)(*)	Screen slot	Pitless adapter		
From depth $(ft)(*)(*)$ To depth $(ft)(*)(*)$	*)(*) Borenoie diame	(*)	in)(*) Screen Type(*)(*)	size(*)(*)	installed		
Delete 37.0 42.0	10.5	2	Steel - stainless	• 0.010	Pump installed		-
Add New					Depth to intake (ft) Apparent quality and		
Annulus fill and seal					Appearance	•	
Section(*) From depth (ft)(*)	To depth (ft)(*)	Material(*)			Odor Type		
Delete Grout  1	6.0	Bentonite	•		Odor-Level		-
Delete Seal  6.0	8.0	Bentonite			Coliform Test		
Delete Filter Pack  8.0	33.0	Sand	-		Coliform test type		•
Delete Seal  33.0	35.0	Bentonite					
Delete Filter Pack 35.0	44.5	Sand					
Add New					Coliform test results	or	
Lithologic log						# colonies per	100 ml
From depth (ft)(*) To depth (ft)(*)	Description(*)				Date Samulad		
Add New					Date Sampled Date Analyzed		
Site Map/Sketch Map(*)	<u> </u>		Browse	Browne	Save For Future R	etrieval	Submit to DEP
Well Diagram (monitoring well) Coliform analysis (if applicable)				Browse			
Signed variance (if applicable)				Browse			
Other laboratory analysis report (if applicable)				Browse			
Casing/Screen Supplemental Info				Browse			
Comments This is the deep well in a 2 well nes	sted set.						
Affirmation: I certify under penalty of law that the		ments were prepared under	my direction or supervision in a	accordance with a			
system designed to assure that qualified personn	nel properly gather and eval	luate the information subm	itted. Based on my inquiry of the	e person or persons			
who manage the system, or those persons direct belief, true, accurate, and complete. I am aware							
imprisonment for knowing violations. By submi							
either by me or by the people I represent.		1					
Signature of certified driller & PIN(*)		Date Signed(*)	03/27/2013				
Driller First Name(*) Todd		Driller Last Name(*)	Mills				
Certification Number 0344-0454-00		Certification Company(*)	Chase Environmental Group, Ir	ıc.			



	Ceg	C	H		5 Gro	Soil Boring Log Page 1 of 1
	ct: Sout	thwest F	lume R			Northeast Boring Location: MW-512
		8/22/12 ted: 8/2				Sampling Method: Dual Tube Surface Elevation:
			25" ID H	ISAs		Total Depth: 30.5
Drilli	ng Com	pany: (	Chase Ei	nvironi	nenta	Group Logged By: Ken Davis, LATA of Kentucky
DEPTH feet	SAMPLE NUMBER	BLOW COUNT 6"	<b>PID</b> mqq	REC	FORMATION	GEOLOGIC DESCRIPTION
0.0						Topsoil w/ Organics Mixed with Pea GRAVEL, Loose, Moist
1.2						White to Light Brown SILT, Soft, Moist
20.0						Reddish Yellow to Light Gray Gravely Fine SAND grading to SILT, Soft to Dense, Moist
22.2						Reddish Yellow to Pinkish Gray Sandy to Clayey GRAVEL, Loose, Moist
23.7						Light Gray to Pale Brown Silty to Gravely Fine SAND, Firm, Moist
30.5						No Refusal – Boring Terminated @ 30.5 in SAND As Above.

**Drilling & Remedial Action Contractors** 9470 Hwy. 60 West – Kevil, Kentucky 42053 270-488-2584 Fax: 270-488.2586

			UNIFC	RM KENTUC	KY WELL CO	ONSTRUCT	ION REC	ORD						
			U	se this form to rep	ort installation of	monitoring or v	water wells.							
			Form must be comp	leted and submitte	ed to the Division	of Water withi	in 60 days of	f well comple	tion.					
					See instructions b	below.								
				One copy to ov	vner and one copy	y to driller'	s files.							
Owner Name	e(*)	Inited S	States Department of	Eporav										
Owner First 1	Nome		states Department of											
(*)	N	IA		Owner Last	Name(*) NA	1		_						
Owner Addro	ess(*) 5	600 Ho	obbs Road											
Owner City(*	*)	Vest Pa	aducah State(	*) Kentucky	• Own	ner Zip(*)	2086							
Owner Phone	e(*) 2	70-441	-6800 C	wner eMail										
Site Name(*)	)	aducal	n Gaseous Diffusion	Plant								Kentucky Well ID		
Site Address	(*) 5	600 Ho	bbs Road									(AKGWA) Number (*)	8006-5912	
Site City(*)	V	Vest Pa	aducah State(	*) Kentucky	<ul> <li>Site</li> </ul>	Zip(*) 4208	6					Owner Well ID	MW-512	
Site Phone	2	70-441	-6800 S	ite eMail								Work Start Date(*)	08/22/2012	
Well Latitude	e(*)	37.1	14 Wall	Longitude(*)	00 01/	Mathad(	*) Map C	rada CBS	Differentially C	arracted		Work End Date(*)	08/24/2012	
DMS to DD	Converte		wei	Longitude(*)		ivietnod(		aue aro -		orrected		Total depth (ft)(*)	30.5	
Agency Intere	est (AI) N	umber	3059 Fa	cility Type & II	CERCLA	•						Depth to bedrock (ft)		_
USGS Topo N	Map(*)	HE	ATH		County(*)	1	McCracker	י ו <u>י</u>			]	Static water level (ft) SWL method(*)	Undetermined -	1
Surface elevat	tion (ft)	370			Elevation dete	ermined by	Topograph	ic map inter	polation - digit	ized 💌		Casing height above		1
	- ·		kson Purchase 💌		Well Use(*)			well - compl		-		surface (in)		
Drilling Metho	od(*)		er - hollow stem	-	Well Status(*		active		<u>•</u>			WATER WELLS ON		
Wellhead(*) Casing / Open	Dorahol		king Cap 💌		Well Condition	л(*) <u>[</u> [	Functioning	g properly	]			Estimated well yield Well Yield Method		
			To depth (ft)(*) Bor	ehole diameter (	in)(*) Casing d	iameter (in)(*	*) Casing t	ype(*)				Well service (# of		
Delete 0	1		17.8 8.5		2		-	stainless				people served)		
Delete 27.	.8		29.8 8.5		2		Steel - s	stainless	•			Disinfectant amount		
Add New												Disinfectant type Pitless adapter		
Screen				Borehole	e diameter (in)	Screen diam	neter (in)(*	·)		Screen slo	ot	installed		
	depth (ft)(	(*)(*)	To depth (ft)(*)(*	) (*)(*)		(*)		Screen 1	'ype(*)(*)	size(*)(*)		Pump installed		
Delete 17.8 Add			27.8	8.5		2		Steel - st	tainless	• 0.010		Depth to intake (ft) Apparent quality and	l odor:	
New												Appearance		
Annulus fill an				1	1							Odor Type	-	
	ction(*)	From	m depth (ft)(*)	To depth (ft)(*		rial(*) tonite		•				Odor-Level Coliform Test	<b>_</b>	
Delete Se		13.8	3	15.8	Bent							Colliform test type	-	
	Iter Pack			30.5	San									
Add New												C-liferen test men lte	or	
Lithologic log		(ft)(*)	To depth (ft)(*) Des	cription(*)								Coliform test results	# colonies per 10	00 ml
Add New	deput	(1)()		cpuon( )										
Site Map/Ske	tch Map(	*)							Browse			Date Sampled		
Well Diagram	(monitori	ng well	)							Browse	1	Date Analyzed		
Coliform analy	ysis (if app	plicable	)							Browse		Save For Future F	Retrieval	Submit to DEP
Signed variand										Browse				
			rt (if applicable)							Browse				
Casing/Screen	1 Supplem	nental li	nto							Browse	1			
Comments Affirmation: Lo	ertify und	ler pop	alty of law that this c	locument and a	1 attachmente v	ere prepared	under my	direction or	supervision in	accordance wi	 th a			
system designe	ed to assur	re that o	qualified personnel p	properly gather a	and evaluate the	information	submitted	. Based on n	ny inquiry of t	he person or per	sons			
belief, true, acc	curate, and	l compi	se persons directly re lete. I am aware that	there are signifi	cant penalties fo	or submitting	false infor	mation, inclu	uding the possi	bility of fine and	đ			
imprisonment f			ations. By submitting represent.	g data, this trans	mission constitu	ttes my signat	ture and I a	am responsit	ole for any and	all content subr	nitted			
Signature of co driller & PIN(	ertified	Todd W				Date Signe	ed(*)	/27/2013						
Driller First N		Todd				Driller Las Name(*)	st Mi	ills						
Certification N	Number	0344-04	154-00			Certificatio Company(		nase Environ	mental Group,	Inc.	_			
(*)						Company(								



A-10

					5 Gro	Soil Boring Log Page 1 of 1
	ct: Sou Drilled:			DSI		Boring Location: MW-514/MW-515/MW-516 Sampling Method: Dual Tube
Date	Comple	ted: 8/2	27/12			Surface Elevation:
Drilli Drilli	ing Meth ing Com	10d: 8.2 many: (	25" ID H Thase Ei	ISAs nvironi	nenta	Total Depth:         44.5           I Group         Logged By:         Ken Davis, LATA of Kentucky
DEPTH feet	SAMPLE NUMBER	BLOW COUNT 6"	PID mqq	REC	FORMATION	GEOLOGIC DESCRIPTION
0.0						Unclassified Select Fill
2.5						Light Gray SILT, Firm, Moist
16.5						Light Gray to Reddish Yellow Gravely to Silty SAND, Dense, Moist
21.3						Reddish Yellow to White Silty Fine SAND, Firm, Moist
25.9						Reddish Yellow to Pale Brown Silty Fine SAND and Gravel, Dense, Moist
37.4						Pale Brown to Pink SILT, Soft, Moist
44.5						No Refusal – Boring Terminated @ 44.5 in SILT As Above.

**Drilling & Remedial Action Contractors** 9470 Hwy. 60 West – Kevil, Kentucky 42053 270-488-2584 Fax: 270-488.2586

			UN	IFORM K	ENTUC	KY WELL CO	ONSTRUC	TION R	ECORE	)						
				Use this f	orm to rep	ort installation of	monitoring of	or water w	ells.							
			Form must be c	completed as	nd submitte	ed to the Division	of Water wi	thin 60 day	ys of well	completio	1.					
						See instructions	below.									
				One	copy to ov	wner and one cop	y to drillerâ€	тмs files.								
Owner Name(*	*)	aited C	tates Departme	nt of Enorg												
Owner First Na	, i		states Departine			]										
(*)	N.	A		Ow	ner Last	Name(*) NA	-1									
Owner Address	s(*) 56	600 Ho	bbs Road													
Owner City(*)	W	est Pa	iducah St	ate(*) Ke	ntucky	• Ow	ner Zip(*)	42086		1						
Owner Phone(*	*) 27	'0-441-	·6800	Owner	eMail 🗌											
Site Name(*)	Pa	aducal	n Gaseous Diffus	sion Plant										Kentucky Well ID		
Site Address(*)	) 50	600 Ho	bbs Road											(AKGWA) Number	8006-5914	
Site City(*)	W	est Pa	iducah St	ate(*) Ke	ntucky	▼ Site	Zip(*) 42	086						(*) Owner Well ID	MW-514	=
Site Phone	27	/0-441-	·6800	Site eM	ail									Work Start Date(*)	08/23/2012	
Well Latitude(*	*)													Work End Date(*)	08/27/2012	
DMS to DD Co	onverter	37.11	12	Well Long	itude(*)	-88.815	Metho	d(*)   Ma	ap Grade	GPS - Di	ferentially C	orrected	1	Total depth (ft)(*)	14.8	
Agency Interest		1	3059	Facility	Гуре & П	CERCLA				_				Depth to bedrock (ft)		
USGS Topo Ma		HEA			•	County(*)		McCrao	cken	-			1	Static water level (ft)		-
Surface elevation		370				Elevation det	ermined by				lation - digiti	zed 💌		SWL method(*) Casing height above	Undetermined _	
Physiographic R	Region(*)	) Jacl	kson Purchase	•		Well Use(*)		Monitor	ring well -	- complia	ice	•		surface (in)		
Drilling Method	(*)	-	er - hollow stem		-	Well Status(*	,	active			•			WATER WELLS ON	LY	
Wellhead(*)		p	king Cap 💌			Well Conditi	on(*)	Functio	oning pro	perly 💌				Estimated well yield		
Casing / Open E			To depth (ft)(*)	Borehole	diameter (	(in)(*) Casing (	liameter (in	)(*) Casi	na type(?	*)				Well Yield Method Well service (# of		-
Delete 0	i depui (		7.8	12.5		2			el - stainl		•			people served)	ļ	
Delete 12.8			14.8	12.5		2		Stee	el - stainl	ess	•			Disinfectant amount		
Add New														Disinfectant type Pitless adapter		
Screen					Borehold	e diameter (in)	Screen dia	meter (i	n)(*)			Screen sl	vt I	installed		
From dej	pth (ft)(	*)(*)	To depth (ft)(	*)(*)	(*)(*)		(*)	unicici (il	Sc	creen Typ	e(*)(*)	size(*)(*)	<i>.</i>	Pump installed		<u> </u>
Delete 7.8			12.8		12.5		2		s	steel - stai	nless	• 0.010		Depth to intake (ft) Apparent quality and	odor:	
New														Appearance	<b></b>	
Annulus fill and	seal									1				Odor Type		
Delete Grou	ion(*)	From	n depth (ft)(*)	To de 3.8	epth (ft)(*		erial(*) tonite			_				Odor-Level	•	
Delete Seal		3.8		5.8			tonite		-					Coliform Test Coliform test type		
	r Pack			14.8		Sar			-							
Add New															or	
Lithologic log	a danth (	<del>6</del> )(*)'	Γo depth (ft)(*)	Docomintio	n(*)									Coliform test results	# colonies per 1	00 ml
Add New	i depui (	n)( )		Descriptio	n( )											
Site Map/Sketcl	h Map(*	<sup>-</sup> )									Browse			Date Sampled		
Well Diagram (n	nonitorir	ıg well	)									Browse		Date Analyzed	J	
Coliform analysi	is (if app	licable	;)									Browse		Save For Future F	Retrieval	Submit to DEP
Signed variance												Browse				
Other laboratory		-										Browse				
Casing/Screen S				<u></u>								Browse				
Comments This Affirmation: I cert					ent and al	l attachments v	vere prenare	ed under	my direc	ction or si	nervision in	accordance wi	tha			
system designed who manage the	to assure	e that o	qualified person	nel properl	y gather a	and evaluate the	e informatic	n submit	tted. Bas	ed on my	inquiry of th	he person or per	sons			
belief, true, accur	rate, and	compl	ete. I am aware	that there a	ire signifi	cant penalties for	or submittin	g false ir	nformatic	on, includ	ng the possil	bility of fine an	đ			
imprisonment for either by me or b				itting data,	unis trans	mission constitu	ites my sigi	nature and	a I am re	sponsible	tor any and	all content subr	nitted			
Signature of cert driller & PIN(*)		odd W	/ Mills				Date Sig	med(*)	03/27/2	013						
Driller First Nan	ne(*) T	odd					Driller L Name(*		Mills							
Certification Nut (*)	umber 0	344-04	54-00				Certifica Compan		Chase	Environm	ental Group,	Inc.				

	UNI	FORM KENTUCK	Y WELL CON	NSTRUCTION R	ECORD					
		Use this form to repor	rt installation of m	nonitoring or water w	ells.					
	Form must be co	ompleted and submitted	l to the Division o	of Water within 60 da	ys of well complet	ion.				
		-	ee instructions be							
		One copy to own	ner and one copy	to driller's files.			-1			
Owner Name(*)	United States Departmen	t of Energy								
Owner First Name (*)	NA	Owner Last N	(ame(*) NA							
Owner Address(*)	5600 Hobbs Road									
Owner City(*)	West Paducah Sta	te(*) Kentucky	- Owne	er Zip(*) 42086						
Owner Phone(*)	270-441-6800	Owner eMail	-	- · · · ] -						
Site Name(*)	Paducah Gaseous Diffusi	ion Plant								
Site Address(*)	5600 Hobbs Road							Kentucky Well ID		
Site City(*)	West Paducah Sta	te(*) Kentucky	▼ Site Z	Zip(*) 42086				(AKGWA) Number (*)	8006-5915	_
Site Phone	270-441-6800	Site eMail						Owner Well ID	MW-515	
Well Latitude(*)				_				Work Start Date(*)	08/23/2012	
DMS to DD Conve		Vell Longitude(*) -8	8.815	Method(*)	p Grade GPS - I	Differentially C	orrected 💌	Work End Date(*)	08/27/2012	
Agency Interest (AI)		Facility Type & ID	CEBC! A					Total depth (ft)(*)	30.8	
			p	McCra				Depth to bedrock (ft)		
USGS Topo Map(*)	·		County(*)		cken 💌	polotion digiti	Tod I	Static water level (ft)		
Surface elevation (ft)	-		Elevation deter					SWL method(*)	Undetermined -	
Physiographic Region	n(*) Jackson Purchase	_	Well Use(*) Well Status(*)	active	ing well - compli			Casing height above surface (in)		
Drilling Method(*) Wellhead(*)	Locking Cap		Well Condition		ning properly			WATER WELLS ON	LY	
			wen condition		ning properly	J		Estimated well yield		•
Casing / Open Boreh	th (ft)(*) To depth (ft)(*) I	Borehole diameter (ir	n)(*) Casing dia	ameter (in)(*) Casi	ng type(*)			Well Yield Method		7
Delete 0		12.5	2		el - stainless	•		Well service (# of		<u> </u>
Delete 28.8		12.5	2		el - stainless	-		people served)		
Add New	P P		,					Disinfectant amount		•
Screen								Disinfectant type	•	
From depth (	ft)(*)(*) To depth (ft)(*	Borehole a	diameter (in)	Screen diameter (i	n)(*) Screen T	vne(*)(*)	Screen slot	Pitless adapter		
	28.8	(*)(*) 12.5	(	(*)			size(*)(*)	Pump installed		•
Delete 18.8 Add	28.8	12.5		2	Steel - st	ainiess	0.010	Depth to intake (ft)		
New								Apparent quality and	l odor:	
Annulus fill and seal								Appearance	-	
Section(*		To depth (ft)(*)	Materi	ial(*)				Odor Type		
Delete Grout	• 1	3.8	Bento					Odor-Level	-	
Delete Seal	3.8	5.8	Bento					Coliform Test	1	
Delete Filter Pac		14.8	Sand					Coliform test type	·	
Delete Seal	▼ 14.8	16.8	Bento		-				-	
Delete Filter Pac Add New	ck 💌 16.8	30.8	Sand					Coliform test results	or	
Lithologic log	1								# colonies per 10	0 ml
	th (ft)(*) To depth (ft)(*) I	Description(*)								
Add New								Date Sampled		
Site Map/Sketch Ma	ap(*)					Browse		Date Analyzed		
Well Diagram (monit	oring well)						Browse	Save For Future I	Retrieval S	ubmit to DEP
Coliform analysis (if	applicable)						Browse			
Signed variance (if a	oplicable)						Browse			
Other laboratory ana	lysis report (if applicable)						Browse			
Casing/Screen Suppl	emental Info						Browse			
Comments This is th	e intermediate well in a 3 w	vell nested set.								
	inder penalty of law that th									
	sure that qualified personn em, or those persons directl							d		
belief, true, accurate, a	and complete. I am aware th	hat there are significa	ant penalties for	submitting false in	formation, inclu	iding the possi	bility of fine and			
imprisonment for kno either by me or by the	wing violations. By submit e people I represent.	tting data, this transm	ussion constitute	es my signature an	d I am responsib	le for any and	all content submitted			
Signature of certified driller & PIN(*)				Date Signed(*)	03/27/2013					
Driller First Name(*)	Todd			Driller Last Name(*)	Mills			-		
Certification Number (*)	0344-0454-00			Certification Company(*)	Chase Environ	mental Group,	Inc.			
<u>  C /</u>	1			Sourbard ()	L					

			UN	IFORM F	KENTUCK	Y WELL C	ONSTRUC	TION RI	ECORD							
				Use this i	form to repo	rt installation c	f monitoring o	or water we	ells.							
			Form must be	completed a	nd submitted	to the Divisio	n of Water wi	thin 60 day	s of well o	completion.						
					s	ee instructions	below.									
				One	copy to ow	ner and one co	py to drillerâ€	™s files.								
Owner N	Jame(*)	United S	States Departme	nt of Energ	ју											
Owner F (*)	irst Name	NA		Ow	/ner Last N	ame(*) NA										
	Address(*)	5600 Ho	obbs Road				-									
Owner C	City(*)	West Pa	aducah Si	ate(*) Ke	entucky	• Ov	vner Zip(*)	42086								
Owner P	hone(*)	270-441	-6800	Owner	eMail			,								
Site Nan	ne(*)	Paduca	h Gaseous Diffu	sion Plant												
Site Add	ress(*)	5600 Ho	obbs Road				-									
Site City	(*)	West Pa	aducah St	ate(*) Ke	entucky	▼ Sit	e Zip(*) 42	086						Kentucky Well ID	8006-5916	
Site Phor	ne	270-441	-6800	Site eM	fail						]			(AKGWA) Number (*)	8006-5916	
Well Lat	itude(*)	37.1	10	W. II T	itude(*) -8	0.015		1(2)	- 0 d	ODC Differential				Owner Well ID	MW-516	
DMS to	DD Conver		12	well Long		8.810	Metho	d(*)   Maj	p Grade (	GPS - Differential	ly Correc	ted 💌		Work Start Date(*)	08/23/2012	
Agency I	nterest (AI)	Number	3059	Facility	Type & ID	CERCLA	-							Work End Date(*) Total depth (ft)(*)	08/27/2012	
USGS To	opo Map(*)	HE	АТН		•	County(*)		McCrac	ken	•				Depth to bedrock (ft)		
	evation (ft)	370		_		Elevation de				p interpolation - d	ligitized	-		Static water level (ft)		
Physiogra Drilling N	phic Region		kson Purchase er - hollow stem	_	•	Well Use(*) Well Status		Monitori	ing well -	compliance		<u> </u>		SWL method(*)	Undetermine	ed 💌
Wellhead		_	king Cap			Well Condit			ning prop					Casing height above surface (in)		
Casing / C	Open Boreho	ole				1								WATER WELLS ON	LY	
Dubte			To depth (ft)(*)	-	diameter (i		diameter (in							Estimated well yield	 	
Delete Delete	0		34.8 41.8	12.5		2			l - stainle		-			Well Yield Method Well service (# of		
Add Nev	v			1		1								people served)		
Screen														Disinfectant amount Disinfectant type		
Fr	om depth (fi	t)(*)(*)	To depth (ft)	(*)(*)	Borehole (*)(*)	diameter (in)	Screen dia (*)	ameter (in	1)(*) Sci	reen Type(*)(*)		Screen slot size(*)(*)		Pitless adapter		<u>•</u>
Delete 34	1.8		39.8		12.5		2		St	eel - stainless	-	0.010		installed		
Add New														Pump installed Depth to intake (ft)		
Annulus f	ill and seal													Apparent quality and	odor:	
	Section(*)		m depth (ft)(*)		epth (ft)(*)		terial(*)							Appearance	-	
Delete Delete	Grout	<ul><li>▼ 1</li><li>▼ 3.8</li></ul>		3.8			ntonite ntonite		-					Odor Type		-
Delete	Filter Pack			14.8		Sa				-				Odor-Level Coliform Test		
Delete	Seal	• 14.8	3	16.8		Ве	ntonite		•					Coliform test type		•
Delete	Filter Pack			30.8		Sa			•						-	]
Delete Delete	Seal Filter Pack	<ul><li>■ 30.8</li><li>&lt; ■ 32.8</li></ul>		32.8		Be	ntonite nd		- -	-				Coliform test results	or	
Add New										<u> </u>					# colonies p	per 100 ml
Lithologic	-				1									Date Sampled		
Add New	-	h (ft)(*)	To depth (ft)(*)	Descriptio	on(*)									Date Sampled		
	/Sketch Map	p(*)								Browse				Save For Future F	Retrieval	Submit to DEP
Well Diag	gram (monito	ring wel	l)									Browse				
Coliform	analysis (if a	pplicable	2)									Browse				
	riance (if ap											Browse				
			rt (if applicable									Browse				
-	reen Supple			J								Browse				
			ell in a 3 well ne alty of law that t		ent and all	attachments	were prepar	ed under r	my direct	tion or supervisio	n in acco	ordance with	a			
system des	signed to ass	ure that	qualified person	nel proper	ly gather ar	nd evaluate th	e informatio	on submitt	ted. Base	ed on my inquiry mitted is, to the b	of the per	rson or perso	ons			
belief, true imprisonm	, accurate, ar	nd comp ving viol	lete. I am aware ations. By subm	that there a	are signific	ant penalties	for submittin	ng false int	formation	n, including the p sponsible for any	ossibility	of fine and				
· · · ·	of certified	Todd V	· ·				Date Sig	gned(*)	03/27/20	)13						
	. ,	Todd					Driller L Name(*		Mills							
Certificati (*)	on Number	0344-04	154-00				Certifica Compar	tion	Chase E	Environmental Gro	oup, Inc.					
							Jonipan	50								

**APPENDIX B** 

THREE-DIMENSIONAL CONTAMINATION MODELS (CD)

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# **APPENDIX B**

THREE-DIMENSIONAL CONTAMINATION MODELS (CD) THIS PAGE INTENTIONALLY LEFT BLANK

**APPENDIX C** 

MODEL SENSITIVITY ANALYSES

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# C.1. SWMU 211-A TCE VOLUME ESTIMATE AND SENSITIVITY ANALYSIS OF ANISOTROPY, MEASURES OF STATISTICAL CONFIDENCE USING HISTORIC (1998 AND 2004) UPPER CONTINENTAL RECHARGE SYSTEM SOIL INVESTIGATION, AND 2012 REMEDIAL DESIGN SUPPORT INVESTIGATION DATA SETS

### C.1.1 PURPOSE

Utilizing the results of soil sampling data provided by LATA Environmental Services of Kentucky, LLC, (LATA Kentucky) Geosyntec has developed estimates of the mass of trichloroethene (TCE) in soils above the Regional Gravel Aquifer (RGA) at Solid Waste Management Unit (SWMU 211-A) 211-A, using C Tech's Environmental Visualization Software (EVS). Provided soil sampling data was collected during evaluation of the Upper Continental Recharge System (UCRS) (1998 and 2004) and Remedial Design Support Investigation (RDSI) (2012) sampling from October 2012 to March 2013. The purpose of this calculation package is to evaluate the sensitivity of TCE mass estimates when interpolating the data using a kriging algorithm by varying the anisotropy of the model and evaluating the statistical confidence of the interpolation.

#### **C.1.2 METHODS**

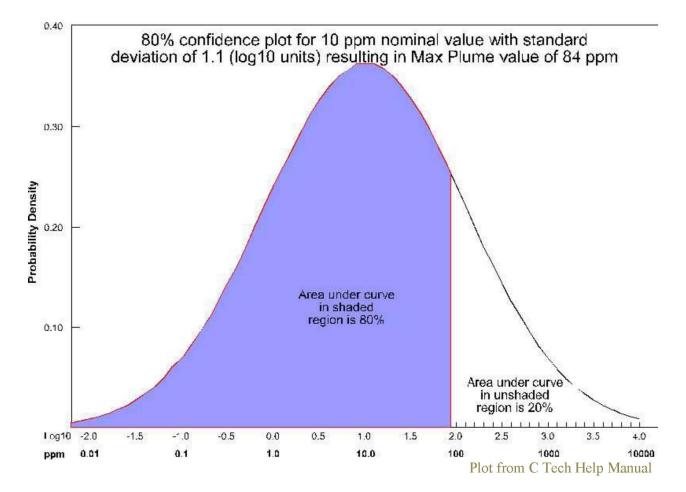
Soil sampling results were interpolated in EVS in order to estimate the volume of TCE in soils. A sensitivity analysis was performed to evaluate the volume of TCE under several different anisotropy ratios: 1, 1.5, 5, and 10. EVS allows for further evaluation of the statistical confidence of the interpolation by providing results at differing user-defined confidence levels. Data were evaluated at 50, 60, 70, 80, and 90% confidence intervals, the results of which are provided in the calculation packages in Appendix C. A site-specific soil density of 1.4 gm/cc was used to calculate TCE mass.

Anisotropy allows the model to consider the effects of anisotropy in the conductivity of soil matrices to fluid flow. In most cases, geologic materials are deposited with platy clay minerals oriented horizontally; thus, flow of water in both the saturated and unsaturated zone can be slower in the vertical direction than in the horizontal direction. Ore deposition also can occur along horizontal or vertical fault or fracture systems. Chemical constituents being transported with flowing fluids, therefore, may show a larger degree of spreading in one or the other direction. The Horiz./Vert. Anisotropy Ratio allows the kriging algorithm to specify a factor to be used to apply biased weighting on data points in horizontal and vertical directions away from a given model node. The default value for fluid flow is 10, which allows data points in a horizontal direction away from a model node to influence the kriged value at that node by a factor of 10 than data points an equal distance away in a vertical direction. A value of 10 typically would be appropriate for dissolved-phase concentrations in an aquifer that is either high-velocity or anisotropic. When the property being modeled is not related to fluid flow or other processes that might be affected by matrix anisotropy, then the recommended value is 1 (i.e., isotropic). Based on observations of data from soil sampling to date in SWMU 211-A, despite the fluid based nature of the release, it is expected that transport is vertically controlled more than horizontally controlled. Therefore the use of a lower anisotropy value is appropriate. Based upon the shape and connectedness of the plume to various sample points, an anisotropy of 1.5 was selected.

EVS can be used to determine the Minimum (Min) and Maximum (Max) Plume, or in this specific case, source area, using a Min-Max algorithm. The Min Plume calculates the minimum estimated size of the

source area at a user-specified confidence level. Conversely, the Max Plume calculates the maximum estimated size of the source area at a user-specified confidence level. To determine the confidence level of the interpolation, EVS first calculates the nominal value and associated standard deviation at every node in the model. For the case of Max Plume and 80% confidence, at each node, a maximum value is determined such that 80% of the time, the actual values will fall below the maximum value (for that nominal concentration and standard deviation). This process is shown below as an example directly from the C Tech Help Manual for the case of an assumed nominal value of 10 ppm with a standard deviation of 1.1 (log units). For this case, the maximum value at that node would be approximately 84 ppm. This process is repeated for every node in the model.

For the plot shown below (from the C Tech Help Manual), the entire left portion of the bell curve is shaded. If assessing the minimum value, it would be the right side.



EVS allows the model to be gridded using several different techniques including convex hull (the default method) and rectilinear gridding. The convex hull of a set of points in two-dimensional space is the smallest convex area containing the set. In the x-y plane, the convex hull can be visualized as the shape assumed by a rubber band that has been stretched around the set and released to conform as closely as possible to it. EVS grids convex hull regions with quadrilaterals. Smoothing techniques are used to create a grid that has reasonably equal area cells. In rectilinear (a.k.a. uniform) gridding, the grid axes are parallel to the coordinate axes and the cells are always rectangular in cross-section. The positions of all the nodes can be computed knowing only the coordinate extents of the grid (minimum and maximum x, y, and z). In both convex hull and rectilinear gridding, adaptive gridding was used. Adaptive gridding is the

localized refinement of a grid to provide higher resolution in the areas or volumes surrounding measured sample data.

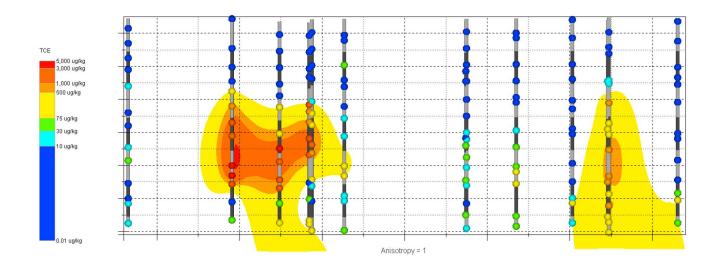
### **C.1.3 RESULTS**

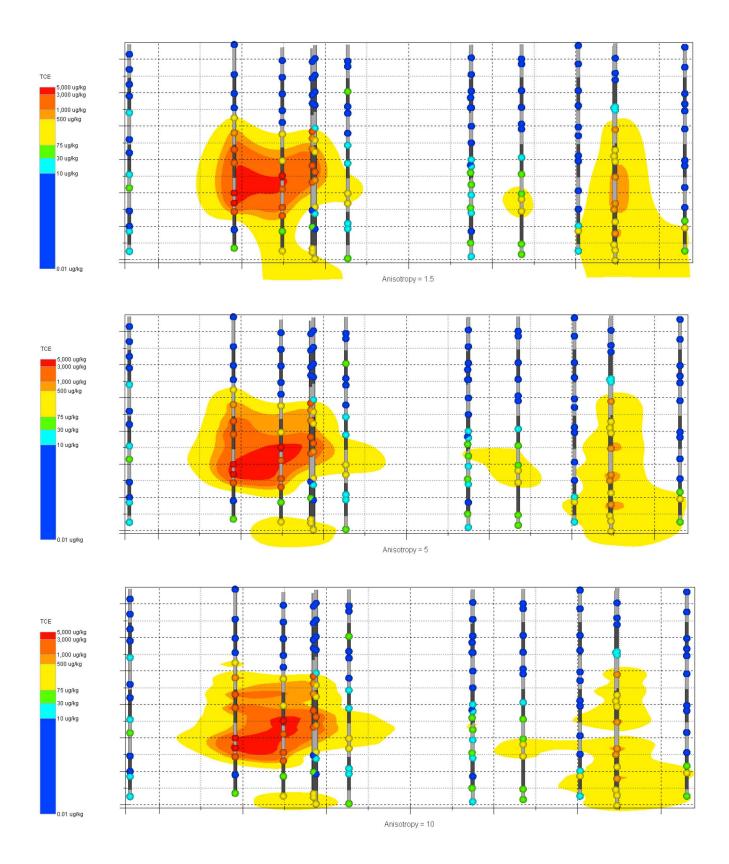
The table below provides the results of the volume estimates in gallons (gal) using the different datasets. The blue shading highlights the 50% nominal source volume estimate and the green shading highlights the results using an anisotropy value of one, which has previously been reported.

		Aniso	tropy	
Confidence Level	1	1.5	5	10
90% - Max Plume	1.5	2.2	3	2.8
80% - Max Plume	1	1.5	2.1	1.9
70% - Max Plume	0.8	1.1	1.6	1.5
60% - Max Plume	0.6	0.9	1.2	1.2
50% - Nominal	0.5	0.7	1	0.9
60% - Min Plume	0.4	0.6	0.8	0.8
70% - Min Plume	0.3	0.4	0.6	0.6
80% - Min Plume	0.2	0.3	0.5	0.5
90% - Min Plume	0.2	0.2	0.3	0.3
Average	0.65	0.94	1.61	2.05

#### Estimated Volume of TCE (gal) above 75 ug/kg in SWMU 211-A Soils

The effects of anisotropy on the model can be visualized with the following cross-sections. As shown below, the higher the anisotropy is set, the more connection is seen between horizontal points and the less connection between vertical points.





#### **C.1.4 CONCLUSIONS**

The volume of TCE in soil is sensitive to the anisotropy used to interpolate the data as well as the statistical confidence bounds placed on the interpolation. A range of TCE volumes, from 0.2 to 2.2 gal, has been estimated by using kriging using various anisotropies and confidence levels. These volumes estimates do not vary by more than one order of magnitude from the nominal estimate under isotropic conditions of 0.7 gal. Given these sensitivity analyses, the 0.7 gal value represents a reasonable nominal value based upon the review of the data, interpolation results, and professional judgment.

# C.2. SWMU 211-B TCE VOLUME ESTIMATE AND SENSITIVITY ANALYSIS OF ANISOTROPY, MEASURES OF STATISTICAL CONFIDENCE USING HISTORIC (1998 AND 2004) UPPER CONTINENTAL RECHARGE SYSTEM (UCRS) SOIL INVESTIGATION AND 2012 REMEDIAL DESIGN SUPPORT INVESTIGATION (RDSI) DATASETS

### C.2.1 PURPOSE

Utilizing the soil sampling data results provided by LATA Kentucky, Geosyntec has developed estimates of the mass of TCE in soils above the RGA at SWMU 211-B, using C Tech's EVS. Provided soil sampling data was collected during evaluation of the UCRS (1998 and 2004) and RDSI (2012) sampling from October 2012. The purpose of this calculation package is to evaluate the sensitivity of TCE mass estimates when interpolating the data using a kriging algorithm by varying the anisotropy of the model and evaluating the statistical confidence of the interpolation.

### C.2.2 METHODS

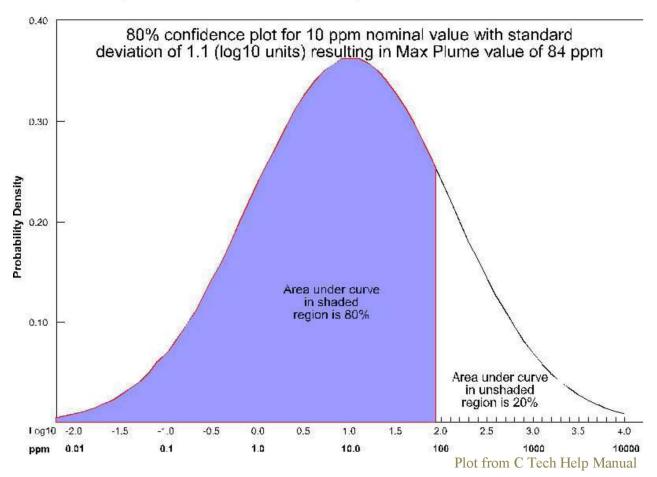
Soil sampling results were interpolated in EVS in order to estimate the volume of TCE in soils. A sensitivity analysis was performed to evaluate the volume of TCE under several different anisotropy levels: 1, 1.5, 5, and 10. EVS allows for further evaluation of the statistical confidence of the interpolation by providing results at differing user-defined confidence levels. Data were evaluated at 50, 60, 70, 80, and 90% confidence intervals, the results of which are provided in the calculation packages in Appendix C. A site-specific soil density of 1.4 gm/cc was used to calculate TCE mass and volume.

Anisotropy allows the model to consider the effects of anisotropy in the conductivity of soil matrices to fluid flow. In most cases, geologic materials are deposited with platy clay minerals oriented horizontally; thus, flow of water in both the saturated and unsaturated zone can be slower in the vertical direction than in the horizontal direction. Ore deposition also can occur along horizontal or vertical fault or fracture systems. Chemical constituents being transported with flowing fluids, therefore, may show a larger degree of spreading in one or the other direction. The Horiz./Vert. Anisotropy Ratio allows the kriging algorithm to specify a factor to be used to apply biased weighting on data points in horizontal and vertical directions away from a given model node. The default value for fluid flow is 10, which allows data points in a horizontal direction away from a model node to influence the kriged value at that node by a factor of 10 than data points an equal distance away in a vertical direction. A value of 10 typically would be appropriate for dissolved-phase concentrations in an aquifer that is either high-velocity or anisotropic. When the property being modeled is not related to fluid flow or other processes that might be affected by

matrix anisotropy, then the recommended value is 1 (i.e., isotropic). Based on observations of data from soil sampling to date in SWMU 211-B, despite the fluid based nature of the release, it is expected that transport is vertically controlled more than horizontally controlled. Therefore the use of a lower anisotropy value is appropriate. Based upon the shape and connectedness of the plume to various sample points, an anisotropy constant of 1.5 was selected.

EVS can be used to determine the Min and Max Plume, or in this specific case, source area, using a Min-Max algorithm. The Min Plume calculates the minimum estimated size of the source area at a user-specified confidence level. Conversely, the Max Plume calculates the maximum estimated size of the source area at a user-specified confidence level. To determine the confidence level of the interpolation, EVS first calculates the nominal value and associated standard deviation at every node in the model. For the case of Max Plume and 80% confidence, at each node, a maximum value is determined such that 80% of the time, the actual values will fall below the maximum value (for that nominal concentration and standard deviation). This process is shown below as an example directly from the C Tech Help Manual for the case of an assumed nominal value of 10 ppm with a standard deviation of 1.1 (log units). For this case, the maximum value at that node would be approximately 84 ppm. This process is repeated for every node in the model.

For the plot shown below (from the C Tech Help Manual), the entire left portion of the bell curve is shaded. If assessing the minimum value, it would be the right side.



EVS allows the model to be gridded using several different techniques including convex hull (the default method) and rectilinear gridding. The convex hull of a set of points in two-dimensional space is the

smallest convex area containing the set. In the x-y plane, the convex hull can be visualized as the shape assumed by a rubber band that has been stretched around the set and released to conform as closely as possible to it. EVS grids convex hull regions with quadrilaterals. Smoothing techniques are used to create a grid that has reasonably equal area cells. In rectilinear (a.k.a. uniform) gridding, the grid axes are parallel to the coordinate axes and the cells are always rectangular in cross-section. The positions of all the nodes can be computed knowing only the coordinate extents of the grid (minimum and maximum x, y, and z). In both convex hull and rectilinear gridding, adaptive gridding was used. Adaptive gridding is the localized refinement of a grid to provide higher resolution in the areas or volumes surrounding measured sample data.

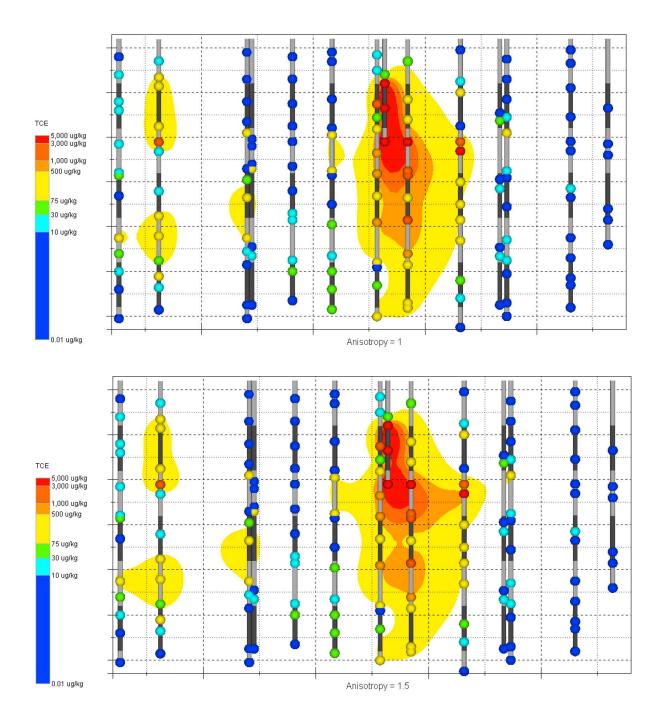
### C.2.3 RESULTS

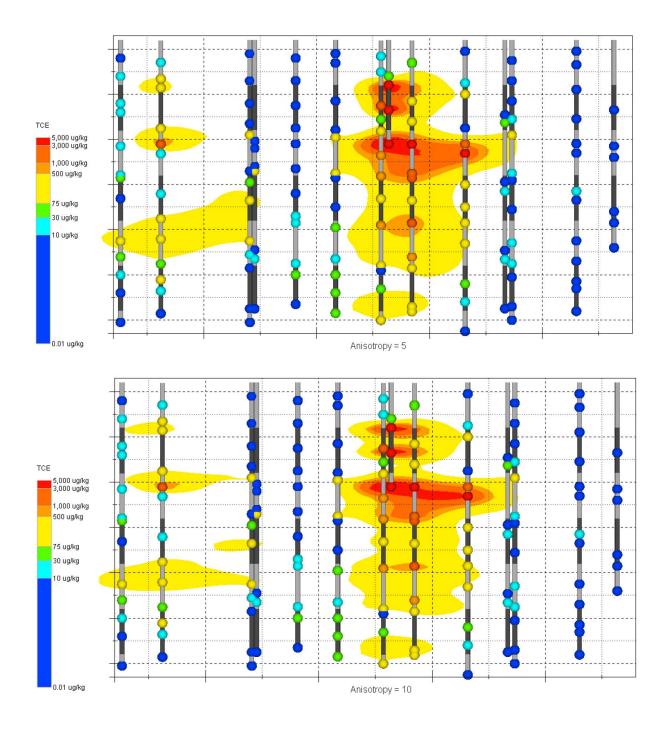
The table below provides the results of the volume estimates in gallons (gal) using the different datasets. The blue shading highlights the 50% nominal source volume estimate and the green shading highlights the results using an anisotropy value of one, which has previously been reported.

		Aniso	tropy	
Confidence Level	1	1.5	5	10
90% - Max Plume	0.8	0.8	1.1	1
80% - Max Plume	0.5	0.6	0.8	0.7
70% - Max Plume	0.4	0.4	0.6	0.6
60% - Max Plume	0.3	0.3	0.5	0.5
50% - Nominal	0.3	0.3	0.4	0.4
60% - Min Plume	0.2	0.2	0.3	0.3
70% - Min Plume	0.2	0.2	0.3	0.3
80% - Min Plume	0.1	0.1	0.2	0.2
90% - Min Plume	0.1	0.1	0.1	0.2
Average	0.39	0.45	0.93	1.42

#### Estimated Volume of TCE (gal) above 75 ug/kg in SWMU 211-B Soils

The effects of anisotropy on the model can be visualized with the following cross-sections. As shown below, the higher the anisotropy is set, the more connection is seen between horizontal points and the less connection between vertical points.





### C.2.4 CONCLUSIONS

The volume of TCE in soil is sensitive to the anisotropy used to interpolate the data as well as the statistical confidence bounds placed on the interpolation. A range of TCE volumes, from 0.1 to 1.1 gal, has been estimated by using kriging using various anisotropies and confidence levels. These volumes estimates do not vary by more than an order of magnitude from the nominal estimate under isotropic conditions of 0.3 gal. Given these sensitivity analyses, the 0.3 gal value represents a reasonable nominal value based upon the review of the data, interpolation results, and professional judgment.

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**APPENDIX D** 

SOIL LITHOLOGY LOGS

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# Plant North -2023.211, Plant East -5059.551

8/29/2012

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	2.7	Gravel with Silt, 10YR6/4 (light yellowish brown), loose, and dry. Gravel is subangular limestone, 0.2- to 0.8-inch diameter (dense gravel aggregate/DGA)	Fill
2.7	3.5	Silt, 10YR8/2 (very pale brown) with some 10YR7/8 (yellow) mottling, moderately hard, nonplastic, and dry	
3.5	14.4	Silt, 10YR7/3 (very pale brown), with some 10YR7/6 (yellow) mottling, soft, moderately plastic, and moist	11111
14.4	16.1	Silt, 10YR7/4 (very pale brown), moderately soft, nonplastic, and moist	HU1
16.1	19.5	Silt, 10YR7/4 (very pale brown), with 10YR8/1 (white) mottling, soft, slightly plastic, and moist. Little gravel (rounded chert with iron patina, 0.3-inch diameter) beginning at 17.8 ft	
19.5	20.0	Silty Gravel with little Clay, 10YR6/6 (brownish vallow) dance and moiet. Gravel is subangular to	
20.0	22.5	No Recovery	
22.5	23.2	Gravelly Silt, 10YR8/1 (white), moderately hard, nonplastic, and moist. Gravel is subrounded chert with and without iron patina, 0.2- to 0.4-inch diameter	
23.2	24.9	Sand, 10YR6/6 (brownish yellow), loose, and moist. Sand is fine to medium, rounded, quartz grains	
24.9	26.0	Silty Gravel, 10YR7/3 (very pale brown), dense, and moist. Gravel is subrounded chert with and without iron patina, 0.2- to 1.0-inch diameter	
26.0	29.5	Silt with little Gravel, 10YR7/1 (light gray) with frequent 10YR7/4 (very pale brown) staining, moderately soft, moderately plastic, and moist. Gravel is rounded chert without iron patina, 0.3-iinch diameter	HU2
29.5	30.1	Silt, 10YR7/4 (very pale brown), moderately hard, moderately plastic, and moist	
30.1	31.0	Silt, 10YR7/1 (light gray) with 10YR7/6 (yellow) mottling, moderately hard, slightly plastic, and moist	
31.0	32.2	Silty Sand, 10YR7/4 (very pale brown), lightly consolidated, and moist. Sand is very fine quartz grains	
32.2	33.5	Silt with Gravel, 10YR7/6 (yellow), moderately hard, slightly plastic, and moist	
33.5	34.7	Silt, 10YR6/4 (light yellowish brown), soft, slightly plastic, and moist	

211-A-001

# Plant North -2023.211, Plant East -5059.551

8/29/2012

	1	Plant North -2023.211, Plant East -3039.331	8/29/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
34.7	35.5	Sand with Gravel, 10YR8/2 (very pale brown) with some 10YR6/4 (light yellowish brown) mottling, loose, and moist. Sand is very fine quartz grains. Gravel is rounded to subrounded chert without iron patina, 0.2- inch diameter	
35.5	36.1	Silt, 10YR8/1 (white), soft, moderately plastic, and moist	
36.1		Silt with Sand, 7.5YR6/6 (reddish yellow) with some 7.5YR8/1 (white) mottling, moderately soft, slightly plastic, and moist. Sand is very fine quartz grains	
37.3	37.9	Silty Clay, 7.5YR7/1 (light gray), moderately hard, plastic, and moist	
37.9	44.0	Silt, 10YR7/4 (very pale brown) mottled with 10YR8/2 (very pale brown), moderately soft, slightly plastic, and moist	
44.0	50.0	Clayey Silt, 7.5YR8/1 (white) with 7.5YR7/6 (reddish yellow) mottling, moderately hard, plastic, and moist	
50.0	51.8	Silt, 7.5YR7/1 (light gray) with little 7.5YR7/6 (reddish yellow) mottling, soft to very soft, moderately plastic, and wet	HU3
51.8	52.2	Silt with Gravel, 7.5YR7/1 (light gray) with little 7.5YR7/6 (reddish yellow) mottling, soft to very soft, moderately plastic, and wet. Gravel is rounded chert without iron patina, 0.1- to 0.2-inch diameter	
52.2	52.6	quartz grains	
52.6	57.8	plastic, and moist	
57.8	59.7	Sand, 10YR8/1 (white) with some 10YR3/1 (very dark gray) staining (manganese?), loose, and very moist. Sand is fine quartz grains	HU4
59.7	60.0	Sandy Gravel, 10YR6/6 (brownish yellow), loose, and moist Gravel is chert with iron pating subrounded to	HU5

Plant North -2023.779, Plant East -5031.236

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	1.8	Silt with Gravel, 10YR7/2 (light gray), moderately hard, nonplastic, and dry. Gravel is subangular limestone, 0.3- to 1.0-inch diameter (dense gravel aggregate/DGA)	FILL
1.8	3.8	Silt, 10YR8/1 (white) with little 10YR8/8 (yellow) mottling, moderately hard, nonplastic, and dry	
3.8	13.9	Silt, 10YR7/2 (light gray) with variable mottling/staining by 10YR6/6 (brownish yellow), soft, nonplastic, and moist	
13.9	16.2	Silt, 10YR7/6 (yellow), moderately hard, nonplastic, and moist	
16.2	17.4	Silt, 10YR7/1 (light gray), very soft, nonplastic, and moist	
17.4	20.0	Silt with trace Gravel, 10YR7/4 (very pale brown) mottled with 10YR7/1 (light gray), moderately soft, slightly plastic, and moist. Gravel is subrounded to subangular chert with iron patina, 0.3-inch diameter	HU1
20.0	20.5	Clay, 10YR6/2 (light brownish gray), moderately hard, plastic, and moist	
20.5	21.7	Sandy Silt, 10YR6/6 (brownish yellow), with blebs of clay, 10YR6/2 (light brownish gray); moderately hard, slightly plastic, and moist. Sand is very fine quartz grains.	
21.7	21.9	Gravel, 10YR6/6 (brownish yellow). Gravel is rounded to subrounded chert with iron patina, 0.3- to 0.8-inch diameter	
21.9	22.7	Silty Clay with some Gravel, 10YR7/2 (light gray), moderately hard, plastic, and moist. Gravel is rounded chert with iron patina, approximately 0.5-inch diameter	
22.7	25.0	Silty Sandy Gravel, 7.5YR6/6 (reddish yellow), hard, and moist. Gravel is subrounded to subangular chert with iron patina, 0.3- to 0.6-inch diameter. Sand is very fine quartz grains	
25.0	26.8	Gravelly Sand, 10YR5/6 (yellowish brown), loose, and moist. Sand is fine quartz grains. Gravel is rounded chert with iron patina, 0.2- to 0.3-inch diameter	HU2
26.8	30.7	Silt, 10YR7/1 (light gray) with 10YR7/6 (yellow) mottling and micro-laminations, moderately plastic, soft, and moist	
30.7	31.3	Silt with some Gravel, 10YR7/1 (light gray) with 10YR7/6 (yellow) mottling and micro-laminations, moderately plastic, soft, and moist. Gravel is subrounded chert with iron patina, 4 mm- to 0.7-inch diameter	
31.3	31.8	Silt, 10YR8/4 (very pale brown) GRADING DOWN to 10YR8/1 (white), soft, slightly plastic, and moist	

Plant North -2023.779, Plant East -5031.236

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
31.8	32.5	Sand with Gravel, 7.5YR7/6 (reddish yellow), lightly consolidated, and moist. Sand is fine quartz grains. Gravel is rounded chert with iron patina, 0.2- to 1.0- inch diameter	
32.5	35.0	No recovery	NO RECOVERY
35.0	39.0	Silty Clay, 7.5YR8/1 (white) with abundant 7.5YR7/6 (reddish yellow) mottling and staining GRADING DOWN to little mottling and staining, moderately soft, plastic, and moist	
39.0	40.5	Silt, 10YR8/2 (very pale brown) mottled with 10YR6/2 (light yellowish brown) and 10YR7/6 (yellow), soft, slightly plastic, and moist	
40.5	43.3	Interlensing Silty Clay and Silt, 10YR8/1 (white) with heavy mottling by 10YR6/6 (brownish yellow) and some 2.5YR7/8 (light red), moderately soft, moderately plastic, and moist	
43.3	49.6	Silty Clay, 7.5YR7/6 (reddish yellow) mottled with 7 5YR8/1 (white) GP ADING DOWN to 7 5YR8/1	HU3
49.6	52.9	Silt with little Clay and Sand, 7.5YR8/1 (white) with 7.5YR7/6 (reddish yellow) mottling, soft, slightly plastic, and moist. Sand is very fine quartz grains	
52.9	56.1	Silty Clay, 7.5YR8/1 (white) with abundant small mottles of 7.5YR7/6 (reddish yellow), moderately hard, moderately plastic, and moist	
56.1	58.2	Silt, 7.5YR6/6 (reddish yellow), moderately hard, slightly plastic, and moist	
58.2	60.0	Sand with some blebs of Silt, 10YR8/1 (white) with some 10YR7/6 (yellow) mottling and some small blebs of 10YR3/1 (very dark gray) (manganese?), lightly consolidated, and very moist. Sand is very fine quartz grains	
60.0	60.4	Sand, 10YR8/1 (white) with few 10YR7/6 (yellow) laminations, lightly consolidated, and wet. Sand is fine quartz grains	HU4
60.4	60.9	Gravelly Sand, 10YR8/2 (very pale brown), loose, and wet. Sand distribution is bimodal: 70% fine quartz grains and 30% coarse to very coarse, subrounded to rounded, chert grains (with and without iron patina). Gravel is rounded to subrounded chert with iron patina, 4 mm- to 0.8-inch diameter	
60.9	62.5	Sandy Gravel, 10YR6/4 (light yellowish brown), loose, and wet. Gravel is rounded to subrounded chert with iron patina, 0.2- to 0.8-inch diameter. Sand distribution is bimodal, 65% fine to medium quartz grains and 35% coarse, subangular, chert grains	HU5

# Plant North -2022.639, Plant East -4994.843

9/12/2012

Start Depth	End Depth	Lithology	Hydrogeologic Unit
(ft bgs)	(ft bgs)	Liniology	inyurogeologic Ullit
		Silt, 10YR6/1 (gray), loose, and dry. Humic material	
0.0	0.2	and root zone	
		Gravelly Silt, 10YR7/1 (light gray), loose (powder),	
0.2	0.5	nonplastic, and dry. Gravel is subangular to rounded	Fill
		chert, 0.2- to 1.0-inch diameter	
0.5	2.2	Silt with some Gravel, 10YR7/4 (very pale brown),	
		moderately hard, nonplastic, and slightly moist Silt, 10YR8/1 (white) with little 10YR7/6 (yellow)	
2.2	3.2	mottling, hard, nonplastic, and slightly moist	
		Silt, 10YR8/2 (very pale brown) with variable mottling	
3.2	16.4	by 10YR6/6 (brownish yellow), soft, nonplastic, and	111.1
		moist	HU1
		Slightly Clayey Silt, 10YR6/4 (light yellowish brown)	
16.4	20.1	with 10YR6/1 (gray) mottling, moderately hard,	
		nonplastic, and slightly moist	
		Silty Sand with Gravel, 7.5YR6/6 (reddish yellow), dense, and moist. Sand is fine quartz grains. Gravel is	
20.1	24.0	subangular to subrounded chert with light iron patina, 4	
		mm- to 0.4-inch diameter	
24.0	25.0	Silt with little Gravel, 10YR8/2 (very pale brown), soft,	
24.0	25.0	slightly plastic, and moist. Gravel is subrounded chert without iron patina, 0.2- to 0.4-inch diameter	
		-	
		Sand with some Gravel, 10YR7/4 (very pale brown),	
25.0	25.5	lightly consolidated, and moist. Sand is 70% fine quartz grains and 30% coarse, rounded, chert grains.	
25.0	25.5	Gravel is subangular chert with iron patina, 0.4-inch	
		diameter	HU2
		Sand, 5YR7/6 (reddish yellow), lightly consolidated,	
25.5	26.3	and moist. Sand is very fine quartz grains	
<b>├</b> ─── <b>↓</b>			
26.3	28.2	Silty Sand with Gravel as 20.1 to 24.0 ft	
20.2	20.0	Silty Sand, 10YR8/1 (white) mottled with 10YR7/6	
28.2	30.0	(yellow), firm/moderately soft, nonplastic, and moist.	
├		Sand is very fine quartz grains Silty Gravelly Sand, 7.5YR6/5 (reddish yellow), firm	
		to soft, nonplastic, and moist to very moist. Sand size	
30.0	36.1	ranges from fine to coarse grains. Gravel is subangular	
		chert, 0.5- to 1.2-inch diameter	
		Sandy Silt, 7.5YR6/8 (reddish yellow) with some	
36.1	39.2	mottling by 7.5YR6/1 (gray), soft to very soft, plastic,	
├		and very moist Silt, 7.5YR7/3 (pink) with 7.5YR8/1 (white) banding,	
39.2	40.0	stiff to firm, and slightly moist	
		Clay with little Silt, 7.5YR6/8 (reddish yellow) mottled	
40.0	40.9	with 10YR7/1 (light gray), very stiff to stiff,	
		nonplastic, and slightly moist	

211-A-003

#### Plant North -2022.639, Plant East -4994.843

9/12/2012

Г		1 Iant North 2022.039, 1 Iant East 4994.043	
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
40.9	42.9	Sandy Silt, 7.5YR7/6 (reddish brown) with 10YR7/1 (gray) and 7.5YR5/8 (strong brown) mottling, stiff to firm, and slightly moist	
42.9	45.0	Sandy Silt, 7.5YR6/8 (reddish yellow) with some 10YR7/1 (light gray) mottling, very firm to firm, and slightly moist. Sand is very fine quartz grains	
45.0	48.4	Clayey Sandy Silt, 7.5YR7/8 (reddish yellow) with slight mottling by 10YR7/1 (light gray) in sections and some 7.5YR5/8 (strong brown) speckling throughout, very firm, nonplastic, and slightly moist	
48.4	49.8	Clayey Silt with very little Sand, 10YR7/1 (light gray) with some 7.5YR6/8 (reddish yellow) mottling, firm, and slightly moist. Sand is very fine quartz grains	HU3
49.8	51.9	Sand is very fine quartz grains	
51.9	52.5	Silty Sand, 10YR7/1 (light gray), firm to very firm, and slightly moist. Sand is mostly very fine quartz grains but with trace of coarse, white, chert grains	
52.5	54.0	very fine quartz grains	
54.0	55.0	Sandy Silty Clay, 10YR7/1 (light gray) mottled with 7.5YR6/8 (reddish yellow), firm to stiff, and slightly moist	
55.0	55.2	Sand, 7.5YR6/8 (reddish yellow), slightly loose, and moist. Sand is very fine to fine quartz grains	
55.2	58.2	Clay, 10YR8/1 (white) mottled with 7.5YR5/6 (strong brown), stiff to very stiff, and slightly moist	
58.2	59.7	Silty Sand, 7.5YR6/8 (reddish yellow), firm, and moist. Sand is fine quartz grains	
59.7	61.0	Sand, 10YR8/1 (white), loose, and wet/saturated	
61.0	61.3	Sand with Gravel 10VR8/1 (white) loose and	
61.3	62.5	Gravelly Silty Sand, 7.5YR6/8 (reddish yellow), very firm, and moist. Gravel is subangular to subrounded chert with iron patina, 0.5- to 1.2-inch diameter	HU4

# Plant North -2048.082, Plant East -5212.811

I			
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	3.6	Gravelly Sand, 2.5YR5/6 (red), dense, and moist. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 0.3- to 0.5-inch diameter	Fill
3.6	7.5	Silt, 10YR7/1 (light gray) with some 10YR7/6 (yellow) mottling, soft, nonplastic, and moist	
7.5	10.0	Permeameter sample - no description	
10.0	12.5	Silt as 3.6 to 7.5 ft	
12.5	13.5	Sand, 10YR8/4 (very pale brown), dense, and moist. Sand is very fine quartz grains	
13.5	14.7	Silt, 10YR7/4 (very pale brown), soft, slightly plastic, and moist	
14.7	15.0	Silt with little Gravel and little Clay, 10YR7/2 (light gray) mottled with 7.5YR6/6 (reddish yellow), moderately hard, slightly to moderately plastic, and moist. Gravel is subangular chert without iron patina, 0.3-inch diameter	HU1
15.0	15.5	Silt, 10YR7/2 (light gray), very soft, nonplastic, and moist. Slough	
15.5	17.2	Silt with little Clay and little Gravel, 7.5YR7/2 (pinkish gray) with 7.5YR7/6 (reddish yellow) staining, moderately hard, moderately plastic, and moist. Gravel is subrounded to subangular chert without iron patina, 0.3- to 1.0-inch diameter	
17.2	17.5	Sand with Gravel, 7.5YR7/4 (pink), firm, and moist. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 0.4- to 0.6-inch diameter	
17.5	20.0	Permeameter sample - no description	
20.0		Silt with little Clay and little Gravel as 15.5 to 17.2 ft	
21.1	23.8	Sand with Gravel, 7.5YR7/4 (pink), dense, and moist. Sand is fine quartz grains. Gravel is subangular to subrounded chert without(?) iron patina, 0.3- to 0.5-inch diameter	
23.8	24.2	Sand, 7.5YR7/4 (pink), firm, and moist. Sand is fine to medium quartz grains	
24.2	24.6	Silt with some Gravel, 10YR7/1 (light gray) with 7.5YR7/6 (reddish yellow) staining, soft, plastic, and moist. Gravel is subrounded chert without(?) iron patina, 1.0-inch diameter	
24.6	26.0	Sand, 10YR8/2 (very pale brown) GRADING DOWN to 10YR8/4 (very pale brown), dense, and moist. Sand is fine quartz grains	
26.0	26.5	Gravelly Sand with Silt, 10YR7/6 (yellow), dense, and moist. Sand is fine quartz grains. Gravel is subrounded chert without iron patina, 0.3- to 0.6-inch diameter	HU2
26.5	28.5	Silt with Sand, 10YR7/4 (very pale brown) mottled with 10YR8/1 (white), soft, nonplastic, and moist. Sand is fine quartz grains	

# Plant North -2048.082, Plant East -5212.811

di i		I I	
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
28.5	30.0	Sand with Gravel, 10YR8/3 (very pale brown), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert without iron patina, 4 mm- to 0.6-inch diameter	
30.0	31.9	Sand with Gravel and some Silt, 7.5YR6/6 (reddish yellow). Sand is 80% fine to medium quartz grains and 20% coarse, subrounded, chert grains. Gravel is subrounded to subangular chert without (?) iron patina, 4 mm- to 0.5-inch diameter	
31.9	32.7	Silt with Clay, 7.5YR6/6 (reddish yellow), moderately soft, plastic, and moist	
32.7	42.4	Silt, 7.5YR6/6 (reddish yellow) GRADING DOWN to 10YR7/6 (yellow) and then to 10YR8/3 (very pale brown) (over 41.0 to 42.4 ft), soft, slightly plastic, and moist	
42.4	50.0	Silt with little Clay, 7.5YR8/4 (pink) with some 7.5YR7/6 (reddish yellow) mottling, moderately soft, plastic, and moist	
50.0	52.1	Silt with Sand, 10YR8/1 (white) with 10YR8/6 (yellow) laminations, soft, nonplastic, and moist. Sand is fine quartz grains	
52.1	54.6	Silt with Sand, 5YR8/2 (pinkish white), soft, nonplastic, and moist. Sand is very fine quartz grains	HU3
54.6	55.4	Sand, 10YR8/3 (very pale brown), firm, and moist. Sand is very fine to fine quartz grains	
55.4	56.8	Silt with Sand, 10YR7/6 (yellow) mottled with 10YR8/1 (white), soft, nonplastic, and moist. Sand is fine quartz grains	
56.8	57.5	Silt with some Clay, 7.5YR7/3 (pink) mottled with 7.5YR8/1 (white), moderately hard, slightly plastic, and moist	
57.5	61.0	Silt with Sand, 7.5YR8/1 (white) mottled with 5YR6/6 (reddish yellow), soft, nonplastic, and moist. Sand is fine quartz grains	
61.0	64.6	Sand, 10YR8/3 (very pale brown), loose, and wet. Sand is fine quartz grains	
64.6	65.0	Sand with Gravel, 10YR8/2 (very pale brown), firm, and moist. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 0.3- to 1.0-inch diameter	HU4

# Plant North -2047.983, Plant East -5179.833

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	0.3	Root zone and humic-rich soil, 10YR4/1 (dark gray)	
0.3	0.8	Silty Gravel (dense gravel aggregate/DGA), 10YR7/1 (light gray), loose, and moist. Gravel is subangular to subrounded limestone, 4-mm to 0.3-inch diameter	Fill
0.8	1.4	Silt with Gravel (fill), 10YR7/3 (very pale brown), soft, nonplastic, and moist. Gravel is rounded chert with iron patina, 0.7- to 1.0-inch diameter	
1.4	2.5	Silt with Gravel (fill) as 0.8 to 1.4 ft but interbedded 10YR5/1 (gray) and 10YR8/1 (white)	
2.5	15.2	Silt, 10YR8/2 (very pale brown) with 10YR6/6 (brownish yellow) mottling and few 10YR4/1 (dark gray) laminations, soft, nonplastic, and moist	HU1
15.2	16.5	Sand, 7.5YR7/6 (reddish yellow), lightly consolidated, and moist. Sand is fine quartz grains	
16.5	18.7	Sand with some Gravel, 7.5YR7/6 (reddish yellow), lightly consolidated, and moist. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 0.5 to 0.8-inch diameter	
18.7	21.5	Slightly Clayey Silt, 10YR7/1 (light gray) with some 10YR7/6 (yellow) mottling, moderately hard, slightly plastic, and moist	
21.5	23.5	Gravel with Silt, 10YR7/1 (light gray) GRADING DOWN to 10YR5/6 (yellowish brown), hard, and moist. Gravel is subrounded to subangular chert with iron patina, 0.3- to 0.8-inch diameter	HU2
23.5	27.5	Sand with Gravel to Gravelly Sand, 10YR7/4 (very pale brown) with some 10YR8/1 (white) laminations, lightly consolidated and moist. Sand is fine quartz grains. Gravel is subrounded to rounded chert with iron patina, 0.3- to 1.0-inch diameter	
27.5	35.2	Gravelly Sand, 10YR8/3 (very pale brown) mottled with 10YR8/1 (white), lightly consolidated, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert with iron patina, 0.2- to 0.8-inch diameter	
35.2	39.6	Slightly Clayey Silt, 7.5YR8/1 (white) mottled with 7.5YR7/4 (pink), soft, slightly-to-moderately plastic, and moist	
39.6	42.5	Silty Sand, 7.5YR8/1 (white) heavily mottled with 7.5YR7/6 (reddish yellow), lightly consolidated/soft, nonplastic, and moist. Sand is very fine quartz grains	
42.5	48.4	Slightly Clayey Silt, 7.5YR7/6 (reddish yellow) with little 7.5YR8/1 (white) mottling, moderately soft, moderately plastic, and moist	

#### Plant North -2047.983, Plant East -5179.833

		Plant North -2047.985, Plant East -5179.855	9/4/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
48.4	49.9	Silt with Sand, 7.5YR8/1 (white) mottled with 7.5YR7/6 (reddish yellow), soft, slightly plastic, and moist	
49.9	52.3	Sandy Silt, 7.5YR7/6 (reddish yellow) mottled with 7.5YR8/1 (white), soft, nonplastic, and moist	
52.3	53.4	Sand with some Gravel, 7.5YR8/6 (reddish yellow), lightly consolidated, and moist. Sand is fine quartz grains. Gravel is subangular chert with iron patina, 0.6- inch diameter	
53.4	53.8	Sand, 10YR7/6 (yellow) GRADING DOWN to 10YR8/1 (white), loose and moist. Sand is predominately (70%) fine grained but includes (30%) coarse, rounded chert grains	HU3
53.8	54.3	Sandy Gravel with Silt, 10YR5/1 (gray) (stained with manganese?), loose, and very moist. Gravel is rounded chert with iron patina, 0.4- to 0.6-inch diameter. Sand is fine grained	
54.3	56.8	Sand with Gravel, 7.5YR8/2 (pinkish white) with 7.5YR7/6 (reddish yellow) laminations, lightly consolidated, and moist. Sand is fine quartz grains. Gravel is rounded to subangular chert with iron patina, 0.2- to 0.4-inch diameter	
56.8	58.5	Clay, 10YR8/2 (very pale brown) with 10YR7/6 (yellow) laminations GRADING DOWN to 2.5YR8/1 (white) with 2.5YR7/6 (light red) laminations, soft, plastic, and moist	
58.5	60.2	Silt with Sand, 2.5YR8/1 (white) with 2.5YR7/6 (light red) laminations GRADING DOWNWARD to 10YR8/1 (white), soft, very slightly plastic, and moist. Sand is very fine quartz grains	
60.2	61.6	Sand, 10YR8.1 (white) with 10YR7/6 (yellow) laminations, lightly consolidated, and very moist. Sand is fine quartz grains	HU4
61.6	62.0	Sandy Gravel, 10YR8/2 (very pale brown), loose, and very moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert with iron patina, 4-mm to 0.6-inch diameter	HU5

## Plant North -2043.464, Plant East -5148.427

9/26/2012

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	0.4	Silt, 10YR5/2 (grayish brown), soft (loose), nonplastic, and moist. Zone of roots and humic material	
0.4	1.7	Silt, 10YR6/3 (pale brown), soft, nonplastic, and moist. Note: some Gravel at 1.7 ft, subangular to subrounded chert with iron patina, 0.3- to 0.8-inch diameter	Fill
1.7	16.0	Silt, 10YR8/2 (very pale brown), mottled with 10YR7/6 (yellow), soft, nonplastic, and moist	
16.0	17.8	Silt, 10YR8/1 (white) with frequent thin interbeds of Sand, 10YR7/6 (yellow). Silt is soft, nonplastic, and moist. Sand is very fine quartz grains, lightly consolidated, and moist	HU1
17.8	18.9	Sand, 7.5YR7/6 (reddish yellow), lightly consolidated, and moist. Sand is very fine quartz grains	
18.9	19.8	Slightly Clayey Silt, 10YR7/3 (very pale brown) with little 10YR7/6 (yellow) mottling, soft, plastic, and moist	
19.8	21.3	Clayey Silt with some Gravel, 10YR7/2 (light gray), soft, plastic, and moist. Gravel is subrounded to rounded chert without iron patina, 0.3- to 0.5-inch diameter	
21.3	25.0	Silty Gravelly Sand, 7.5YR6/4 (light brown), dense, and moist. Sand consists of 70% fine quartz grains and 30% coarse to very coarse, subrounded, chert grains. Gravel is subangular to subrounded chert without iron patina, 0.3- to 0.4-inch diameter	HU2
25.0	30.0	Silt, 10YR8/2 (very pale brown) mottled with 10YR8/6 (yellow), soft, moderately plastic, and moist	
30.0	32.3	Silt with Sand, 10YR7/4 (very pale brown) mottled with 10YR8/1 (white), soft, slightly plastic, and moist. Sand is fine quartz grains	
32.3	33.6	Sand, 10YR8/2 (very pale brown), lightly consolidated, and moist. Sand is very fine quartz grains	
33.6	36.7	Silty Sand with Gravel, 10YR7/4 (very pale brown), dense, and moist. Sand consists of 80% fine quartz grains and 20% coarse, subrounded, chert grains. Gravel is subrounded chert without iron patina, 0.4- inch diameter	
36.7	38.0	Slightly Clavey Silt 7 5VR7/6 (reddish yellow) with	
38.0	41.0	Silt with Sand, 10YR8/2 (very pale brown), soft, nonplastic, and moist. Sand is very fine quartz grains	
41.0	48.0	Silt, 7.5YR7/6 (reddish yellow) mottled with 7.5YR8/1 (white), soft, plastic, and moist	

#### Plant North -2043.464, Plant East -5148.427

9/26/2012

		Flaint Norul -2045.404, Flaint East -5146.427	 9/20/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
48.0	49.0	Silt with Sand, 7.5YR7/6 (reddish yellow) mottled with 7.5YR8/1 (white), moderately soft, nonplastic, and moist. Sand is very fine quartz grains	
49.0	54.1	Sand, 7.5YR7/6 (reddish yellow) GRADING DOWN to 7.5YR8/1 (white), firm, and moist. Sand is very fine quartz grains	
54.1	55.3	Sand with Gravel, 10YR8/2 (very pale brown), loose, and moist. Sand is fine quartz grains. Gravel is rounded chert without iron patina, 0.3- to 0.4-inch diameter	HU3
55.3	55.5	Sand, 7.5YR7/6 (reddish yellow), firm, and moist. Sand is very fine quartz grains	
55.5	57.4	Clay, 7.5YR7/6 (reddish yellow) mottled with 7.5YR8/1 (white) GRADING DOWN to 7.5YR8/1 (white) with 7.5YR7/6 (reddish yellow) laminations, moderately hard, plastic, and moist	
57.4	59.4	Silt, 7.5YR8/1 (white) with 7.5YR7/6 (reddish yellow) laminations GRADING DOWN to massive 7.5YR8/1 (white), soft, moderately plastic, and moist	
59.4	61.2	fine quartz grains	
61.2	62.5	Gravelly Sand, 10YR8/4 (very pale brown), loose, and wet. Sand is fine to medium, rounded, quartz grains. Gravel is subrounded to subangular chert with iron patina, 0.3- to 0.7-inch diameter	HU4

## Plant North -2043.219, Plant East -5088.804

	<b>F</b> 7	1 Iant 1401ul 2045.21), 1 Iant Last 5000.004	5/20/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0		Sand with Gravel to Gravelly Sand, 2.5YR5/6 (red), dense, and moist. Sand is 90% fine quartz grains and 10% coarse, subrounded, chert grains. Gravel is subrounded chert with iron patina, 0.3- to 0.50inch diameter	Fill
2.7	13.1	Silt, 10YR7/1 (light gray) with some 10YR7/6 (yellow) mottling, soft, nonplastic, and moist	HU1
13.1	14.8	Interbedded Fine Sand, 7.5YR6/6 (reddish yellow), and Very Fine Sand, 7.5YR8/1 (white); firm, and moist	
14.8	17.0	Gravelly Sand, 7.5YR5/6 (strong brown), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert with iron patina, 4 mm- to 0.6-inch diameter	
17.0	17.7	Sand, 10YR7/6 (reddish yellow), dense, and moist. Sand is fine quartz grains	
17.7	21.3	Gravelly Sand as 14.8 to 17.0 ft	
21.3	21.7	Sand with Gravel, 10YR8/3 (very pale brown), firm, and moist. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 0.3- to 0.6-inch diameter	
21.7	22.3	Sand, 10YR8/3 (very pale brown), firm, and moist. Sand is fine quartz grains	
22.3	26.0	Silt, 10YR8/4 (very pale brown) mottled with 10YR8/1 (white), soft, plastic to moderately plastic, and moist	HU2
26.0	27.1	Sand with little Gravel, 10YR7/6 (yellow), firm, and moist. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 0.3- to 0.5-inch diameter	
27.1		with iron patina, 4 mm- to 0.4-inch diameter	
28.0	28.8	Sand, 10YR7/6 (yellow), firm, and moist. Sand is fine quartz grains	
28.8	30.0	Sandy Gravel, 10YR8/2 (very pale brown), dense, and moist. Gravel is subrounded to subangular chert with iron patina, 0.3- to 0.6-inch diameter	
30.0	30.8	Sandy Gravel as 28.8 to 30.0 ft but with Silt	
30.8	32.4	Sandy Gravel as 28.8 to 30.0 ft	
32.4		Silt with little Clay, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white) CPADING DOWN to 7.5YR8/2	
37.0	40.8	Silt with Clay 7 5YR7/3 (pink) mottled with 7 5YR8/1	
40.8	44.5	Silt with Clay as 37.0 to 40.8 ft but very soft	

### Plant North -2043.219, Plant East -5088.804

Start Depth	End Depth	Lithology	Hydrogeologic Unit
(ft bgs)	(ft bgs)		
41.7	43.0	Silt with Clay, 7.5YR7/3 (pink) mottled with 7.5YR8/1 (white) GRADING DOWN to 10YR8/2 (very pale brown), moderately hard, moderately plastic, and moist	
43.0	47.4	Silt with Clay, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white), moderately soft with blebs of moderately hard and blebs of soft, slightly to moderately plastic, and moist	HU3
47.4	49.5	Sand, 10YR7/4 (very pale brown), firm, and moist. Sand is fine quartz grains. Note: with subrounded chert gravel with iron patina, 0.3-inch diameter, at 49.2 to 49.5 ft	
49.5	55.1	Silt with Clay, 7.5YR6/6 (reddish yellow) mottled with 7.5YR8/1 (white), moderately hard, slightly plastic, and moist	
55.1	58.0	Silt with Sand, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white) GRADING DOWN to 10YR8/3 (very pale brown), soft, slightly plastic, and moist. Sand is fine quartz grains	
58.0	58.5	Sand, 10YR8/6 (yellow), firm, and moist. Sand is very fine quartz grains	
58.5	60.2	Sand, 10YR8/4 (very pale brown), firm, and moist. Sand is fine quartz grains	
60.2	60.5	Sand with Silt and Gravel, 10YR7/6 (yellow), firm, and moist. Sand is fine quartz grains. Gravel is rounded chert without iron patina, 0.3-inch diameter	HU4
60.5	62.0	Sand with a few Silt interbeds, 10YR8/2 (very pale brown), lightly consolidated to firm, and moist. Sand is fine quartz grains	
62.0		Sandy Gravel, 10YR7/4 (very pale brown), loose, and moist. Gravel is subrounded chert with iron patina, 0.3- inch diameter. Sand is fine quartz grains	HU5
62.1	62.5	Sand with a few Silt interbeds as 60.5 to 62.0 ft	

## Plant North -2043.587, Plant East -5058.315

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	0.2	Silt, 10YR5/1 (gray), soft, nonplastic, and moist. Zone of roots and humic material	
0.2	1.2	Silt, 10YR6/3 (pale brown), soft, nonplastic, and moist	
1.2	5.0	Silt, 10YR7/1 (light gray), hard, nonplastic, and dry	
5.0	5.9	Silt, 10YR7/1 (light gray), moderately hard, nonplastic, and moist	
5.9	17.5	Silt, 10YR8/2 (very pale brown) with 10YR6/6 (brownish yellow) mottling, soft, slightly plastic, and moist	HU1
17.5	20.2	Silt with some Clay and Gravel, 10YR6/6 (brownish yellow) with 10YR8/2 (very pale brown) mottling, moderately soft, plastic, and moist. Gravel consists of subangular to subrounded chert without iron patina, 0.3-to 0.8-inch diameter	
20.2	21.1	Silty Sand with Gravel, 7.5YR6/6 (reddish yellow), moderately dense, and moist. Sand consists of 70% fine quartz grains and 30% medium, rounded, quartz grains. Gravel consists of subangular to subrounded chert with iron patina, 0.3- to 0.4-inch diameter	
21.1	21.4	Silt, 10YR7/1 (light gray), moderately soft, nonplastic, and moist	
21.4	22.6	Silty Sand with some Gravel, 7.5YR5/6 (strong brown), moderately dense, and moist. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 0.3- to 0.4-inch diameter	
22.6	25.1	Silt, 10YR8/2 (very pale brown) with little 10YR7/6 (yellow) mottling, moderately hard, slightly plastic, and moist	HU2
25.1	25.5	Sandy Gravel, 7.5YR6/6 (reddish yellow)	
25.5	28.0	plastic, and moist. Gravel is rounded chert with iron patina, 1.0-inch diameter	
28.0	33.0	Silt with little Gravel, 10YR8/2 (very pale brown) with 10YR7/6 (yellow) mottling GRADING DOWN to 10YR7/3 (very pale brown), soft, nonplastic, and moist. Gravel is rounded chert without iron patina, 0.4- to 0.8-inch diameter	
33.0	35.0	Silty Sand with Gravel, 10YR6/6 (brownish yellow), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert with and without iron patina, 0.2 - to 0.6-inch diameter	
35.0	37.8	Slightly Clayey Silt, 7.5YR6/6 (reddish yellow) mottled with 7.5YR8/1 (white), soft, plastic, and moist	
37.8	42.0	Silt, 10YR7/2 (light gray) mottled with 10YR6/6 (yellow), soft, moderately plastic, and moist	

#### Plant North -2043.587, Plant East -5058.315

		Plant North -2045.587, Plant East -5058.515	9/20/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
42.0	42.2	Sand is very fine quartz grains	
42.2	51.6	Silty Clay, 7.5YR7/1 (light gray) mottled with 7.5YR6/6 (reddish yellow), moderately hard, moderately plastic, and moist	
51.6	52.7	Sand with little Gravel, 10YR8/1 (white) GRADING DOWN to 10YR8/4 (very pale brown), firm, and moist. Sand is very fine to fine quartz grains. Gravel is subrounded to subangular chert without iron patina, 0.4- to 0.5-inich diameter	HU3
52.7	53.5	Silty Clay as 42.2 to 51.6 ft	
53.5		Silty Sand, 10YR8/3 (very pale brown) GRADING DOWN to 7.5YR7/6 (reddish yellow), firm, and moist. Sand is fine quartz grains	
54.7	58.8	Silt with some Clay, 10YR7/6 (yellow) with mottling/laminations of 10YR8/1 (white), moderately hard, moderately plastic, and moist	
58.8	59.9	Silt, 10YR8/4 (very pale brown) with 10YR7/6 (yellow) laminations, soft, slightly plastic, and moist	
59.9	61.8	Sand is very fine quartz grains	HU4
61.8	62.3	Silt, 10YR8/2 (very pale brown), soft, moderately plastic, and moist	1104
62.3	62.5	Sandy Gravel, 5YR5/3 (brown), loose, and wet. Gravel is subrounded to rounded chert with iron patina, 0.4- to 1.0-inch diameter. Sand is fine quartz grains	HU5

Plant North -2045.429, Plant East -5030.721

9/13/2012 & 9/17/2012

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	1.2	Surface soil and pea gravel	Fill
1.2	5.0	yellow) mottling, and dry	
5.0	6.5	Silt, 10YR8/1 (white) with traces of 5YR6/8 (reddish yellow), and dry to slightly moist	
6.5	10.0	yellow), slightly plastic, and moist to very moist	
10.0	11.2	Silt, 10YR7/1 (light gray) mottled with 5YR6/8 (reddish yellow), firm, and moist	
11.2	12.0	moist	
12.0	12.6	moist	
12.6	13.7	Silt, 7.5YR7/8 (reddish yellow) mottled with 10YR7/1 (light gray), firm, and slightly moist	
13.7	14.5	(reddish yellow), firm, and slightly moist	HU1
14.5	15.0	Silt with little Sand, 10YR8/4 (very pale brown), firm, and dry to slightly moist. Sand is very fine quartz grains	
15.0	15.6	Sandy Silt, 10YR8/4 (very pale brown), firm, and slightly moist. Sand is very fine grained	
15.6	15.8	Sandy Silt, 2.5YR5/6 (red), and slightly moist. Sand ranges from fine to coarse grained and subangular	
15.8	16.5	Silt, 7.5YR6/8 (reddish yellow) mottled with 10YR7/1 (light gray), firm, and slightly moist	
16.5	17.4	Clayey Silt, 7.5YR6/8 (reddish yellow) with slight 7.5YR7/1 (light gray) mottling, firm to stiff, and slightly moist	
17.4	20.0	Clayey Silt, 10YR6/1 (gray) with some 2.5YR5/8 (red) mottling, firm, slightly plastic, and slightly moist	
20.0	20.6	Gravel with some Sand, 7.5YR6/6 (reddish yellow), loose, and moist. Gravel is subrounded to subangular chert with iron patina, 4-mm to 0.4-inch diameter	
20.6	21.2	Clay with Gravel, 7.5YR7/2 (pinkish gray), hard to moderately plastic, and slightly moist. Gravel is subrounded to rounded chert without iron patina, 0.4- inch diameter	
21.2	21.7	Sandy Gravel, 7.5YR6/6 (reddish yellow), loose, and moist. Gravel is subrounded to subangular chert with	
21.7	22.2	Silt 10VP7/1 (light gray) with 10VP7/4 (very pale	

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
22.2		Sandy Gravel, 10YR7/4 (very pale brown), loose and moist. Gravel is subrounded to subangular chert with iron patina, 4-mm to 0.7-inch diameter. Sand consists of 60% fine grains and 40 % coarse, rounded, chert grains	
23.7	26.4	Sand with Gravel, 7.5YR7/6 (reddish yellow), firm,	HU2
26.4	26.8	Sand with little Gravel, 10YR8/2 (very pale brown) stained with 10YR7/4 (reddish yellow), firm, and moist. Sand is fine quartz grains. Gravel is subrounded chert with light iron patina, 0.3 to 0.4-inch diameter	
26.8	32.2	Silt with Sand, 10YR8/1 (very pale brown) mottled with 10YR7/6 (yellow), moderately soft, nonplastic, and moist. Sand is fine quartz grains	
32.2	33.9	Sandy Gravel, 7.5YR6/6 (reddish yellow), dense, and moist. Gravel is subangular to subrounded chert without iron patina, 0.3- to 0.8-inch diameter. Sand is fine grained	
33.9	34.1	Sand, 10YR8/1 (white), lightly consolidated, and moist. Sand is fine quartz grains	
34.1	34.6	Sandy Gravel, 10YR8/2 (very pale brown), lightly consolidated, and moist. Gravel is subangular chert with light iron patina, 0.2- to 0.4-inch diameter. Sand is fine grained	
34.6	36.3	Clay, 7.5YR7/4 (pink) mottled with 7.5YR8/3 (pink), soft, very plastic, and moist	
36.3	40.0	Slightly Clayey Silt, 7.5YR7/6 (reddish yellow) with 7.5YR8/1 (white) mottling, soft, moderately plastic, and moist	
40.0	42.4	Silt with some Sand, 10YR8/2 (very pale brown) with frequent mottling by 10YR7/6 (yellow), moderately hard, nonplastic, and moist. Sand is fine quartz grains	
42.4	47.5	Slightly Clayey Silt, 7.5YR7/6 (reddish yellow) mottled with 7.5YR8/1 (white), moderately hard to hard, slightly plastic, and moist	
47.5	51.1	Silt, 7.5YR8/1 (white) with some 7.5YR7/6 (reddish yellow) mottling, soft, moderately plastic, and moist	11112
51.1	51.9	Silt as 47.5 to 51.1 with Gravel. Gravel is rounded chert without iron patina, 4-mm to 0.3-inch diameter	HU3
51.9	52.1	Gravelly Sand with "salt and pepper" texture - 10YR8/1 (white) and 10YR5/1 (gray) - loose, and moist. Sand consists of both fine grains and rounded coarse grains. Gravel is subrounded chert without iron patina, 4-mm to 0.5-inch diameter	

Plant North -2045.429, Plant East -5030.721 9/13/2012 & 9/17/2012

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
52.1	55.0	Silt, 10YR8/2 (very pale brown) with 10YR7/6 (yellow) mottling, moderately soft, nonplastic, and moist	
55.0	59.9	Silt with minor interbeds of Silt with Sand, 7.5YR8/1 (white) mottled with 7.5YR7/6 (reddish yellow), moderately hard, moderately plastic, and moist. Sand is fine quartz grains	
59.9	60.8	Sand, 10YR7/4 (very pale brown), firm, and moist. Sand is fine quartz grains	
60.8	61.2	Sand as 59.9 to 60.8 ft but with 7.5YR8/1 (white) and 7.5YR7/6 (reddish yellow) "beds"	HU4
61.2	62.2	Sand as 59.9 to 60.8 ft but colored 7.5YR8/4 (pink)	
62.2	62.5	Sandy Gravel, 10YR7/4 (very pale brown), loose, and moist. Gravel is subangular chert with iron patina, 4- mm to 0.8-inch diameter. Sand is fine grained	HU5

Plant North -2048.2, Plant East -4995.49

8/17/2012

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0		Soil - made land - limestone gravel	FILL
1.2		Silt, 10YR7/3 (very pale brown) with some mottling by 10YR8/1 (white), loose to slightly firm, and dry to slightly moist	
2.6	6.0	Silt, 10YR8/1 (white) with mottling by 10YR7/8 (yellow), slightly moist	
6.0	10.0	Silt, 10YR7/1 (light gray) mottled and speckled with 10YR6/8 (brownish yellow), firm GRADING DOWN to soft, and slightly moist to moist	
10.0	12.4	Silt, 10YR7/1 (light gray) mottled with 7.5YR6/8 (reddish yellow), soft, and slightly moist	
12.4	14.0	Silt, 10YR7/2 (light gray) speckled with 10YR7/8 (yellow), firm, and slightly moist	
14.0	15.0	Silt with little Clay, 10YR6/6 (brownish yellow) banded with 7.5YR6/6 (reddish yellow), firm, and slightly moist	HU1
15.0	16.4	Silt with very little Sand, 10YR7/3 (very pale brown), soft to firm, and moist. Sand is very fine quartz grains	
16.4	18.0	Silt with little Clay, 10YR7/8 (yellow), firm, and moist	
18.0	19.5	and moist	
19.5	20.0	Gravelly Clayey Silt, 10YR7/8 (yellow), very firm to stiff, and slightly moist. Gravel is subangular chert, 0.2-to 0.5-inch diameter	
20.0	25.0	Sandy Silt with some Gravel, 7.5YR5/8 (strong brown) mottled with 7.5YR7/1 (light gray) and 7.5YR6/1 (gray), firm, and moist. Gravel is subrounded chert, 0.2- to 0.8-inch diameter	
25.0	25.7	Silty Sand, 7.5YR7/1 (light gray), firm, and very moist. Sand consists of fine and coarse grains. Coarse grains are 1- to 3-mm in diameter and colored white and rose	
25.7	27.0	Silty Sand, 7.5YR7/6 (reddish brown) with inclusions of 7.5YR8/1 (white), firm, and moist. Sand consists of fine and coarse grains. Coarse grains are 1- to 3-mm in diameter (trace subangular grains, 5- to 6-mm diameter)	
27.0	27.2	Silty Sand, 10YR8/1 (white), firm, and moist. Sand is fine quartz grains	
27.2	28.0	grains. Gravel is subangular to subrounded chert, 0.5 to 0.8-inch diameter	HU2
28.0	30.6	Silty Sand with trace Gravel, 10YR7/1 (light gray), firm, and moist. Sand is fine quartz grains. Gravel is colored rose and white, 0.5-inch diameter	

## Plant North -2048.2, Plant East -4995.49

8/17/2012

		1 Iant North -2040.2, 1 Iant East -4775.47	0/17/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
30.6	33.0	Gravelly Sand, 7.5YR6/8 (reddish yellow), semi-loose, and very moist. Sand is coarse grains (1- to 5-mm diameter). Gravel is subangular chert, 0.2- to 0.5-inch diameter	
33.0	33.4	firm, and moist	
33.4	35.9	Silty Gravelly Sand, 7.5YR6/6 (reddish yellow),moderately soft to firm, and moist. Gravel (10% of soil) is subangular chert, 0.2- to 1.0-inch diameter	
35.9	37.5	Sandy Silt, 7.5YR7/8 (reddish brown) with inclusions of 7.5YR7/1 (light gray), soft to firm, and moist	
37.5	39.4	Silty Clay, 7.5YR7/1 (light gray) speckled with 7.5YR3/1 (very dark gray), firm, slightly plastic to plastic, and moist	
39.4	40.0	Silt, 10YR6/3 (pale brown) with zones of 10YR4/1 (dark gray), moderately soft, moderately plastic, and moist	
40.0	42.6	Silt 10VR7/1 (light gray) soft moderately plastic and	
42.6	45.0	Very Clayey Silt, 10YR7/3 (very pale brown) mottled with 5YR5/8 (yellowish red), firm to stiff, plastic, and slightly moist	
45.0	48.0	Silt, 7.5YR5/8 (strong brown) with some 7.5YR7/1 (light gray) banding, firm, slightly plastic, and slightly moist	
48.0	49.0	Silty Clay, 7.5YR5/8 (strong brown) with 7.5YR7/1 (light gray) banding, firm, plastic, and slightly moist	
49.0	51.3	Silt with trace Sand, 10YR7/1 (light gray), soft, and very moist. Sand is very fine quartz grains	HU3
51.3	52.2	Sandy Silt, 10YR6/8 (yellowish brown), with 10YR7/2 (light gray) mottling, firm, and slightly moist. Sand is very fine quartz grains	
52.2	52.4	Gravelly Sandy Silt, 10YR6/8 (yellowish brown), with 10YR7/2 (light gray) mottling, firm, and slightly moist. Sand is very fine quartz grains	
52.4	55.0	Clayey Silt, 10YR7/2 (light gray) with 10YR7/8 (yellow) mottling, firm, plastic, and slightly moist	
55.0	57.5	Silty Clay, 10YR7/1 (light gray) with vertical mottling by 2.5YR4/8 (red), stiff, moderately plastic, and slightly moist	
57.5	58.8	Sandy Silt, 10YR7/6 (yellow) with laminations of 7.5YR6/8 (reddish yellow), firm, and moist	
58.8	60.8	Clayev Silt 10YR7/2 (light gray) mottled with	
60.8	62.0	Sand, 7.5YR6/8 (reddish yellow), soft to loose, and wet	

Plant North -2048.2, Plant East -4995.49	8/17/2012

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
62.0	62.7	Sand, 10YR8/1 (white), loose, and wet. Sand is very fine quartz grains	HU4
62.7	64.5	Silt, 10YR8/1 (white), soft, plastic, and wet	
64.5	65.0	Sand and Gravel, wet. Sand is composed of fine and coarse grains. Gravel is subrounded chert, 0.5- to 1.0-inch diameter	HU5

# Plant North -2043.984, Plant East -4973.547

9/17/2012

Sterrt.	Der 1	Than Norm 2045.704, Than Last 4775.547	
Start Depth	End Depth	Lithology	Hydrogeologic Unit
(ft bgs)	(ft bgs)		
		Gravelly Sand, 2.5YR5/6 (red), dense, and moist. Sand	
0.0	0.1	is fine quartz grains. Gravel is subrounded to	1.11
0.0	3.1	subangular chert with iron patina, 4 mm- to 0.5-inch	Fill
		diameter	
		Silt, 10YR7/2 (light gray) mottled with 10YR7/4 (very	
3.1	15.2	pale brown), soft, nonplastic to slightly plastic, and	
		moist	
		Silt with little Clay and Gravel, 10YR7/2 (light gray)	HU1
		with some 10YR7/3 (very pale brown) mottling,	ног
15.2	18.6	moderately hard, moderately plastic, and moist. Gravel	
		is rounded to subangular chert without iron patina, 0.3-	
		inch diameter	
		Gravely Sand with little Silt, 10YR5/4 (yellowish	
18.6	18.9	brown), firm, and slightly moist. Sand is fine quartz	
18.0	10.9	grains. Gravel is subangular to subrounded chert	
		without(?) iron patina, 4 mm- to 0.4-inch diameter	
		Silty Sand with some Gravel, 10YR7/2 (light gray),	
18.9	19.9	firm, and moist. Sand is very fine quartz grains. Gravel	
10.9	19.9	is subrounded to subangular chert without iron patina,	
		0.3- to 0.4-inch diameter	
		Silty Sand with little Gravel, 7.5YR7/2 (pinkish gray),	
		firm, and moist. Sand consists of 70% fine quartz	
19.9	21.4	grains and 30% very coarse, subrounded, chert grains.	
		Gravel is subrounded chert without(?) iron patina, 4	
		mm- to 0.3-inch diameter	
		Sand, 7.5YR7/6 (reddish yellow) GRADING DOWN	
21.4	22.6	to 10YR7/6 (yellow) mottled with 10YR8/1 (white),	
		firm, and moist. Sand is very fine quartz grains	
		Gravelly Sand with Silt, 10YR6/6 (brownish yellow),	
22.6	23.6	dense, and moist. Sand is fine quartz grains. Gravel is	
		subrounded to subangular chert without iron patina, 0.4-	HU2
		to 0.8-inch diameter Sand, 7.5YR7/6 (reddish yellow), firm, and moist.	
23.6	25.1	Sand, 7.51 K7/0 (redusin yenow), mm, and moist. Sand is fine quartz grains	
		Silt with Sand, 7.5YR7/6 (reddish yellow) mottled with	
25.1	25 0	7.5YR8/1 (white), soft, slightly plastic, and moist.	
23.1	23.9	Sand is fine quartz grains	
		Sand with Gravel, 7.5YR6/8 (reddish yellow) with	
		some 7.5YR8/1 (white) mottling, firm-to-dense, and	
25.9	28.1	moist. Sand is fine quartz grains. Gravel is subrounded	
	2011	to subangular chert without iron patina, 4 mm- to 0.8-	
		inch diameter	
		Sand, 10YR7/3 (very pale brown), firm, and moist.	
28.1	29.1	Sand is fine quartz grains	
29.1	30.0	Sand with Gravel as 25.9 to 28.1 ft	
	20.0	Sand with Gravel, 10YR6/4 (light yellowish brown),	
		firm-to-dense, and moist. Sand is 80% fine quartz	
30.0	32.1	grains and 20% coarse, subrounded, chert grains.	
50.0	52.1	Gravel is subrounded chert with(?) iron patina, 0.3- to	
		0.9-inch diameter	
	1		

### Plant North -2043.984, Plant East -4973.547

9/17/2012

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
32.1	35.6	moist	
35.6	37.5	Silt with Sand, 10YR8/3 (very pale brown), soft, nonplastic, and moist. Sand is very fine quartz grains	
37.5	44.9	Silt GRADING DOWN to Silt with little Clay, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white), soft, moderately plastic to plastic, and moist	
44.9	48.1	Silt, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white), very soft, moderately plastic, and moist	
48.1	48.6	Silty Sand, 7.5YR7/6 (reddish yellow), firm, and moist. Sand is very fine quartz grains	111/2
48.6	50.1	Silt as 44.9 to 48.1 ft	HU3
50.1	50.8	Sand is fine quartz grains	
50.8	51.2	Clay, 7.5YR6/4 (light brown) mottled with 7.5YR8/1 (white), moderately hard, plastic, and moist	
51.2	54.6	Silt with Clay, 7.5YR8/1 (white) with 7.5YR7/6 (reddish yellow) mottling, moderately soft, moderately plastic, and moist	
54.6	55.6	Clay as 50.8 to 51.2 ft	
55.6	57.4	Silt with some Sand, 10YR8/3 (very pale brown), soft, slightly plastic, and moist. Sand is fine quartz grains	
57.4	62.7	Sand is the quartz grains	
62.7	65.0	Sand with Gravel, 10YR8/3 (very pale brown), firm, and wet. Sand is 80% fine quartz grains and 20% coarse, rounded, chert gains. Gravel is rounded to subrounded chert without iron patina, 4 mm- to 0.5- inch diameter	HU4

### Plant North -2066.264, Plant East -5194.135

		Flaint Notul -2000.204, Flaint East -5194.155	9/3/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	3.8	Missing	
3.8	4.2	Fill: Sandy Silty Gravel, 10YR7/1 (light gray), loose, and moist. Gravel is rounded chert, 0.8- to 1.1-inch diameter. Sand is fine quartz grains	Missing and Fill
4.2		Fill: Gravelly Sand, 2.5YR6/8 (light red), loose, and moist. Sand is fine quartz grains. Gravel is rounded chert, 0.8- to 1.1-inch diameter	Trissing and Fin
4.8	4.9	Wood fragments, 10YR2/1 (black)	
4.9	5.0	Silt, 10YR7/1 (light gray) with greenish tinge, soft, nonplastic, and moist	
5.0	5.1	Silt as 4.9 to 5.0 ft	HU1
5.1	17.2	Silt, 10YR8/1 (white) mottled with 10YR7/6 (yellow), moderately soft to soft, nonplastic, and moist	
17.2	19.5	Sand, 7.5YR7/6 (reddish yellow), lightly consolidated, and moist. Sand is very fine GRADING DOWN to fine quartz grains	
19.5	19.8	Sand with Gravel, 10YR7/4 (very pale brown), hard,	
19.8	21.7	Clayey Silt with some Gravel, 10YR7/1 (light gray), hard, moderately plastic, and slightly moist. Gravel is rounded chert without iron patina, 0.2- to 0.3-inch diameter	
21.7	23.0	Sandy Silt with Gravel, 10YR7/2 (light gray), moderately soft, slightly plastic, and moist. Sand is fine quartz grains. Gravel is subangular to subrounded chert without iron patina, 4 mm- to 0.6-inch diameter	
23.0	24.7	Sandy Gravel with Silt, 10YR7/4 (very pale brown), hard, and moist. Gravel is rounded to subrounded chert without iron patina, 0.3- to 0.7-inch diameter. Sand is fine quartz grains	HU2
24.7	25.7	Sandy Silt, 10YR8/1 (white) mottled with 10YR7/6 (yellow), moderately soft, nonplastic, and moist	
25.7	27.3	Sand, 10YR7/6 (yellow) with some 10YR8/1 (white) laminations, lightly consolidated, and moist. Sand is fine quartz grains	
27.3	32.5	Sandy Silt with some Gravel, 7.5YR8/2 (pinkish white) mottled with 7.5YR8/1 (white), moderately soft, nonplastic, and moist. Sand is fine quartz grains. Gravel is rounded to subrounded chert with iron patina, 0.3- to 1.0-inch diameter	
32.5	35.7	Sandy Silty Gravel, 10YR7/4 (very pale brown), lightly consolidated, and moist. Gravel is rounded to subrounded chert with iron patina, 0.3- to 1.0-inch diameter. Sand is fine quartz grains	

## Plant North -2066.264, Plant East -5194.135

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology		Hydrogeologic Unit
35.7	37.4	Clayey Silt, 10YR7/4 (pink), very soft, slightly plastic, and moist		
37.4	45.0	Sandy Silt, 10YR8/1 (white) mottled with 10YR7/6 (yellow), soft, nonplastic, and moist		
45.0	46.0	Silt, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white), soft, moderately plastic, and moist		
46.0	46.3	Silt with Gravel, 7.5YR6/6 (reddish yellow), soft, moderately plastic, and moist. Gravel is rounded to subrounded chert with iron patina, 0.3-inch diameter		
46.3	46.5	Silt, 7.5YR6/6 (reddish yellow), soft, moderately plastic, and moist		
46.5	48.1	Sand, 7.5YR7/6 (reddish yellow) mottled with 7.5YR8/1 (white), lightly consolidated/ moderately soft, slightly plastic, and moist. Sand is very fine quartz grains		
48.1	50.0	Clayey Silt, mottled 7.5YR7/4 (pink) and 7.5YR8/1 (white), soft to moderately soft, plastic, and moist		
50.0	51.7	Sandy Silt, 7.5YR8/2 (pinkish white) mottled with 7.5YR7/4 (pink) and with some 7.5YR3/1 (very dark gray) blebs (manganese?), soft, moderately plastic to slightly plastic, and moist		
51.7	52.1	Sand, 7.5YR8/2 (pinkish white) GRADING DOWN to 7.5YR7/6 (reddish yellow), lightly consolidated, and moist. Sand is fine quartz grains		
52.1	52.3	Clay, 7.5YR7/2 (pinkish gray), moderately soft, plastic, and moist		
52.3	54.5	Sand, 7.5YR7/4 (pink) with few 7.5YR8/1 (white) laminations, lightly consolidated, and moist. Sand is fine quartz grains		HU3
54.5	54.8	Gravelly Sand, 7.5YR7/4 (pink), loose, and very moist. Sand is fine quartz grains. Gravel is subrounded to rounded chert with iron patina, 0.3- to 0.8-inch diameter		
54.8	55.9	Sand with trace Gravel, 7.5YR7/4 (pink), loose, and very moist. Sand is fine quartz grains. Gravel is rounded to subrounded chert with iron patina, 4 mm- to 0.3-inch diameter		
55.9	56.2	Sandy Gravel, 7.5YR7/4 (pink), loose, and very moist. Gravel is rounded to subrounded chert with iron patina, 4 mm- to 0.3-inch diameter. Sand is fine quartz grains		
56.2	56.4	Sand, 10YR8/4 (very pale brown), loose, and wet. Sand is very fine quartz grains		
56.4	56.8	Gravelly Sand, 10YR6/6 (brownish yellow), loose, and moist. Sand is predominately fine quartz grains but includes coarse, subrounded, chert grains. Gravel is rounded to subrounded chert with iron patina, 0.2- to 1.0-inch diameter		

### Plant North -2066.264, Plant East -5194.135

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Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
56.8	58.4	Slightly Clayey Silt, 10YR8/1 (white) with abundant 10YR7/6 (yellow) laminations, moderately soft, moderately plastic, and moist	
58.4	59.8	Clayey Silt, 5YR8/1 (white) with abundant 5YR7/8 (reddish yellow) laminations, moderately soft, plastic, and moist	
59.8	62.6	Silt, 10YR8/6 (yellow) with 10YR8/1 (white) mottling, soft, slightly plastic, and moist	
62.6	64.2	Sand, 10YR8/4 (very pale brown) with 10YR7/6 (yellow) laminations GRADING DOWN to 10YR8/1 (white), lightly consolidated, and moist. Sand is very fine to fine quartz grains	
64.2	65.0	Gravelly Sand, 10YR8/2 (very pale brown), loose, and moist. Sand is predominately fine quartz grains but includes 15 to 20% coarse, subangular, chert grains. Gravel is subrounded to rounded chert with iron patina, 0.2- to 1.0-inch diameter	HU4

## Plant North -2065.901, Plant East -5119.305

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Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	0.5	nonplastic, and dry	
0.5	3.4	Sandy Gravel, 5YR5/8 (yellowish red), loose, and moist. Gravel is rounded to subrounded chert with iron patina, 0.2- to 0.8-inch diameter. Sand is fine quartz grains	Fill
3.4	5.0	Silt, 10YR7/1 (light gray) with green tinge, moderately soft, nonplastic, and slightly moist	
5.0	15.0	mottling	
15.0	18.4	10YR//1 (light gray) mottling	HU2
18.4	22.3	of subrounded to subangular chert gravel (with little iron patina), 0.2- to 0.4-inch diameter	
22.3	25.0	Silty Sandy Gravel, 10YR6/3 (pale brown), dense/hard, and moist. Gravel is subangular chert with little iron patina, 4 mm- to 0.3-inch diameter. Sand is fine quartz grains	
25.0	28.8	Interbedded Sand and Silt, 10YR6/4 (light yellowish brown) with some 10YR8/1 (white) mottling, lightly consolidated/soft, nonplastic to slightly plastic, and moist. Sand is very fine quartz grains	
28.8	33.1	Gravelly Sand, 10YR6/3 (pale brown) mottled with 10YR8/1 (white), moderately dense/hard, and moist. Sand is very fine quartz grains. Gravel is subrounded chert with light iron patina, 0.3- to 1.1-inch diameter	HU3
33.1	34.5	Gravelly Sand as 28.8 to 33.1 ft but with some Clay	
34.5	35.8	and moist. Sand is fine quartz grains	
35.8	37.5	Silty Sandy Gravel, 10YR7/2 (light gray), moderately dense/hard, and moist. Gravel is rounded to subangular chert with iron patina, 0.3- to 1.0-inch diameter. Sand is fine quartz grains	
37.5	38.7	Silty Sand, 10YR8/2 (very pale brown) with 10YR7/6 (yellow) laminations, lightly consolidated/soft, nonplastic, and moist. Sand is fine quartz grains	
38.7	39.8	very moist	
39.8	40.6	fine quartz grains	
40.6	42.4	Clayey Silt, 10YR8/2 (very pale brown) with light 10YR7/6 (yellow) mottling, moderately soft, moderately plastic, and moist	

#### Plant North -2065.901, Plant East -5119.305

		Plant North -2065.901, Plant East -5119.305	9/5/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
42.4	43.4	Sand, 10YR8/2 (very pale brown), lightly consolidated, and very moist. Sand is fine quartz grains	
43.4	45.8	Clayey Silt, 10YR8/2 (very pale brown) with light mottling by 10YR7/6 (yellow), moderately soft, moderately plastic, and moist	
45.8	49.6	soft, slightly plastic to nonplastic, and moist. Sand is very fine quartz grains	HU3
49.6	52.4	Sand, 10YR8/1 (white) with 10YR7/6 (yellow) mottling, lightly consolidated, and moist. Sand is very fine quartz grains	105
52.4	54.2	Sand, 10YR8/2 (very pale brown) with 10YR7/6 (yellow) laminations and staining, lightly consolidated and moist. Sand is fine quartz grains	
54.2	56.9	Gravelly Sand, 10YR7/2 (light gray), loose, and moist.	
56.9	58.4	Clayey Silt, 7.5YR7/4 (pink) with some 7.5YR7/1 (light gray) mottling, soft, moderately plastic, and moist	
58.4	60.0	Silt with some Sand, 10YR8/2 (very pale brown) with 10YR7/6 (yellow) laminations, soft, slightly plastic, and moist. Sand is fine quartz grains	
60.0	60.2	Clay, 10YR8/1 (white), soft, plastic, and moist	
60.2	62.0	Sand with Silt, 10YR8/1 (white) with some 10YR7/6 (yellow) mottling, lightly consolidated/soft, nonplastic, and moist. Sand is very fine quartz grains	
62.0	63.5	Sand, 10YR7/6 (yellow), lightly consolidated, and moist. Sand is fine quartz grains	HU4
63.5	63.8	Clay as 60.0 to 60.2 ft	
63.8		Sandy Gravel, 10YR6/4 (light yellowish brown), loose, and moist. Gravel is subangular to subrounded chert with iron patina, 0.2- to 0.4-inch diameter. Sand is equal parts fine quartz grains and medium and coarse, subrounded, chert grains	HU5

### Plant North -2066.201, Plant East -5088.967

9/6/2012

		Flain Notul -2000.201, Flain East -5088.907	9/0/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	0.4	mm- to 0.6-inch diameter (dense gravel aggregate/DGA)	Fill
0.4	3.8	Fill: Silty Sandy Gravel, 2.5YR5/8 (red), moderately dense/hard, and moist. Gravel is subrounded to subangular chert with iron patina, 0.4- to 1.0-inch diameter. Sand is fine quartz grains	
3.8	5.1	Silt, 10YR7/1 (light gray), soft, nonplastic, and moist	
5.1	14.8	Silt, 10YR7/3 (very pale brown) mottled with 10YR7/1 (light gray), soft, nonplastic to slightly plastic, and moist	
14.8	15.8	Silt, 10YR8/3 (very pale brown), moderately hard, nonplastic, and slightly moist	
15.8	17.3	Sand, 10YR8/2 (very pale brown) with little 10YR7/4 (very pale brown) mottling, lightly consolidated/soft, nonplastic, and moist. Sand is very fine quartz grains	HU1
17.3	21.6	Clayey Silt with trace of Gravel, 10YR7/1 (light gray), moderately hard, slightly to moderately plastic, and moist. Gravel is rounded chert with light iron patina, 0.2- to 0.3-inch diameter	
21.6	25.5	Gravelly Sand with Silt, 10YR7/4 (very pale brown), dense/hard, and moist. Sand is predominately fine quartz grains but includes some coarse, subrounded, chert grains. Gravel is subrounded to subangular chert with iron patina, 0.2- to 0.8-inch diameter	
25.5	26.4	10YR8/1 (white), soft, plastic, and moist	
26.4	28.1	Interbeds of Sand (fine quartz grains) and Clayey Silt, 7.5YR7/8 (reddish yellow) with blebs of 7.5YR8/1 (white), soft, slightly plastic, and moist	HU2
28.1	33.8	Sandy Silt, 10YR8/2 (very pale brown) with light 10YR7/6 (yellow) mottling, soft, slightly plastic, and moist	
33.8	35.5	Gravelly Sand with Silt, 10YR8/2 (very pale brown) with 10YR8/1 (white) mottling GRADING DOWN to 7.5YR7/4 (pink), dense/hard, and moist. Sand is fine to medium quartz grains. Gravel is rounded to subangular chert with iron patina, 0.2- to 0.8-inch diameter	
35.5	37.9	(white), soft, plastic, and moist	
37.9	42.8	Slightly Clayey Silt, 10YR8/1 (white) with heavy 10YR7/6 (yellow) mottling, soft, slightly plastic, and moist	

#### Plant North -2066.201, Plant East -5088.967

9/6/2012

		1 Iant 101111 - 2000.201, 1 Iant East - 3088.907	9/0/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
42.8		Silt, 10YR8/2 (very pale brown) mottled with 10YR6/6 (brownish yellow), moderately soft, slightly plastic, and moist	HU3
53.3	58.6	Silty Sand, 10YR8/1 (white) GRADING DOWN to 10YR7/6 (yellow) mottled with 10YR8/1 (white), lightly consolidated/soft, nonplastic to slightly plastic, and moist. Sand is fine quartz grains	
58.6	60.8	Clayey Silt, 10YR8/1 (white) with light 10YR7/6 (yellow) laminations, moderately soft, plastic, and moist	
60.8		Sand, 10YR8/4 (very pale brown) GRADING DOWN to 10YR8/1 (white), lightly consolidated, and very moist. Sand is fine quartz grains	HU4
65.6	66.0	Sandy Gravel, 7.5YR8/2 (pinkish white), loose, and wet. Gravel is subrounded to subangular chert with iron patina, 0.3- to 1.0-inch diameter. Sand is 85% fine quartz grains and 15% coarse, subangular, chert grains	HU5

## Plant North -2065.945, Plant East -5059.023

9/27/2012

Start	End		
Depth (ft hgs)	Depth (ft bgg)	Lithology	Hydrogeologic Unit
(ft bgs)	(ft bgs)	Sandy Gravel, 2.5YR6/6 (light red), dense, and moist.	
		Gravel is subangular to subrounded chert with iron	
0.0	2.2	patina, 0.4- to 0.8-inch diameter. Sand is fine quartz	FILL
		grains	
2.2	6.0	Silt, 10YR7/2 (light gray) mottled with 10YR6/1	
		(gray), moderately hard, nonplastic, and moist	
6.0	14.7	Silt, 10YR8/2 (very pale brown) mottled with 10YR7/6 (yellow), soft, nonplastic, and moist	
	1.5.0	Sand 10VR7/3 (very pale brown) firm and moist	
14.7	15.8	Sand is very fine quartz grains	
		Interbedded Silt, 7.5YR7/4 (pink), soft, slightly plastic,	
15.8	16.7	and moist AND Sand, 7.5YR6/6 (reddish yellow), firm,	
		and moist. Sand is very fine quartz grains	
167	19.0	Clay, 7.5YR7/6 (reddish yellow), moderately hard,	HU1
16.7	19.0	plastic, and moist	
		Clay with some Silt and some Gravel, 10YR7/2 (light	
19.0	20.0	gray) with 10YR7/4 (very pale brown) mottling.	
19.0	20.0	Gravel is subangular chert without iron patina, 0.3- to 0.4-inch diameter AND rounded chert without iron	
		patina, 0.6-inch diameter	
		Silt with Sand, 10YR8/1 (white) with 10YR7/6	
20.0	23.8	(yellow) mottling, soft, nonplastic, and moist. Sand is	
		very fine quartz grains	
		Silty Gravel with Sand, 7.5YR6/6 (reddish yellow)	
		with some 7.5YR3/1 (very dark gray) stain	
23.8	25.7	(manganese?), dense, and moist. Gravel is subrounded to subangular chert without iron patina, 4-mm to 0.6-	
		inch diameter. Sand is 80% fine quartz grains and 20%	
		coarse, subrounded, chert grains	
25.5	24.4	Sand, 10YR8/4 (very pale brown), firm, and moist.	
25.7	26.1	Sand is fine quartz grains	
		Gravelly Sand, 10YR7/4 (very pale brown), firm, and	
26.1	26.4	moist. Sand is fine quartz grains. Gravel is rounded to	HU2
		subangular chert without iron patina, 0.3- to 0.4-inch diameter	
		Silt with Sand, 10YR8/3 (very pale brown) with	
26.4	33.1	10YR7/6 (yellow) mottling, soft, nonplastic, and moist.	
		Sand is very fine quartz grains	
33.1	34.7	Sand, 10YR8/2 (very pale brown), firm, and moist.	
		Sand is very fine quartz grains Silty Gravel with Sand, 7.5YR6/4 (light brown), dense,	
34.7	35.2	and moist. Gravel is subrounded chert without iron	
		patina, 4-mm to 0.4-inch diameter	
		Silt with Clay, 7.5YR7/4 (pink) mottled with 7.5YR8/1	
35.2	39.5	(white) GRADING DOWN to 7.5YR8/1 (white)	
		mottled with 7.5YR7/4 (pink), soft, plastic, and moist	
			· · ·

### Plant North -2065.945, Plant East -5059.023

9/27/2012

		Plaint Norul -2003.945, Plaint East -3059.025	9/27/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
39.5	43.2	Silt, 10YR8/1 (white) mottled with 10YR7/6 (yellow), soft, slightly plastic, and moist	
43.2	44.9	Silt with Clay, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white)	
44.9	48.0	Silt, 10YR8/2 (very pale brown) mottled with 7.5YR5/8 (strong brown), moderately soft, moderately plastic, and moist	
48.0	48.9	Clay with Silt, 10YR8/3 (very pale brown), moderately hard, plastic, and moist	
48.9	49.6	Silt with Sand and Gravel, 10YR8/2 (very pale brown), moderately hard, nonplastic, and moist. Sand is very fine quartz grains. Gravel is subrounded chert without iron patina, 4-mm to 0.7-inch diameter	
49.6	50.0	Sand, 10YR8/1 (white) mottled with 10YR7/6 (yellow), firm, and moist. Sand is very fine quartz grains	HU3
50.0	51.0	Clay with Silt, 10YR8/2 (very pale brown) mottled with 7.5YR7/6 (reddish yellow), moderately hard, plastic, and moist	
51.0	54.9	Silt with Sand, 10YR8/1 (white) mottled with 10YR7/6 (yellow) and 7.5YR7/6 (reddish yellow), moderately soft, nonplastic, and moist. Sand is very fine quartz grains	
54.9	56.8	Clay with some Silt, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white), moderately soft, plastic, and moist	
56.8	58.1	Sand, 10YR8/2 (very pale brown) with 10YR8/6 (yellow) staining, lightly consolidated, and moist. Sand is very fine quartz grains	
58.1	60.2	Silt, 7.5YR7/6 (reddish yellow) mottled with 7.5YR8/1 (white), soft, moderately plastic, and moist	
60.2	65.0	Sand, 10YR8/2 (very pale brown) with 7.5YR8/4 (pink) mottling, lightly consolidated, and moist. Sand is very fine quartz grains	HU4
65.0	65.2	Sandy Gravel, 10YR4/2 (dark grayish brown) (stained with manganese?), loose, and moist. Gravel is subrounded to subangular chert with iron patina, 0.3- to 0.6-inch diameter. Sand is fine quartz grains	HU5

### Plant North -2066.342, Plant East -5029.003

9/21/2012

		Flaint Norul -2000.542, Flaint East -5029.005	9/21/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	2.1	Gravelly Sand, 2.5YR6/4 (light reddish brown), loose, and moist. Sand is 80% fine quartz grains and 20% coarse, subrounded, quartz grains. Gravel is subangular to subrounded chert with iron patina, 4-mm to 0.5-inch diameter	Fill
2.1	5.1	Silt, 10YR7/1 (light gray), moderately soft, nonplastic, and moist	
5.1	17.6	Silt, 10YR7/2 (light gray) with 10YR7/6 (yellow) mottling, soft, slightly plastic, and moist	
17.6	18.3	Sand 7 5VR6/4 (light brown) loose and wet Sand is	HU1
18.3	20.1	Silt with little Clay, 7.5YR8/1 (white) with heavy mottling by 7.5YR7/6 (reddish yellow), moderately hard, moderately plastic, and moist	
20.1	21.6	Gravelly Sand with some Silt, 7.5YR6/4 (light brown), moderately dense, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert with iron patina, 4-mm to 0.4-inch diameter	
21.6	22.0	Sandy Silt with some Clay, 10YR8/2 (very pale brown), soft, slightly plastic, and wet	
22.0	22.8	Sand, 10YR7/3 (Very pale brown), loose, and wet. Sand is very fine quartz grains	
22.8	23.7	Silt GRADING DOWN to Sand, 10YR7/3 (very pale brown), soft, nonplastic, and moist. Sand is fine quartz grains	
23.7	24.3	Silt with some Clay and little Gravel, 10YR7/1 (light gray), moderately hard, plastic, and moist	
24.3	26.0	Sandy Gravel with little Silt, 10YR7/4 (very pale	HU2
26.0	27.0	Sand, 10YR8/2 (very pale brown), firm, and moist. Sand is fine quartz grains	
27.0		Sandy Gravel with little Silt as 24.3 to 26.0 ft	
27.3		Silt with little Sand, 10YR8/2 (very pale brown) mottled with 10YR7/6 (yellow), soft, nonplastic, and moist. Sand is fine quartz grains	
30.0	32.5	Silt, 7.5YR7/4 (pink), moderately hard, slightly plastic, and moist	
32.5	34.0	Sand with Gravel, 7.5YR7/6 (reddish yellow) GRADING DOWN to 7.5YR8/2 (pinkish white), dense, and moist. Sand is very fine quartz grains. Gravel is subrounded chert with iron patina, 0.3- to 0.8- inch diameter	
34.0	35.0	Sand, 10YR7/6 (yellow), firm, and moist. Sand is very fine to fine quartz grains	
35.0	39.0	Clay, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white), soft, plastic, and moist	

#### Plant North -2066.342, Plant East -5029.003

9/21/2012

		Plant North -2066.342, Plant East -5029.003	9/21/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
39.0	42.6	Silt with little Sand, 10YR8/2 (very pale brown) mottled with 10YR7/6 (yellow), soft, nonplastic, and moist. Sand is very fine quartz grains	
42.6	47.1	Silt with little Clay, 10YR7/3 (very pale brown) with 10YR7/6 (yellow) and 10YR7/1 (light gray) mottling, soft, slightly plastic, and moist	
47.1	50.0	Silt with Clay, 7.5YR7/1 (light gray) mottled with 7.5YR7/4 (pink), soft, moderately plastic, and moist	
50.0	51.6	Silt, 10YR7/1 (light gray), soft, moderately plastic, and moist	HU3
51.6	52.6	Silt with Sand, 10YR7/1 (light gray), firm/moderately soft, nonplastic, and moist. Sand is very fine quartz grains	
52.6	53.7	Sand, 7.5YR7/6 (reddish yellow) with 7.5YR8/1 (white) mottling, firm, and moist. Sand is fine quartz grains	
53.7	58.4	Silt with little Clay, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white) GRADING DOWN to 7.5YR8/1 (white), soft, moderately plastic, and moist	
58.4	61.0	Clay with Silt, 10YR8/2 (very pale brown), soft, plastic, and moist	
61.0	64.4	Sand, 10YR8/2 (very pale brown) GRADING DOWN to 10YR7/3 (very pale brown), lightly consolidated to loose, and moist to wet. Sand is very fine quartz grains	HU4
64.4	65.0	Silt with little Clay, 10YR8/1 (white), soft, moderately plastic, and moist	
65.0	65.1	Sand as 61.0 to 64.4 ft	
65.1	65.2	Sandy Gravel. Gravel is subangular chert with iron patina, 0.4- to 1.0 inch diameter	HU5

Plant North -2066.381, Plant East -4994.899

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0		Concrete and gravel	FILL
1.0		Silt, 10YR7/1 (light gray), firm, and moist	
5.0	7.0	Silt 10VP7/1 (light gray) mottled with 7 5VP7/8	
5.0	7.0	(reddish yellow), firm, and slightly moist	
7.0	10.0	Silt, 10YR7/1 (light gray) mottled with 7.5YR7/8 (reddish yellow) and containing blebs of 10YR4/1 (dark gray), firm, and slightly moist	
10.0	13.5	Silt, 10YR7/1 (light gray) with slight mottling by 10YR6/8 (brownish yellow), moderately firm, and slightly moist	
13.5	15.0	Silt, 10YR6/8 (brownish yellow), moderately firm, and slightly moist	
15.0	18.5	Silt, 10YR7/4 (very pale brown), firm, and slightly moist	HU1
18.5	20.0	Gravelly Silty Clay, 10YR7/2 (light gray) intermixed with 10YR5/8 (dark yellowish brown), stiff, and slightly moist. Gravel is subrounded chert with and without (white) iron patina, 0.5- to 1.2-inch diameter	
20.0	23.5	Silty Clayey Sand with trace Gravel, 10YR5/6 (yellowish brown), firm, and slightly moist. Sand is medium to coarse grained	
23.5	25.0	Clayey Sand, 10YR7/1 (light gray) mottled with 10YR6/8 (brownish yellow), firm, and slightly moist. Sand is fine to medium quartz grains	
25.0	28.7	Clayey Gravelly Sand, 7.5YR5/8 (strong brown), firm, and slightly moist. Sand is fine to coarse grained. Gravel is subrounded to subangular chert, 0.5- to 0.8- inch diameter	
28.7	30.0	Silty Sand 10VR7/2 (light gray) semi-firm and	HU2
30.0	35.9	Silty Gravelly Sand, 7.5YR6/8 (reddish yellow). Sand is medium to coarse quartz grains. Gravel (5 to 10% of sample) is chert, 0.2- to 1.0-inch diameter	
35.9	41.0	Intermixed Silts 10VP7/1 (light gray) and 7 5VP7/8	
41.0	41.5	Sandy Silt 10VR5/4 (vellowish brown) moderately	
41.5	44.5	Silt 10VD7/1 (light gray) mottled with 5VD6/9	
44.5	45.0	Silty Sand 10YR7/2 (light gray) firm and slightly	
45.0	52.0	Silty Sand, 7.5YR7/1 (light gray) mottled with 7.5YR6/8 (reddish yellow), moderately firm, and slightly moist	
52.0	55.0	Silty Gravelly Sand, 10YR7/1 (light gray) mottled with 7.5YR6/8 (reddish yellow), firm, and slightly moist. Gravel is subrounded chert, 0.2- to 0.8-inch diameter	HU3

## Plant North -2066.381, Plant East -4994.899

Start	End		
Depth	Depth	Lithology	Hydrogeologic Unit
(ft bgs)	(ft bgs)		
55.0	56.3	Clayey Silt, 10YR7/1 (light gray) mottled with 7.5YR5/8 (strong brown), stiff, and moist	
56.3	57.0	Sand, 10YR7/1 (light gray), loose, and saturated (flowing)	
57.0	57.5	Silty Clay, 7.5YR5/8 (strong brown), firm, and slightly moist	
57.5	58.6	No recovery	
58.6	60.9	Clayey Silt, 5YR7/6 (reddish yellow) mottled with 5YR8/1 (white), moderately hard, slightly plastic, and moist	
60.9	62.1	Sand, 10YR8/1 (white) with 10YR7/6 (yellow) laminations, lightly consolidated, and moist. Sand is very fine quartz grains	
62.1	63.7	Silt, 10YR8/2 (very pale brown) with 10YR7/6 (yellow) laminations, soft, slightly plastic, and moist	HU4
63.7	64.1	Sand, 10YR8/1 (white), loose, and wet. Sand is very fine quartz grains	
64.1	64.4	subrounded to subangular chert with iron patina, 0.2- to 0.5-inch diameter	
64.4	65.0	Sandy Gravel, 10YR7/4 (very pale brown), loose, and wet. Gravel is subangular to subrounded chert with iron patina, 0.3- to 1.0-inch diameter. Sand is 80% very fine quartz grains and 20% coarse, rounded, chert with iron patina grains	HU5

## Plant North -2066.175, Plant East -4974.143

<u> </u>	<b></b>	Fight Hora 2000.175, Fight East 1771.115	
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	1.8	Gravelly Silt, 10YR7/1 (light gray), loose, and slightly moist. Gravel is subangular limestone, 0.2- to 0.4-inch diameter (dense gravel aggregate/DGA)	FILL
1.8	4.2	Silt, 10YR7/1 (light gray) with light blue tinge, soft, nonplastic, and slightly moist	
4.2	14.9	Silt, 10YR8/2 (very pale brown) with variable mottling by 10YR7/6 (yellow), soft, slightly plastic, and moist. Note: some 10YR3/1 (very dark gray) mottling (manganese?) beginning at 13.0 ft	
14.9	18.9	Silt 7 5VR7/4 (nink) with 7 5VR8/1 (white) mottling	
18.9	20.6	and moist. Gravel is rounded chert, predominately 0.3- inch diameter but up to 0.7-inch diameter	HU1
20.6	21.1	Gravelly Sand with Silt, 7.5YR6/6 (Reddish yellow), firm, and moist. Sand is very fine quartz grains. Gravel is subangular to subrounded chert with iron patina, 4 mm- to 0.4-inch diameter	
21.1	22.2	Clayey Silt with some Gravel, 7.5YR7/1 (light gray) mottled with 7.5YR7/6 (reddish yellow), moderately soft, plastic, and moist	
22.2	22.5	Silt, 10YR8/1 (white), soft, nonplastic, and moist	
22.5	23.2	Sand, 7.5YR6/6 (reddish yellow), firm, and moist. Sand is fine quartz grains	
23.2	23.6	Gravelly Sand with Silt as 20.6 to 21.1 ft	
23.6		Silt with Sand, 7.5YR8/1 (white) with little 7.5YR7/6 (yellow) mottling, moderately soft, nonplastic, and moist. Sand is very fine quartz grains	
24.9	26.0	Sandy Gravel, 7.5YR7/4 (pink), dense, and slightly moist. Gravel is subangular chert with no-to-little iron patina, 4-mm to 0.6-inch diameter. Sand is 60% fine quartz grains and 40% coarse, rounded, chert grains	
26.0	27.2	Silty Gravelly Sand, 10YR7/4 (very pale brown), dense, and moist. Sand is fine quartz grains. Gravel is rounded to subrounded chert with light iron patina, 0.4- to 1.0-inch diameter	
27.2	28.9	Slightly Clayey Silt, 7.5YR7/6 (reddish yellow) mottled with 7.5YR8/1 (white), soft, moderately plastic, and moist	HU2
28.9	33.2	Silty Gravelly Sand, 7.5YR5/6 (strong brown), dense, and moist. Sand is 60% fine quartz grains and 40% coarse, rounded, chert grains. Gravel is subrounded to subangular chert with iron patina, 4 mm- to 0.7-inch diameter	

# Plant North -2066.175, Plant East -4974.143

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
33.2	34.5	Sand GRADING DOWN to Sand with Gravel, 7.5YR8/6 (reddish yellow), lightly consolidated, and moist. Sand is fine quartz grains. Gravel is subangular chert with iron patina, 0.4- to 0.5-inch diameter	
34.5	35.3	Sandy Gravel with Silt, 10YR5/1 (gray) (stained with manganese?) GRADING DOWN to 10YR6/4 (light yellowish brown), dense, and moist. Gravel is subangular to subrounded chert with iron patina, 4 mm- to 0.8-inch diameter. Sand is fine quartz grains	
35.3	39.0	Slightly Clayey Silt, 7.5YR7/4 (pink) with 7.5YR7/1 (light gray) mottling GRADING DOWN to 7.5YR6/1 (gray), moderately hard, slightly plastic, and moist	
39.0	42.1	Silt, 10YR7/3 (very pale brown), moderately soft to moderately hard, slightly plastic, and moist	
42.1	43.6	Slightly Clavey Silt 10YR6/2 (light brownish gray)	
43.6	44.8	Silt 10VR6/3 (nale brown) moderately soft	
44.8	47.0	Slightly Clayey Silt as 42.1 to 43.6 ft	
47.0	50.5	Slightly Clayey Silt, 7.5YR6/8 (reddish yellow) mottled with 7.5YR7/1 (light gray), moderately hard, slightly plastic, and moist	HU3
50.5	54.6	Silt, 10YR8/3 (very pale brown) mottled with 10YR7/1 (light gray) and 10YR7/6 (yellow), moderately soft, slightly plastic, and moist Slightly Clayey Silt, 7.5YR8/4 (pink) mottled with	
54.6	58.3	7.5YR8/1 (white) and 7.5YR6/8 (reddish yellow), moderately hard, slightly plastic, and moist	
58.3	61.0	Silt with Sand, 7.5YR8/1 (white) mottled with 7.5YR7/4 (pink), soft, nonplastic, and moist. Sand is very fine quartz grains	
61.0	63.0	Sand, 10YR8/3 (very pale brown) with some 10YR7/8 (yellow) laminations, firm, and moist. Sand is very fine quartz grains	HU4
63.0	64.0	Silt, 10YR8/1 (white) with 10YR7/6 (yellow) laminations, loose, nonplastic, and moist	
64.0	65.0	Gravelly Sand, 7.5YR7/3 (pink), loose, and wet. Sand is 80% fine quartz grains and 20% coarse, subangular	HU5

Plant North -2085.988, Plant East -5035.164

9/24/2012

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	3.9	Silty Gravelly Sand, 2.5YR5/6 (red), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to rounded chert with iron patina, 0.4- to 0.6-inch diameter	FILL
3.9	14.9	Silt, 10YR8/2 (very pale brown) mottled with 10YR7/6 (yellow), soft, nonplastic to slightly plastic, and moist	
14.9	15.2	Sand, 10YR8/1 (white), dense, and moist. Sand is very fine quartz grains	
15.2	18.3	Silt, 10YR6/6 (brownish yellow) mottled with 10YR8/2 (very pale brown), soft, nonplastic, and moist	HU1
18.3	19.8	Silty Clay, 10YR7/1 (light gray), moderately hard, moderately plastic, and moist	
19.8	20.9	Silt with some Gravel, 10YR8/2 (very pale brown)	
20.9	21.5	Sand with Gravel, 7.5YR6/6 (reddish yellow), lightly consolidated, and moist. Sand is fine to medium, rounded, quartz grains. Gravel is subangular chert without iron patina, 0.3- to 0.4-inch diameter	
21.5	22.3	Silty Gravel with Sand, 7.5YR6/4 (light brown), dense, and moist. Gravel is rounded to subangular chert without iron patina, 0.3- to 0.4-inch diameter. Sand is fine quartz grains	
22.3	22.8	Clay, 10YR7/1 (light gray), moderately soft, plastic, and moist	
22.8	24.4	Gravelly Sand, 7.5YR7/4 (pink) with some staining by 7.5YR3/1 (very dark gray) (manganese?), firm, and moist. Sand is fine quartz grains. Gravel is subangular chert with iron patina, 0.4- to 0.6-inch diameter	
24.4	26.8	Gravel is subangular to subrounded chert with iron patina, 0.4- to 0.6-inch diameter	HU2
26.8	27.4	Sandy Gravel, 10YR8/3 (very pale brown), loose, and moist. Gravel is rounded to subrounded chert without iron patina, 0.3- to 0.4-inch diameter	
27.4	30.9	Silt, 10YR7/3 (very pale brown) with little mottling by 10YR8/1 (white), soft, nonplastic, and moist	
30.9	31.7	Silt with some Gravel, 10YR7/3 (very pale brown) with little mottling by 10YR8/1 (white), soft, plastic, and moist. Gravel is subrounded to subangular chert without iron patina, 0.4-inch diameter	

## Plant North -2085.988, Plant East -5035.164

9/24/2012

		1 Iant North -2005.700, 1 Iant East -5055.104	)/24/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
31.7	32.5	Sand with Gravel, 10YR8/2 (very pale brown), firm, and moist. Sand is very fine quartz grains. Gravel is subrounded to subangular chert without iron patina, 0.4- inch diameter	
32.5	35.0	No recovery	NO RECOVERY
35.0	35.6	Silt with little Clay and Gravel, 10YR7/4 (very pale brown), soft, moderately plastic, and moist. Gravel is rounded chert without iron patina, 4-mm to 0.3-inch diameter	
35.6	39.5	Silt with little Clay, 7.5YR7/6 (reddish yellow) mottled with 7.5YR8/1 (white) GRADING DOWN to 7.5YR8/1 (white), soft, plastic, and moist	
39.5	43.1	Silt, 10YR8/2 (very pale brown) mottled with 10YR7/4 (very pale brown), soft, nonplastic, and moist	
43.1	45.0	Silt with little Clay, 10YR7/1 (light gray) with some 10YR6/6 (brownish yellow) mottling, moderately hard, plastic, and moist. Note: red tinge over 44.5 to 45.0 ft	
45.0	47.5	Silt with Sand, 10YR8/1 (white) with some 10YR6/6 (brownish yellow) mottling, soft, nonplastic, and moist. Sand is very fine quartz grains	
47.5	53.0	Silt with Sand, 10YR8/2 (very pale brown) mottled with 10YR7/6 (yellow), soft, nonplastic, and moist. Sand is very fine quartz grains	
53.0	53.4	Sand, 10YR8/1 (white) with 2.5YR8/3 (pink) tinge, firm, and moist. Sand is very fine quartz grains	HU3
53.4	54.5	Sandy Gravel, 10YR8/1 (white) with some 10YR7/6 (yellow) staining, firm/moderately consolidated, and moist. Gravel is subrounded to subangular chert without iron patina, 0.3- to 0.4-inch diameter. Sand is fine quartz grains	
54.5	55.0	Sand with some Gravel, 10YR7/6 (yellow), firm, and moist. Sand is fine quartz grains. Gravel is subrounded chert without iron patina, 0.4- to 0.8-inch diameter	
55.0	56.9	Silt with some Clay, 10YR8/2 (very pale brown) with 10YR7/6 (yellow) laminations, soft, slightly to moderately plastic, and moist	
56.9	58.4	Silt with some Sand, 10YR8/2 (very pale brown), soft, slightly plastic, and moist. Sand is very fine quartz grains	
58.4	59.1	Sand, 10YR8/1 (white), loose, and wet. Sand is very fine quartz grains	
59.1	61.1	Silty Sand with Silt interbeds, 10YR8/1 (white) with 10YR7/6 (yellow) laminations, lightly consolidated, and moist. Sand is very fine quartz grains	
61.1	62.6	Sand 10YR8/6 (vellow) firm and moist Sand is very	

#### Plant North -2085.988, Plant East -5035.164

9/24/2012

		1 failt 1(0)th 2005.900, 1 failt East 5055.101	J72 1/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
62.6	64.6	Sand, 10YR8/3 (very pale brown), loose, and wet. Sand is very fine quartz grains	HU4
64.6	65.0	Silt, 10YR8/1 (white), soft, plastic, and moist	
65.0	65.3	Sand, 10YR7/3 (very pale brown), firm, and moist. Sand is fine quartz grains	
65.3	67.5	Sandy Gravel, 10YR6/3 (pale brown), loose, and wet. Gravel is subangular to subrounded chert, 0.3- to 1.0- inch diameter. Sand is 75% fine to medium, rounded, quartz grains and 25% coarse, rounded, chert grains. Note: 10YR5/1 (gray) staining (manganese?) over 66.1 to 66.5 ft	HU5

## Plant North -2096.095, Plant East -5089.217

9/6/2012

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	1.0	No description	
1.0	4.0	Sandy Gravel, 2.5YR6/6 (light red), moderately dense/hard, and moist. Gravel is subrounded chert with iron patina, 0.3- to 0.4-inch diameter. Sand is fine quartz grains	Fill
4.0	5.0	Silt, 10YR7/1 (light gray) with bluish tinge, moderately hard, nonplastic, and moist	
5.0	15.0	Silt, 10YR7/1 (light gray) with 10YR7/6 (yellow) staining and mottling, soft, nonplastic, and moist	
15.0	18.5	Slightly Clayey Silt with some Sand, 7.5YR7/6 (reddish yellow) with little 7.5YR8/1 (white) mottling, soft, moderately plastic, and moist	
18.5	19.9	Clayey Silt, 10YR7/1 (light gray) with 10YR7/4 (very pale brown) mottling, moderately hard to hard, moderately plastic, and moist	HU1
19.9	20.0	Sand, 10YR6/6 (brownish yellow), loose, and moist. Sand is very coarse, angular, chert grains	
20.0	20.9	and moist	
20.9	23.4	Clayey Silt, 10YR7/1 (light gray) with 10YR7/6 (yellow) mottling, moderately hard, moderately plastic, and moist. Trace chert gravel without iron patina, rounded, 0.2-inch diameter	
23.4	24.0	Sandy Gravel with Silt, 7.5YR5/6 (strong brown), moderately dense/hard, and moist. Gravel is subangular chert with light iron patina, 0.2- to 0.3-inch diameter	
24.0	24.8	Sandy Silt, 10YR8/1 (white), soft, nonplastic, and moist	
24.8	25.0	Sandy Gravel, 10YR6/6 (brownish yellow), loose, and moist. Gravel is subrounded to subangular chert with iron patina, 0.3-inch diameter. Sand is fine quartz grains	
25.0	25.7	Silt, 10YR6/4 (light yellowish brown), soft, moderately plastic, and moist	
25.7	29.8	Interbedded Silt with some Sand and slightly Clayey Silt, 10YR8/1 (white) with light 10YR7/6 (yellow) staining and mottling, moderately soft, slightly to moderately plastic, and moist	HU2
29.8	30.0	Sandy Gravel, 10YR6/6 (brownish yellow), loose, and moist. Gravel is subangular to subrounded chert with	
30.0	30.5	Sand, 7.5YR7/4 (pink), lightly consolidated, and moist. Sand is fine quartz grains	
30.5	33.1	Sandy Gravel as at 29.8 to 30.0 ft	
33.1	34.4	Sandy Gravel as above but with silt	

#### Plant North -2096.095, Plant East -5089.217

9/6/2012

		1 fait North -2090.095, 1 fait East -5089.217	9/0/2012
Start	End		
Depth	Depth	Lithology	Hydrogeologic Unit
(ft bgs)	(ft bgs)		
		Sandy Gravel, 10YR7/4 (very pale brown), loose, and	
		moist Gravel is rounded to subangular chart with iron	
34.4	34.7	patina, 0.3- to 1.0-inch diameter. Sand is fine to	
		medium quartz grains	
		Slightly Clayey Silt, 7.5YR7/6 (reddish yellow)	
34.7	38.6	mottled with 7.5YR8/1 (white), soft, moderately	
54.7	50.0	plastic, and moist	
		Silt, 10YR8/2 (very pale brown) with light 10YR7/6	
38.6	44.3	(yellow) laminations, soft, nonplastic, and soft	
		Clay, 10YR7/1 (light gray) with 10YR6/4 (light	
44.3	15 1	yellowish brown) mottling, moderately soft, plastic,	
44.5	45.1		
45.1	46.6		
16.6	515		
46.6	54.5		
		and moist. Sand is very fine grains	
		Sandy Gravel 10VR6/3 (pale brown) loose and	HU3
54.5	54.7		
		-	
54.7	55.0		
55.0	56.9	mottling, lightly consolidated, and moist. Sand is fine	
		quartz grains	
56.9	58.4	light 10YR7/6 (yellow) laminations, moderately soft,	
		slightly plastic, and moist	
59 /	50.0	Sand, 10YR8/1 (white), lightly consolidated, and	
38.4	59.9	moist. Sand is very fine quartz grains	
50.0	(2.4	Silt, 10YR8/3 (very pale brown), soft, nonplastic, and	
59.9	02.4	moist	
		Sand, 10YR8/2 (very pale brown) with 10YR7/6	
62.4	65.8	(yellow) laminations and staining, firm, and moist.	
		Sand is very fine grains	11114
		Gravelly Sand, 10YR8/1 (white), loose, and moist.	HU4
65.8		Sand is fine quartz grains. Gravel is rounded chert with	
	66.0		
45.1 46.6 54.5 54.7 55.0 56.9 58.4 59.9 62.4	46.6 54.5 54.7 55.0 56.9 58.4 59.9 62.4 65.8	and moist Silt, 10YR7/3 (very pale brown), soft, nonplastic, and moist Sand, 10YR8/2 (very pale brown) with some light 10YR7/6 (yellow) laminations, lightly consolidated, and moist. Sand is very fine grains Sandy Gravel, 10YR6/3 (pale brown), loose, and moist. Gravel is subrounded chert with iron patina, 0.3- to 0.5-inch diameter. Sand is very fine quartz grains Sand as at 46.6 to 54.5 ft Sand, 10YR7/6 (yellow) with light 10YR8/1 (white) mottling, lightly consolidated, and moist. Sand is fine quartz grains Slightly Clayey Silt, 10YR8/2 (very pale brown) with light 10YR7/6 (yellow) laminations, moderately soft, slightly plastic, and moist Sand, 10YR8/1 (white), lightly consolidated, and moist. Sand is very fine quartz grains Silt, 10YR8/3 (very pale brown), soft, nonplastic, and moist Sand, 10YR8/2 (very pale brown) with 10YR7/6 (yellow) laminations and staining, firm, and moist. Sand is very fine grains Gravelly Sand, 10YR8/1 (white), loose, and moist.	HU3

Plant North -2095.823, Plant East -5058.897

9/27/2012

di i		1 Iant Worth -2095.025, 1 Iant East -5050.097	9/2//2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	2.5	Gravelly Sand, 2.5YR5/6 (red), dense, and moist. Sand is fine quartz grains. Gravel is subangular to subrounded chert with iron patina, 0.3- to 0.8-inch diameter	FILL
2.5	5.5	Silt, 10YR7/2 (light gray) with green tinge, moderately hard, nonplastic, and moist	
5.5	18.0	Silt, 10YR7/2 (light gray) with 10YR7/6 (yellow) mottling, moderately soft to soft, nonplastic, and moist	
18.0	20.0	Silt with Clay, 10YR8/2 (very pale brown) mottled with 10YR7/1 (light gray), moderately hard to hard, moderately plastic, and moist	HU1
20.0	22.7	Silt with some Clay, 10YR8/2 (very pale brown) mottled with 10YR7/6 (yellow), moderately hard, moderately plastic, and moist	
22.7	23.0	Silty Gravel with Sand, 10YR4/4 (dark yellowish brown) firm and moist. Gravel is subrounded chert	
23.0	23.2	Silt, 10YR5/6 (yellowish brown), soft, nonplastic, and moist	
23.2	24.6	Sand, 10YR8/2 (very pale brown), firm, and moist. Sand is very fine quartz grains	
24.6	25.6	without iron patina, 4-mm to 0.6-inch diameter. Sand is	
25.6	26.6	fine quartz grains Sandy Gravel with Silt, 10YR6/6 (brownish yellow), dense, and moist. Gravel is subangular to subrounded chert without iron patina, 4-mm to 0.6-inch diameter. Sand is fine quartz grains	HU2
26.6	30.8	Silt with Sand, 10YR7/4 (very pale brown) mottled with 10YR8/4 (very pale brown), soft, nonplastic, and moist. Sand is very fine quartz grains	
30.8	31.7	Clay with Silt, 10YR8/2 (very pale brown) with 10YR7/6 (yellow) mottling and strong 2.5YR6/6 (light red) staining at 30.9 to 31.1 ft, moderately hard, moderately plastic, and moist	
31.7	32.6	Silt, 7.5YR8/1 (white) mottled with 7.5YR7/6 (reddish yellow), moderately soft, slightly plastic, and moist	
32.6	33.5	Silt with Sand, 10YR8/2 (very pale brown), moderately soft, nonplastic, and moist. Sand is very fine quartz grains	
33.5	35.2	Sand, 10YR7/8 (yellow), firm, and moist. Sand is fine quartz grains	
35.2	36.5	Silt with little Clay, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white) GRADING DOWN to 10YR7/6 (yellow), soft, moderately plastic, and moist	

### Plant North -2095.823, Plant East -5058.897

9/27/2012

		1 Iant North -2095.825, 1 Iant East -5058.897	
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
36.5	46.1	Silt, 10YR8/2 (very pale brown) with some 10YR7/6 (yellow) laminations, soft, nonplastic, and moist	
46.1	51.5	Sand, 10YR8/2 (very pale brown) with 10YR7/6 (yellow) laminations, firm, and moist. Sand is very fine quartz grains	
51.5	52.5	Silt with little Gravel, 10YR8/2 (very pale brown) with light 2.5YR6/6 (light red) staining, soft, nonplastic, and moist. Gravel is rounded chert without iron patina, 0.4- to 0.6-inch diameter	
52.5	55.1	Gravelly Sand, 10YR8/2 (very pale brown), lightly consolidated, and very moist. Sand is very fine quartz grains. Gravel is rounded to subrounded chert without iron patina, 4-mm to 0.7-inch diameter	
55.1	56.0	Sand, 10YR8/2 (very pale brown) with few 10YR7/6 (yellow) laminations, lightly consolidated, and wet. Sand is very fine quartz grains	HU3
56.0	56.4	Sand GRADING DOWN to poorly sorted Sandy Gravel, 10YR7/3 (very pale brown), firm, and wet.	
56.4	57.1	Silt with some Clay, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white), soft, slightly plastic, and moist	
57.1	58.3	Silt, 10YR8/2 (very pale brown) with 10YR8/6 (yellow) laminations, soft, nonplastic, and moist Sand, 10YR8/2 (very pale brown) with 7.5YR7/4	
58.3	59.3	(pink) laminations, lightly consolidated, and wet. Sand is very fine quartz grains	
59.3	60.9	Silt, 10YR8/2 (very pale brown), moderately soft, nonplastic, and moist	
60.9	63.6	Sand, 10YR8/4 (very pale brown), firm, and wet. Sand is very fine quartz grains	HU4
63.6	64.0	Silt as 59.3 to 60.9 ft	
64.0	64.4	Sandy Gravel, 7.5YR7/6 (reddish yellow), firm, and moist. Gravel is subrounded chert with iron patina, 4- mm to 0.5-inch diameter. Sand is very fine quartz grains	
64.4	67.7	Sand, 10YR7/4 (very pale brown), firm, and wet. Sand is very fine quartz grains	HU5
67.7	68.0	Sandy Gravel, 10YR7/4 (very pale brown), loose, and wet. Gravel is subrounded chert with iron patina, 0.3- to 0.5-inch diameter. Sand is very fine to fine quartz grains	

# Plant North -2096.132, Plant East -4994.506

9/11/2012

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	2.0	Concrete and subgrade gravel	Fill
2.0	5.0	Silt, 10YR6/1 (gray) speckled with 10YR3/1 (very dark gray), firm, and dry to slightly moist	
5.0	10.0	(yellow), firm, nonplastic, and dry to slightly moist	
10.0	11.5	Silt as above but soft and moist	
11.5	15.0	Silt, 10YR7/1 (light gray) with some mottling by 10YR6/4 (light yellowish brown), firm, nonplastic, and slightly moist	
15.0	17.5	Silt, 10YR7/2 (light gray), slightly soft, slightly plastic, and moist	HU1
17.5	18.0	Silty Sand with trace Gravel, 7.5YR6/8 (reddish yellow), slightly loose, and very moist. Sand is fine to medium quartz grains. Gravel is subangular chert with iron patina, 0.8-inch diameter	
18.0	20.0	Clayey Sandy Silt, 7.5YR6/1 (gray) with some mottling by 7.5YR6/8 (reddish yellow), firm to very firm, and slightly moist	
20.0	26.0	Clayey Gravelly Sand, 7.5YR6/8 (reddish brown), firm and slightly moist Sand ranges from fine to	
26.0	28.0	Silty Sand 10YR7/2 (light gray) firm and moist	
28.0	30.5	(reddish yellow) laminations, firm, and moist	HU2
30.5	33.0	Gravelly Silty Sand, 10YR6/8 (brownish yellow), firm, and slightly moist. Sand is fine to coarse, subangular, quartz grains. Gravel is subangular chert, 0.3- to 0.5- inch diameter	
33.0	36.2	Silty Sand 10VR7/1 (light gray) semi firm and very	
36.2	40.0	Silty Clay with little Sand, 7.5YR5/8 (strong brown) with slight mottling by 10YR7/1 (light gray), firm to stiff, very plastic, and slightly moist to moist	
40.0	45.0	Clayey Silt, 10YR8/2 (very pale brown) mottled with 10YR6/8 (brownish yellow), soft to slightly soft, very plastic, and very moist. Trace fine quartz sand	
45.0	47.5	gravel, 0.2-inch diameter	
47.5	52.1	Silty Clayey Sand, 10YR8/2 (very pale brown), soft, and very moist to slightly wet. Sand is very fine quartz grains	HU3
52.1	53.1	Silty Gravelly Sand, 10YR4/6 (dark yellowish brown), firm, and slightly moist. Gravel is subangular chert, 0.3- to 1.2-inch diameter	1105
53.1	55.2	Silty Sand, 10YR5/3 (brown) mottled with 7.5YR6/8 (reddish yellow), firm, and slightly moist.	

211-A-023

#### Plant North -2096.132, Plant East -4994.506

Start Depth	-	Lithology	Hydrogeologic Unit
(ft bgs)	(ft bgs)		
55.2	57.5	Silty Clay with trace Gravel, 10YR7/2 (very pale brown) mottled with 10YR6/8 (brownish yellow)	
55.2	57.5		
		Gravelly Silty Clay, 10YR7/2 (very pale brown)	
57.5	58.0	mottled with 10YR6/8 (brownish yellow). Gravel is	
		white, subrounded, chert	
59.0	(1.0	Silty Sand, 10YR7/1 (light gray), soft, and very moist	
58.0		to wet Sand is very time quartz grains	
61.9	62.5	Sand, 10YR8/3 (very pale brown), firm to slightly	
61.9	62.5	loose, and wet. Sand is fine quartz grains	
62.5	64.9	Sand as above but loose and saturated	HU4
64.9	65.0	Sand and Gravel. Gravel is chert, 0.2- to 0.4-inch	
04.9	03.0	diameter	

# Plant North -2115.892, Plant East -5065.208

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	0.8	Concrete residue from drilling through road bed	
0.8	1.2	Silt, 10YR6/1 (gray), hard, nonplastic, and dry	
1.2	2.1	Gravelly Sand, 5YR7/8 (reddish yellow), loose, and moist. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 0.3- to 0.5-inch diameter	FILL
2.1	3.6	Silt, 10YR7/1 (light gray), moderately soft, nonplastic, and slightly moist	
3.6	18.1	Silt, 10YR8/2 (very pale brown) mottled with 10YR6/6 (brownish yellow), soft, nonplastic, and moist	11111
18.1	21.8	Slightly Clayey Silt with trace Gravel, 10YR7/1 (light gray) with 10YR6/6 (brownish yellow) mottling, moderately hard, slightly to moderately plastic, and moist. Gravel is rounded chert without iron patina, 0.2- inch diameter	HU1
21.8	23.9	Gravelly Sand with Silt, 10YR7/4 (very pale brown), moderately dense/hard, and moist. Sand is 60% fine quartz grains and 40% coarse, subangular, chert grains. Gravel is subangular to rounded chert without iron patina or with light patina, 0.3- to 0.8-inch diameter	
23.9	25.1	Sand, 10YR8/1 (white) with light 10YR7/6 (yellow) staining, firm, and moist. Sand is very fine quartz grains	
25.1	26.6	Gravelly Sand, 10YR7/4 (very pale brown), loose, and moist. Sand is fine quartz grains. Gravel is subrounded to rounded chert with iron patina, 0.5- to 1.0-inch diameter	
26.6		Clayey Silt with Gravel, 10YR7/1 (light gray) with little 10YR7/6 (yellow) mottling, moderately soft, moderately plastic, and moist. Gravel is subrounded to rounded chert without iron patina, 0.4- to 0.6-inch diameter	HU2
30.1	31.0	Silty Gravelly Sand, 7.5YR7/6 (reddish yellow), moderately dense, and moist. Sand is fine quartz grains. Gravel is subangular to subrounded chert with iron patina, 0.2- to 0.4-inch diameter	
31.0	31.4	Sand, 7.5YR6/8 (reddish yellow), lightly consolidated, and moist. Sand is very fine quartz grains	
31.4	32.3	Silt, 10YR8/1 (white), soft, nonplastic, and moist	
32.3	34.7	Silty Sandy Gravel, 10YR7/3 (very pale brown), dense to moderately dense, and moist. Gravel is subrounded to subangular chert with light iron patina, 4-mm to 0.7- inch diameter. Sand is fine quartz grains	

#### Plant North -2115.892, Plant East -5065.208

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
34.7	39.3	Slightly Clayey Silt, 7.5YR7/6 (reddish yellow) mottled with 7.5YR8/1 (white), very soft, moderately plastic, and moist	
39.3	46.3	(yellow) mottling, soft, slightly plastic, and moist	
46.3	48.6	Silty Sand, 10YR8/2 (very pale brown), lightly consolidated, nonplastic, and very moist. Sand is very fine quartz grains	
48.6	51.9	Sand, 10YR8/1 (white) with light 10YR7/6 (yellow) laminations, lightly consolidated, and moist. Sand is very fine quartz grains	HU3
51.9	52.9	Gravelly Sand, 10YR7/6 (yellow), lightly consolidated to loose, and moist. Sand is very fine quartz grains. Gravel is subrounded to subangular chert without iron patina, 0.5- to 0.6-inch diameter	
52.9	56.3	Sand, 10YR7/3 (very pale brown) GRADING DOWN to 10YP7/6 (vallow) with fow 5YP6/8 (raddich	
56.3	59.9	Silt with Sand, 10YR8/2 (very pale brown), very soft, nonplastic, and very moist	
59.9	65.8	Sand, 10YR8/3 (very pale brown) with some 10YR7/6 (yellow) laminations GRADING DOWN to 5YR6/6 (reddish yellow), lightly consolidated to loose, and wet. Sand is very fine quartz grains	HU4
65.8	66.3	Gravel, 10YR8/4 (very pale brown), loose, and wet. Gravel is subrounded to rounded chert with no iron patina or light iron patina, 0.2- to 0.5-inch diameter	HU5
66.3	67.5	Sand with Gravel, 7.5YR7/6 (reddish yellow), loose, and wet. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 0.2- to 0.5-inch diameter	

# Plant North -2114.246, Plant East -5040.02

		1 Iant North -2114.240, 1 Iant East -3040.02	9/10/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	0.4	Concrete residue from drilling through road bed	
0.4	1.1	Gravelly Silt, 10YR7/1 (light gray), loose/soft, nonplastic, and slightly moist. Gravel is subangular limestone, 0.3- to 0.5-inch diameter (dense gravel aggregate/DGA)	FILL
1.1	2.0	Sandy Gravel, 2.5YR5/4 (reddish brown), dense, and moist. Gravel is subrounded chert with iron patina, 0.2- to 0.6-inch diameter. Sand is fine quartz grains	
2.0	3.0	Silt, 10YR7/1 (light gray) with green/blue tinge, moderately soft, nonplastic, and slightly moist	
3.0	17.3	Silt 10VR7/1 (light gray) mottled and stained with	HU1
17.3	21.5	Slightly Clayey Silt, 10YR7/2 (light gray) with heavy mottling by 10YR7/6 (yellow), moderately hard, slightly plastic, and moist	
21.5	22.6	Sandy Gravel, 10YR4/4 (dark yellowish brown),	
22.6	23.0	Sand 5VR5/4 (reddish brown) firm and moist Sand	
23.0	23.5	Silty Clay, 10YR7/3 (very pale brown), moderately soft, moderately plastic, and moist	
23.5	24.1	Sandy Gravel as 21.5 to 22.6 ft	
24.1	24.4	Sand, 10YR4/3 (brown), dense, and moist. Sand is poorly sorted, ranging from fine to coarse, rounded, quartz grains	
24.4	25.2	Sand 10VP8/2 (yery note brown) firm and moist	
25.2	26.5	Silty Sandy Gravel, 10YR7/3 (very pale brown), dense, and moist. Gravel is subangular to subrounded chert with and without iron patina, 0.2- to 0.6-inch diameter. Sand is 40% fine quartz grains and 60% coarse, angular, chert grains	
26.5	27.1	Gravelly Sand, 7.5YR7/6 (reddish yellow), lightly consolidated, and moist. Sand is fine quartz grains. Gravel is subangular to subrounded chert with iron patina, 0.3- to 0.5-inch diameter	HU2
27.1	27.4	Silt with Sand, 7.5YR8/4 (pink), moderately soft, nonplastic, and moist. Sand is fine quartz grains	
27.4	30.0	Silt with Sand, 10YR8/1 (white) with light 10YR7/6 (vallow) mottling GPADING DOWN to 10YP7/1	
30.0	33.5	Sand, 10YR8/2 (very pale brown) with some 10YR7/6 (yellow) laminations, firm, and moist. Sand is very fine quartz grains	

Plant North -2114.246, Plant East -5040.02

		Plain Norui -2114.240, Plain East -3040.02	9/10/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
33.5	34.4	Silty Gravelly Sand with blebs of Clay, 10YR6/4 (light yellowish brown), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert without iron patina, 0.2- to 0.4-inch diameter	
34.4	35.6	Sand, 10YR6/6 (brownish yellow), firm, and moist. Sand is very fine quartz grains	
35.6	40.0	Slightly Clayey Silt, 7.5YR6/6 (reddish yellow) with 7.5YR8/1 (white) mottling, soft, moderately plastic, and moist	
40.0		Slightly Clayey Silt, 10YR8/2 (very pale brown) with light 10YR7/6 (yellow) mottling, soft, moderately plastic, and moist	
42.2		Slightly Clayey Silt, 5YR7/2 (pinkish gray), soft, moderately plastic, and moist	
44.7	45.0	Sand, 7.5YR7/2 (pinkish gray), firm, and moist. Sand is very fine quartz grains	
45.0	49.3	Interbedded slightly Clayey Silt and Silt, 10YR8/1 (white) with some 10YR7/6 (yellow) mottling, soft, slightly to moderately plastic, and moist	
49.3	55.0	Sand, 10YR8/1 (white), lightly consolidated, and moist. Sand is very fine quartz grains	HU3
55.0	56.6	Sand with trace Gravel, 10YR8/4 (very pale brown) with 10YR6/6 (brownish yellow) laminations from 55.6 to 56.6 ft, firm, and moist. Sand is very fine quartz grains. Gravel is subrounded to rounded chert without iron patina, 0.2- to 0.4-inch diameter	
56.6	57.9	Silty Clay, 7.5YR7/2 (pinkish gray) with 7.5YR6/6 (reddish yellow) mottling, moderately hard, moderately plastic, and moist	
57.9		Silt, 10YR8/2 (very pale brown) with 10YR7/6 (yellow) staining and laminations, soft, nonplastic, and moist	
61.9	65.0	Sand, 10YR8/1 (white) with 10YR7/6 (yellow) and 10YR6/6 (brownish yellow) laminations, firm, and very moist. Sand is very fine quartz grains	HU4
65.0	65.2	Gravelly Sand, 10YR8/3 (very pale brown), loose, and wet. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 0.2- to 0.4-inch diameter	HU5

# Plant North -2131.264, Plant East -5088.823

9/7/2012

<b>G</b> ( )	<b>F</b> '	1 Iant North -2131.204, 1 Iant East -3000.023	
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	1.0	Silty Gravel, 10YR7/1 (light gray), loose, and slightly moist. Gravel is subangular to subrounded limestone (dense gravel aggregate/DGA), 4 mm- to 0.3-inch diameter	
1.0	1.7	Silty Gravel as 0.0 to 1.0 ft but moist	Fill
1.7		Silty Sandy Gravel, 2.5YR5/4 (reddish brown), dense, and moist. Gravel is subrounded chert with iron patina, 4 mm- to 0.4-inch diameter. Sand is fine quartz grains.	
2.1	3.0	slightly moist	
3.0	15.0	Silt, 10YR7/2 (light gray) mottled with 10YR6/6 (brownish yellow), soft, nonplastic, and moist	
15.0	16.3	Silt as 3.0 to 15.0 ft but colored 10YR7/3 (very pale brown)	HU1
16.3	22.3	Clayey Silt with some Gravel, 10YR7/4 (very pale brown) with little 10YR7/1 (light gray) mottling GRADING DOWN to 10YR6/2 (light brownish gray), moderately hard, slightly plastic, and moist. Gravel is rounded to subrounded chert without iron patina, 0.2- inch diameter	
22.3	23.0	Gravelly Sand, 7.5YR6/6 (reddish yellow), firm to dense, and moist. Sand is predominately fine quartz grains but includes some coarse, rounded, quartz grains. Gravel is subrounded to subangular chert with iron patina, 0.2- to 0.4-inch diameter	
23.0	24.2	Silt, 10YR8/2 (very pale brown) with 10YR6/6 (brownish yellow) mottling/laminations, moderately soft, slightly plastic, and moist	
24.2		Sandy Gravel, 7.5YR6/6 (reddish yellow), dense, and moist. Gravel is subrounded to subangular chert with iron patina, 0.2- to 0.8-inch diameter. Sand is fine quartz grains	
26.0	29.8	Interbedded Clayey Silt, moderately soft, plastic, and moist AND Sandy Silt, soft, nonplastic, and moist	HU2
29.8	30.6	Sand 10VP8// (very pale brown) lightly consolidated	
30.6	33.5	Gravelly Sand, 7.5YR7/6 (reddish yellow), firm, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert with iron patina, 4 mm- to 0.3-inch diameter	
33.5	36.0	Gravelly Sand as 30.6 to 33.5 ft but with Silt	
36.0		Slightly Clayey Silt, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white), very soft, slightly plastic, and moist	

211-A-026

#### Plant North -2131.264, Plant East -5088.823

9/7/2012

· · · · ·		F Iant Notul -2151.204, F Iant East -5088.825	3/1/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
44.2	45.0	Silt, 7.5YR7/2 (pinkish gray) with 7.5YR7/4 (pink) mottling, soft, plastic, and moist	
45.0	49.9	Slightly Clavey Silt as 36.0 to 44.2 ft. Includes little	
49.9	51.5	Sand, 7.5YR8/4 (pink), loosely consolidated, and moist. Sand is fine quartz grains	
51.5	51.8	Sand, 7.5YR8/4 (pink), firm, and moist. Sand is	
51.8	52.7	Sand, 10YR8/2 (very pale brown), lightly consolidated, and wet. Sand is very fine quartz grains	
52.7	53.1	Gravelly Sand, 10YR8/4 (very pale brown), loose, and moist. Sand is a mix of fine quartz grains and coarse, subangular, chert grains. Gravel is rounded to subrounded chert without iron patina, 4 mm- to 0.4- inch diameter	HU3
53.1	55.1	Sand, 10YR8/2 (very pale brown), lightly consolidated, and very moist. Sand is very fine quartz grains	
55.1	55.5	Sand, 10YR8/2 (very pale brown) with some 10YR7/6 (yellow) staining, firm, and moist. Sand is fine quartz grains	
55.5	56.4	Sandy Gravel, 10YR7/4 (very pale brown), loose, and moist. Gravel is rounded to subangular chert without iron patina, 0.2- to 0.8-inch diameter. Sand is equal portions of fine and medium, rounded, quartz grains	
56.4	61.4	Silt, 10YR8/3 (very pale brown) with light 10YR7/6 (yellow) laminations, soft, slightly plastic, and moist	
61.4	66.1	Sand, 10YR7/6 (reddish yellow), loose, and wet. Sand is fine quartz grains	
66.1	66.5	Sandy Gravel, 10YR7/4 (very pale brown), loose, and moist. Gravel is subrounded to subangular chert with iron patina, 0.2- to 1.0-inch diameter. Sand is fine quartz grains	HU4

Plant North -2125.771, Plant East -4995.046

9/11/2012

		Plant Norui -2125.771, Plant East -4995.040	9/11/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	1.7	Silty dark brown soil over Gravel and Sand, white to medium gray. Gravel is limestone. Sand is coarse grains.	Fill
1.7	5.0	Silt, 10YR8/1 (white), soft, and dry	
5.0	8.5	Silt, 10YR7/1 (light gray) speckled with 10YR8/4 (very pale brown), firm, and moist	
8.5	10.0	plastic, and very moist	
10.0	12.5	Permeameter sample - no description	
12.5	15.0	Silt, 10YR7/1 (light gray), soft, nonplastic, and moist	
15.0	16.1	Silt with Sand, 10YR6/6 (brownish yellow), soft, nonplastic, and moist. Sand is fine quartz grains	HU1
16.1	17.5	Silty Gravelly Sand, 10YR5/4 (yellowish brown), moderately loose, and moist. Sand is 70% fine quartz grains and 30% coarse, subrounded, chert grains. Gravel is subrounded chert with iron patina, 0.3-inch diameter	
17.5	19.6	Silt with Clay, 10YR6/2 (light brownish gray), hard, slightly to moderately plastic, and slightly moist	
19.6	20.0	Sandy Gravel, 10YR6/6 (brownish yellow), dense, and moist. Gravel is rounded to subrounded chert without iron patina, 0.3- to 1.0-inch diameter. Sand is fine quartz grains	
20.0	21.0	Silt 10VR5/3 (brown) very soft moderately plastic	
21.0	22.0	Sandy Gravel, 7.5YR6/6 (reddish yellow), dense, and maint Gravel is subrounded to rounded chart without	
22.0	24.5	Permeameter sample - no description	
24.5	25.0	Sand Gravel as 21.0 to 22.0 ft but gravel ranges up to 0.8-inch diameter	
25.0	26.2	Sandy Gravel, 10YR5/4 (yellowish brown), dense, and moist Gravel is subangular to subrounded chert with	
26.2	27.2	Silt with Clay and some Gravel, 10YR7/1 (light gray), hard, moderately plastic, and slightly moist. Gravel is subrounded to rounded chert without iron patina, mostly 0.3-inch diameter but some 0.8- to 1.0-inch diameter	
27.2	28.6	Silty Gravelly Sand, 7.5YR7/6 (reddish yellow), dense, and moist. Sand is fine quartz grains. Gravel is rounded to subrounded chert without iron patina, 0.3- to 0.5- inch diameter	HU2
28.6	28.9	Silt, 7.5YR7/6 (reddish yellow) mottled with 7.5YR8/1 (white), soft, nonplastic, and moist	

211-A-027

# Plant North -2125.771, Plant East -4995.046

9/11/2012

Start	End		
Depth (ft bgs)	Depth (ft bgs)	Lithology	Hydrogeologic Unit
28.9	30.5	Slightly Clayey Silt, 10YR7/1 (light gray) with 10YR7/6 (yellow) mottling, hard, slightly plastic, and slightly moist	
30.5	32.0	Silty Sand, 10YR7/8 (yellow) with 10YR7/1 (light gray) mottling, firm/moderately soft, (nonplastic), and moist. Sand is very fine quartz grains	
32.0	34.1	Silty Sandy Gravel, 7.5YR6/6 (reddish yellow), dense, and moist. Gravel is subangular to subrounded chert without iron patina or with light iron patina, 4 mm- to 0.5-inch diameter. Sand is 80% fine quartz grains and 20% coarse, subangular, chert grains	
34.1	35.0	Sandy Gravel, 7.5YR6/8 (reddish yellow), dense, and moist. Gravel is subrounded to rounded chert without iron patina, 0.3- to 0.5-inch diameter. Sand is 80% fine quartz grains and 20% coarse, subangular, chert grains	
35.0	35.3	SLOUGH: Silt, 10YR5/4 (yellowish brown), very soft, nonplastic, and very moist	
35.3	37.5	Sandy Gravel as 34.1 to 35.0 ft but gravel ranges up to 0.8-inch diameter	
37.5	40.0	Permeameter sample - no description	No Description
40.0	43.9	Silt, 10YR8/3 (very pale brown) with little 10YR8/1 (white) mottling, soft, moderately plastic, and moist	
43.9		Sand, 10YR8/1 (white) with 10YR7/6 (yellow) laminations, firm, and moist. Sand is very fine quartz grains	
44.7	47.4	Silt, 10YR8/2 (very pale brown) with 10YR7/6 (yellow) mottling, soft, nonplastic, and moist	
47.4	49.7	Silt with some Clay, 7.5YR7/4 (pink) with 7.5YR8/1 (white) mottling, moderately soft to soft, plastic, and moist	HU3
49.7	53.2	Sand with some Gravel, 7.5YR7/4 (pink) with 7.5YR8/1 (white) mottling, lightly consolidated, and moist. Sand is fine quartz grains. Gravel is rounded to subrounded chert without iron patina, 0.3- to 0.5-inch diameter	
53.2	60.1	Sand interbedded with Clayey Silt, 10YR8/1 (white) with 10YR7/6 (yellow) laminations and staining and some 2.5YR7/8 (light red) blebs, moist. Sand is lightly consolidated, fine, quartz grains. Clayey Silt is soft and moderately plastic	
60.1	66.2	Sand, 10YR8/4 (very pale brown) with some 10YR7/6 (yellow) laminations, loose, and wet. Sand is fine quartz grains	

#### 211-A-027

	Plant North -2125.771	Plant East -4995.046
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Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
66.2		Sandy Gravel, 10YR6/6 (brownish yellow), loose, and wet. Gravel is subrounded to subangular chert with iron patina, 4 mm- to 1.0-inch diameter. Sand is 85% fine quartz grains and 15% medium, rounded, quartz grains	HU4

# Plant North -2048.759, Plant East -5231.166

9/24/2012

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	0.4	Silt, 10YR6/3 (pale brown), soft, nonplastic, and slightly moist. Zone of roots and humic material	
0.4	3.7	Silt, 10YR8/2 (very pale brown) with little 10YR6/6 (brownish yellow) mottling, soft (crumbles to powder), nonplastic, and moist GRADING DOWN to dry	HU1
3.7	16.4	Silt, 10YR8/2 (very pale brown) mottled with 10YR7/6 (yellow), soft, slightly plastic, and moist	
16.4	18.0	Gravelly Sand, 7.5YR6/4 (light brown), dense, and moist. Sand is fine quartz grains. Gravel is subangular chert with iron patina, 0.3- to 0.6-inch diameter	
18.0	18.7	Sand, 7.5YR6/4 (light brown), firm, and moist. Sand is fine to medium, subrounded, quartz grains	
18.7	20.2	Silt, 7.5YR7/1 (light gray) mottled with 7.5YR7/6 (reddish yellow), moderately soft, moderately plastic, and moist	
20.2	20.5	Gravelly Sand, 7.5YR7/3 (pink), firm, and moist. Sand is fine quartz grains. Gravel is subrounded chert without iron patina, 0.3-inch diameter	
20.5	20.9	Sand 10VR7// (nink) firm and moist Sand is very	
20.9	21.4	Gravelly Sand as 20.2 to 20.5 ft	
21.4	23.1	Sandy Gravel, 7.5YR7/3 (pink), dense, and moist. Gravel is subangular chert without iron patina, 0.3-to 0.6-inch diameter. Sand is 80% fine quartz grains and 20% coarse, subrounded, chert grains. Note: 20.5 to 23.1 ft is a coarsening downward sequence	
23.1	23.6	Silty Sand with little Gravel, 10YR7/3 (very pale brown), firm, and moist. Sand is very fine quartz grains. Gravel is subrounded to rounded chert without iron patina, 0.4- to 0.5-inch diameter	HU2
23.6	25.1	Sand with Gravel, 10YR6/3 (pale brown), dense, and moist. Sand is 80% fine quartz grains and 20% coarse to very coarse, subrounded, chert grains. Gravel is subrounded chert without iron patina, 0.3-inch diameter	
25.1	25.6	Sand with Gravel as 23.6 to 25.1 ft but sand is medium, subrounded, quartz grains	
25.6	28.3	Sand with little Gravel, 7.5YR7/4 (pink), firm, and moist. Sand is fine quartz grains. Gravel is subangular chert with iron patina, 0.3- to 0.5-inch diameter	
28.3	28.6	Sandy Gravel, 7.5YR7/4 (pink), dense, and moist. Gravel is subrounded to rounded chert without iron patina, 4 mm - to 0.4-inch diameter	

# Plant North -2048.759, Plant East -5231.166

9/24/2012

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
28.6	31.4	Sand with some Gravel, 10YR7/4 (very pale brown), firm, and moist. Sand is very fine quartz grains. Gravel is subrounded chert without iron patina, 0.6 to 0.8-inch diameter	
31.4	35.0	Sandy Gravel, 10YR6/6 (brownish yellow), dense, and moist. Gravel is subrounded to subangular chert without iron patina, 4 mm- to 1.0-inch diameter. Sand is 80% fine quartz grains and 20% coarse to very coarse, subrounded, chert grains	
35.0	35.5	Silty Clay, 7.5YR7/3 (pink), soft, plastic, and moist	
35.5	35.7	Silty Sand, 7.5YR7/3 (pink), lightly consolidated, and moist. Sand is fine quartz grains	
35.7	36.6	Slightly Clayey Silt, 7.5YR8/2 (pinkish white), soft, plastic, and moist	
36.6	36.8	Silty Sand as 35.5 to 35.7 ft	
36.8	39.9	Silt, 2.5YR7/1 (light reddish gray), soft, moderately plastic, and moist	
39.9	43.1	Silt with Sand, 10YR8/2 (very pale brown) with 10YR7/6 (yellow) laminations, soft, nonplastic, and moist. Sand is very fine quartz grains	
43.1	44.6	Silt, 10YR8/2 (very pale brown) with 10YR7/6 (yellow) laminations, moderately hard, slightly to moderately plastic, and moist	
44.6	46.0	Clay with Silt, 7.5YR6/6 (reddish yellow) mottled with 7.5YR8/1 (white), moderately soft, moderately plastic, and moist	
46.0	48.0	Silt, 10YR7/4 (very pale brown) with some 10YR8/1 (white) mottling, soft, nonplastic, and moist	HU3
48.0	50.9	Sand, 10YR7/4 (very pale brown) mottled with 10YR8/1 (white), firm, and moist. Sand is very fine quartz grains	
50.9	52.4	Silt with little Clay, 7.5YR7/4 (pink) with light 7.5YR7/1 (light gray) mottling, soft, plastic, and moist	
52.4	54.4	Silty Sand, 10YR7/6 (yellow) with 10YR8/1 (white) mottling, firm, and moist. Sand is very fine quartz grains	
54.4	55.5	Sandy Gravel, 7.5YR6/6 (reddish yellow), firm, and moist. Gravel is rounded to subangular chert without iron patina, 0.3- to 1.0-inch diameter. Sand is very fine quartz grains	
55.5	55.9	Sand, 7.5YR6/6 (reddish yellow), firm, and moist. Sand is very fine quartz grains	
55.9	60.0	Silt, 10YR8/2 (very pale brown) with 10YR7/6 (yellow) laminations, soft, slightly plastic, and moist	
60.0	61.3	Sand, 10YR8/1 (white), loose to lightly consolidated, and wet. Sand is very fine quartz grains	

#### 211-A-028

Plant North -2048.759, Plant East -5231.166

9/24/2012

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
61.3		Gravelly Sand, 10YR8/1 (white), firm, and wet. Sand is fine quartz grains. Gravel is rounded to subrounded chert without iron patina, 0.4- to 1.0-inch diameter	HU4
62.1	62.5	Gravelly Sand, 10YR7/6 (yellow), loose, and wet. Sand is fine to medium, rounded, quartz grains. Gravel is subangular to subrounded chert with iron patina, 0.8- to 1.0-inch diameter	

# Plant North -2066.748, Plant East -5214.094

· · · · ·		Fiant Norui -2000.748, Fiant East -3214.074	9/23/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	0.4	Silt, 10YR5/2 (grayish brown), soft (noncohesive), nonplastic, and dry. Zone or roots and humic material	
0.4	3.8	Silt, 10YR8/2 (very pale brown) with little 10YR7/6 (yellow) mottling, moderately hard, nonplastic, and dry	HU1
3.8	16.3	(yellow), soft, slightly plastic, and moist	
16.3	17.0	Sand, 10YR7/4 (very pale brown), firm, and moist. Sand is very fine quartz grains	
17.0	19.2	is rounded to subrounded chert with iron patina, 0.3- to 0.5-inch diameter	
19.2	21.7	Silt, 10YR8/2 (very pale brown) mottled with10YR7/4 (very pale brown), moderately hard, nonplastic to slightly plastic, and moist	
21.7	23.3	Silt with some Gravel and little Clay, 10YR8/2 (very pale brown) mottled with10YR7/4 (very pale brown), moderately hard, plastic, and moist. Gravel is rounded chert without iron patina, 0.3- to 0.5-inch diameter	
23.3	25.5	Gravelly Sand, 7.5YR6/4 (light brown), dense, and moist. Sand is 70% fine quartz grains and 30% coarse to very coarse, subrounded, chert grains. Gravel is subrounded to subangular chert with iron patina, 4 mm- to 0.4-inch diameter	
25.5	28.9	Sand GRADING DOWN to Sand with Gravel, 10YR8/2 (very pale brown) with 10YR7/6 (yellow) staining, lightly consolidated to firm, and moist. Sand is fine quartz grains. Gravel is subrounded to rounded chert with iron patina, 0.4- to 0.5-inch diameter	HU2
28.9	29.6	Silt with some Clay and little Gravel, 10YR7/2 (light gray), soft, plastic, and moist. Gravel is subangular chert with iron patina, 0.4- to 0.6-inch diameter	
29.6	29.9	Sandy Silt with little Gravel, 10YR7/2 (light gray), soft, nonplastic, and moist. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 0.3- to 0.5-inch diameter	
29.9	32.6	Gravelly Sand, 7.5YR7/4 (pink), dense, and moist. Sand is 70% fine quartz grains and 30% coarse to very coarse, subrounded, chert grains. Gravel is subrounded to subangular chert with iron patina, mostly 0.3-inch diameter but some 0.7- to 1.0-inch diameter	
32.6	34.0	Sand, 7.5YR7/4 (pink), lightly consolidated, and moist. Sand is very fine quartz grains	

#### Plant North -2066.748, Plant East -5214.094

		Plant North -2000.748, Plant East -5214.094	9/25/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
34.0	35.3	subrounded to subangular chert with iron patina, 0.3-to 0.6-inch diameter	
35.3	40.0	Silt, 10YR8/2 (very pale brown) mottled with 10YR7/4 (very pale brown), soft, plastic, and moist	
40.0	42.5	Silt with Sand, 7.5YR8/3 (pink) with some 7.5YR7/6 (reddish yellow) laminations, soft, moderately plastic, and moist. Sand is very fine quartz grains	
42.5	48.1	Silt with little Clay, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white), soft, moderately plastic to plastic, and moist	
48.1	49.9	Sand with Silt, 10YR7/4 (very pale brown) mottled with 10YR8/2 (very pale brown), lightly consolidated, and moist. Sand is very fine quartz grains	HU3
49.9	52.1	Sand, 10YR8/1 (white) mottled with 10YR7/6 (yellow), firm, and moist. Sand is very fine to fine quartz grains	nos
52.1	56.9	Sandy Gravel, 10YR8/2 (very pale brown), lightly consolidated, and moist. Gravel is subrounded chert without iron patina, 0.3- to 0.6-inch diameter. Sand is fine quartz grains	
56.9	60.0	Clay with Silt, 10YR8/2 (very pale brown) with 10YR8/4 (very pale brown) laminations, soft, plastic, and moist	
60.0	62.3	Silt, 10YR8/2 (very pale brown), soft, moderately plastic, and moist	
62.3	63.1	Sand, interbedded 10YR8/1 (white) and 10YR8/4 (very pale brown), firm, and moist. Sand is very fine quartz grains	
63.1	63.6	moist	HU4
63.6	64.0	Sand, 10YR7/6 (yellow), loose, and wet. Sand is very fine quartz grains	
64.0	65.0	Sandy Gravel, 10YR7/6 (yellow), stained 10YR6/2 (light brownish gray) at 64.8 to 65.0 ft (manganese?), loose, and wet. Gravel is subangular to subrounded chert with iron patina, 0.3- to 0.8-inch diameter. Sand is 80% fine quartz grains and 20% coarse, subrounded, chert grains	HU5

		F Ialit North -2027.302, F Ialit East -3204.028	9/23/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	5.0	No recovery	Missing
5.0	18.6	Silt, 10YR7/2 (light gray) with 10YR7/4 (very pale brown) mottling and a few 10YR3/1 (very dark gray) blebs (manganese?), soft, nonplastic, and moist	
18.6	21.2	Clay with Silt and some Gravel, 10YR7/2 (light gray) with 10YR6/8 (brownish yellow) mottling, moderately hard, plastic, and moist. Gravel is subrounded to subangular chert without iron patina, 0.4- to 0.5-inch diameter	HU1
21.2	22.7	Silty Sand with Gravel, 10YR7/2 (light gray), firm, and moist. Sand is very fine quartz grains. Gravel is subrounded to subangular chert without iron patina, 0.3- to 0.5-inch diameter	
22.7	24.0	Sandy Gravel, 7.5YR6/6 (reddish yellow), dense, and moist. Gravel is subrounded to subangular chert without iron patina, 0.3- to 0.5-inch diameter. Sand is 70% fine quartz grains and 30% coarse to very coarse, subangular, chert grains. Suspect DNAPL presence based on PID trend and distinct smell	
24.0	25.1	Silty Gravelly Sand, 7.5YR6/6 (reddish yellow), firm, and moist. Sand is fine quartz grains. Gravel is subrounded chert without iron patina, 0.4- to 0.7-inch diameter	
25.1	26.2	Sand with little Gravel, 7.5YR7/4 (pink), lightly consolidated, and moist. Sand is fine quartz grains. Gravel is rounded chert without iron patina, 0.3-inch diameter	
26.2	27.6	Interbedded Silt and Sand, 10YR8/2 (very pale brown) with 10YR7/6 (yellow) laminations. Silt is soft, nonplastic, and moist. Sand is very fine quartz grains, lightly consolidated, and moist	HU2
27.6	28.9	Sand, 10YR8/2 (very pale brown) mottled with 10YR6/6 (brownish yellow), lightly consolidated, and moist. Sand is 90% fine quartz grains and 10% coarse, rounded, chert grains	
28.9	31.0	Gravelly Sand, 10YR7/4 (very pale brown), dense, and moist. Sand is 80% fine quartz grains and 20% coarse to very coarse, subangular, chert gains. Gravel is subrounded to subangular chert without iron patina, 0.3- to 0.5-inch diameter	
31.0	31.8	Sand with little Gravel, 10YR8/1 (white), firm, and moist. Sand is fine quartz grains. Gravel is rounded chert without iron patina, 0.4- to 0.6-inch diameter	
31.8	32.7	Silty Gravelly Sand as 24.0 to 25.1 ft	

#### Plant North -2027.362, Plant East -5204.628

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
32.7	33.9	Silt GRADING DOWN to Silt with Sand, 7.5YR7/1 (light gray) mottled with 7.5YR6/6 (reddish yellow), soft, moderately plastic to nonplastic, and moist. Sand is very fine quartz grains	
33.9	35.5	Gravelly Sand as 28.9 to 31.0 ft	
35.5	37.5	Silt, 10YR7/3 (very pale brown), soft, slightly plastic, and moist	
37.5	39.9	Silt with Sand, 10YR8/2 (very pale brown), soft, nonplastic, and moist. Sand is very fine quartz grains	
39.9	45.0	Clayey Silt, 7.5YR7/6 (reddish yellow) mottled with 7.5YR8/1 (white), moderately hard, moderately plastic, and moist	
45.0	48.4	Silt, 7.5YR7/6 (reddish yellow) with little 7.5YR8/1 (white) mottling, moderately hard, slightly plastic, and moist	
48.4	49.5	Silt, 7.5YR8/1 (white) with 7.5YR7/8 (reddish yellow) mottling, soft, nonplastic, and moist	
49.5	50.5	Sand, 10YR8/2 (very pale brown), firm to dense, and moist. Sand is very fine quartz grains	
50.5	53.1	Slightly Clayey Silt, 7.5YR8/2 (pinkish white) with some 7.5YR7/8 (reddish yellow) mottling, soft, plastic, and moist	HU3
53.1	54.9	Sand with little Gravel, 10YR8/1 (white), lightly consolidated, and moist. Sand is 90% fine quartz grains and 10% coarse, rounded, chert grains. Gravel is rounded chert without iron patina, 0.5- to 1.0-inch diameter	
54.9	55.4	Sandy Gravel, 10YR8/1 (white), loose, and moist. Gravel is subangular to subrounded chert without iron patina, 0.3- to 1.0-inch diameter. Sand is fine quartz grains	
55.4	56.4	Sand, 10YR8/4 (very pale brown), loose, and wet. Sand is very fine quartz grains	
56.4	57.8	Silt, 7.5YR8/4 (pink) with some 7.5YR7/6 (reddish yellow) laminations, soft, slightly plastic, and moist	
57.8	61.5	Sand is very fine quartz granis	
61.5	65.0	Gravelly Sand, 10YR7/6 (yellow), loose, and wet. Sand is fine to medium, rounded, quartz grains. Gravel is subrounded to subangular chert with iron patina, 0.4- to 0.7-inch diameter	HU4

# Plant North -2136.286, Plant East -5040.074

9/26/2012

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	0.5	Sand with Gravel, 2.5YR6/8 (light red), loose, and moist. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 0.3-inch diameter	Fill
0.5	4.6	Silt, 10YR7/1 (light gray) with bluish tinge, soft, nonplastic, and moist (suspected fill material)	
4.6	20.0	(yellow), soft, nonplastic, and moist	
20.0	20.7	Clay with some Silt and some Gravel, 10YR7/2 (light gray) with some 10YR7/6 (yellow) mottling, moderately hard, plastic, and moist. Gravel is subrounded chert without iron patina, 0.3- to 0.4-inch diameter	HU1
20.7	22.7	Silty Gravelly Sand, 7.5YR5/6 (strong brown) GRADING DOWN to 7.5YR7/6 (reddish yellow), dense, and moist. Sand is 80% fine quartz grains and 20% coarse, subangular, chert grains. Gravel is subangular to subrounded chert without iron patina, 0.3- to 1.0-inch diameter	
22.7	24.2	Silt, 10YR7/1 (light gray), moderately soft, moderately plastic, and moist	
24.2	25.6	Gravelly Sand, 10YR8/2 (very pale brown), firm, and moist. Sand is very fine quartz grains. Gravel is subrounded chert without iron patina, 0.3- to 0.8-inch diameter	
25.6	28.1	Sandy Gravel with some Silt, 7.5YR6/4 (light brown), dense, and moist. Gravel is subrounded to subangular chert without iron patina, 0.3- to 0.6-inch diameter. Sand is 60% fine quartz grains and 40% coarse-to-very- coarse, subangular, chert grains	HU2
28.1	30.8	Sand with some Gravel, firm-to-dense, and moist. Sand is very fine quartz grains. Gravel is subrounded chert with iron patina, 0.3- to 0.5-inch diameter	
30.8	32.5	Silty Gravel with Sand, 7.5YR6/4 (light brown), dense, and moist. Gravel is subangular to subrounded chert without iron patina, 0.3- to 1.0-inch diameter. Sand is 80% fine quartz grains and 20% coarse, rounded, chert grains	
32.5	33.3	Silt with some Gravel and little Clay, 10YR6/4 (light yellowish brown) mottled with 10YR8/1 (white), moderately soft, slightly plastic, and moist	
33.3	36.2	Silty Sand with Gravel, 10YR7/4 (very pale brown), firm, and moist. Sand is very fine quartz grains. Gravel is subrounded chert without iron patina, 0.4- to 0.7- inch diameter	
36.2	38.3	Clavey Silt 7 5VR7/4 (nink) with 7 5VR7/2 (ninkish	

# Plant North -2136.286, Plant East -5040.074

9/26/2012

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
38.3	42.5	Silt GRADING DOWN to Silt with Sand, 7.5YR7/1 (light gray) with 7.5YR7/4 (pink) mottling, soft, nonplastic, and moist. Sand is very fine quartz grains	
42.5	44.1	Sand, 10YR8/2 (very pale brown) with some 10YR7/6 (yellow) laminations, firm, and moist. Sand is very fine quartz grains	
44.1	45.3	Silt with little Clay, 10YR7/4 (very pale brown) with 10YR7/1 (light gray) mottling, soft, plastic, and moist	
45.3	48.2	Silt, 10YR7/4 (very pale brown) with mottling by 10YR7/6 (yellow) and 2.5YR6/6 (light red) (2.5YR6/6 prominent from 46.8 to 47.4 ft), soft, slightly plastic, and moist	
48.2	51.0	Sand, 10YR7/6 (yellow), firm, and moist. Sand is very fine quartz grains GRADING Down to fine quartz grains. Note: 0.05-ft horizon of 10YR3/1 (very dark gray) staining at 48.8 ft (manganese?)	
51.0	53.4	Sand with Gravel interbedded with Sandy Gravel, 10YR8/3 (very pale brown), firm, and moist. Sand is very fine quartz grains. Gravel ranges from subangular chert with 0.3-inch diameter to rounded chert without iron patina, 0.5-inch diameter	HU3
53.4	54.2	Sand, 10YR8/2 (very pale brown) with some 10YR7/6 (yellow) laminations, firm, and wet. Sand is very fine quartz grains	
54.2	55.1	Sand with Gravel, 10YR7/3 (very pale brown), firm-to- dense, and moist. Sand is 80% fine quartz grains and 20% coarse, subrounded, chert trains. Gravel is subrounded chert without iron patina, 4 mm- to 0.3- inch diameter	
55.1	55.6	Sand as at 53.4 to 54.2 ft but without laminations. Sand is very fine quartz grains	
55.6	56.2	Sand with Gravel as at 54.2 to 55.1 ft	
56.2	56.6	moist. Sand is very fine quartz grains	
56.6	57.0	hard, moderatery plastic, and moist	
57.0	58.1	Silt, 10YR8/3 (very pale brown), moderately soft, slightly plastic, and moist	
58.1		Sand, 10YR8/1 (white) with 10YR7/6 (yellow) laminations, slightly consolidated, and moist. Sand is very fine quartz grains	
59.9	60.7	Clayey Silt as at 56.6 to 57.0 ft	
60.7	66.0	Sand, 10YR8/4 (very pale brown), lightly consolidated to loose, and wet. Sand is very fine quartz grains. Note: 65.0 to 66.0 ft appears to be 'flowing sand' - no structure.	HU4

### 211-A-031

		Plant North -2136.286, Plant East -5040.074	9/26/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
66.0	66.0	Subrounded chert Gravel without iron patina, 0.4- to 1.0-inch diameter	HU5

#### Plant North -1999.905, Plant East -5031.516

9/28/2012

r		Plant North -1999.903, Plant East -3031.310	9/28/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	0.2	Silt, 10YR4/1 (dark gray), soft (loose), nonplastic, and moist. Zone of roots and humic material	
0.2	1.5	Silt, 10YR6/3 (pale brown), soft, nonplastic, and moist	
1.5	4.0	Silt, 10YR7/2 (light gray), soft, nonplastic, and moist	
4.0	5.5	Silt, 10YR7/1 (light gray), moderately hard, nonplastic, and dry	HU1
5.5	19.8	Silt, 10YR7/2 (light gray) with 7.5YR7/6 (reddish yellow) mottling, soft, nonplastic, and moist	1101
19.8	20.6	Silty Sand with Gravel, 10YR7/4 (pink), dense, and moist. Sand is fine quartz grains. Gravel is subangular to rounded chert, with and without iron patina, 0.3- to 0.5-inch diameter	
20.6	21.1	Silty Clay, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white), soft, plastic, and moist	
21.1	22.6	Silty Sandy Gravel, 7.5YR7/4 (pink) with little 7.5YR8/1 (white) mottling, dense, and moist. Gravel is subangular to rounded chert with iron patina, 4 mm- to 0.8-inch diameter. Sand is 70% fine quartz grains and 30% coarse, rounded, chert grains	
22.6	23.8	Silt, 10YR8/1 (white) mottled with 7.5YR7/6 (reddish yellow) GRADING DOWN to 10YR8/1 (white), moderately soft, moderately plastic, and moist	
23.8	25.0	Sand, 10YR8/3 (very pale brown) mottled with 10YR8/1 (white), firm, and moist. Sand is very fine quartz grains	
25.0	25.2	Silt with Gravel, 7.5YR7/1 (light gray), soft, plastic, and moist. Gravel is subrounded chert with iron patina, 0.4- to 1.0-inch diameter	
25.2	25.6	Sand 10VR8/1 (very nale brown) firm and moist	
25.6	30.5	Silt, 10YR8/1 (white) with 10YR7/6 (yellow) mottling and staining, soft, nonplastic, and moist	HU2
30.5	31.6	Silt with little Gravel, 10YR7/1 (light gray), soft, nonplastic, and moist. Gravel is subrounded chert without iron patina, 1.0-inch diameter	
31.6	33.2	Gravelly Sand, 10YR8/3 (very pale brown) mottled with 10YR8/1 (white), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert with iron patina, 0.3- to 0.6-inch diameter	
33.2	34.3	Sandy Gravel with Silt, 10YR7/4 (very pale brown) GRADING DOWN to 10YR7/2 (light gray), dense, and moist. Gravel is subangular chert with iron patina, 4 mm- to 1.0-inch diameter. Sand is fine quartz grains	

#### Plant North -1999.905, Plant East -5031.516

9/28/2012

Start       End       Lithology       Hydrogeologic         0 pepth       0 pepth       Lithology       Hydrogeologic         (ft bgs)       (ft bgs)       Sand with Gravel, 10YR7/4 (very pale brown), loose, and wet. Sand is very fine quartz grains. Gravel is subrounded chert with iron patina, 0.3- to 0.7-inch diameter       Hydrogeologic	Unit
(ft bgs)       (ft bgs)         34.3       35.1         Sand with Gravel, 10YR7/4 (very pale brown), loose, and wet. Sand is very fine quartz grains. Gravel is subrounded chert with iron patina, 0.3- to 0.7-inch diameter	Unit
34.3 35.1 Sand with Gravel, 10YR7/4 (very pale brown), loose, and wet. Sand is very fine quartz grains. Gravel is subrounded chert with iron patina, 0.3- to 0.7-inch diameter	
34.3 35.1 and wet. Sand is very fine quartz grains. Gravel is subrounded chert with iron patina, 0.3- to 0.7-inch diameter	
34.3 35.1 subrounded chert with iron patina, 0.3- to 0.7-inch diameter	
subrounded chert with iron patina, 0.3- to 0.7-inch diameter	
diameter	
Clay with some Silt, 7.5YR7/4 (pink) GRADING	
35.1 37.9 DOWN to 7.5YR8/1 (white) mottled with 7.5YR7/4	
(pink), soft, plastic, and moist	
37.9 38.3 Sand, 10YR7/3 (very pale brown), firm, and moist.	
Sand is very fine quartz grains	
Silt with some Clay, 7.5YR7/4 (pink) mottled with	
38.3 47.6 7.5YR8/1 (white), moderately hard, slightly to	
moderately plastic, and moist	
Silt, 10YR7/6 (yellow) with some 10YR8/1 (white)	
47.6 50.0 mottling soft to moderately soft, popplastic, and moist	
HUS	
Silt with Clay, 10YR8/1 (white) with some 7.5YR7/4	
50.0 (pink) mottling GRADING DOWN to 7.5YR7/4 (pink)	
with 10YR8/1 (white) mottling, moderately hard,	
plastic, and moist	
Sandy Silt, 7.5YR7/6 (reddish yellow), soft, nonplastic,	
54.6 55.0 and moist. Contains trace, subrounded, chert gravel	
without iron patina, 1.0-inch diameter	
Sand, 7.5YR7/6 (reddish yellow) with frequent	
55.0 57.4 mottling by 7.5YR4/1 (dark gray), firm, and moist.	
Sand is very fine quartz grains	
Groupl with Sand 7 5VD6/4 (light brown) dance and	
Gravel with Sand, 7.5YR6/4 (light brown), dense, and	
57.4 57.9 moist. Gravel is subangular to angular chert with iron	
patina, 4 mm- to 1.1-inch diameter. Sand is 80% fine	
quartz grains and 20% coarse, angular, chert grains HU4	
57.9 58.2 Sand as 55.0 to 57.4 ft	
Sandy Gravel, 7.5YR7/4 (pink), loose, and wet. Gravel	
58.2 60.0 is subangular chert with iron patina, 0.4- to 0.7-inch	
diameter. Sand is fine quartz grains	

# Plant North -2094.976, Plant East -5216.53

10/1/2012

I		1 Iant 1 (01th 20) 1.970, 1 Iant East 5210.55	10/1/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	0.0	Fill: Silt, 10YR4/1 (dark gray), soft, nonplastic, and	
0.0	0.2	moist. Zone of roots and humic material	
		Fill: Silty Gravel, 10YR6/2 (light brownish gray),	
0.2	0.6	loose, and moist. Gravel is subangular limestone, 0.3-	
		inch diameter	Fill
		Fill: Silty Sandy Gravel, 2.5YR5/8 (red), dense, and	
0.6	3.0	moist. Gravel is subangular to subrounded chert with	
0.0	5.0	iron patina, 4 mm- to 0.4-inch diameter. Sand is fine	
		quartz grains	
3.0	4.2	Silt, 10YR7/1 (light gray), soft, nonplastic, and moist	*****
1.0	15.0	Silt, 10YR7/2 (light gray) mottled with 10YR7/4 (very	HU1
4.2	15.3	pale brown), soft, nonplastic, and moist	
15.2	16.0	Silty Sand, 10YR8/2 (very pale brown), dense, and dry.	
15.3	16.0	Sand is very fine quartz grains	
16.0	19.0	Sand, 7.5YR6/6 (reddish yellow), firm, and moist.	
10.0	17.0	Sand is fine quartz grains	
		Silty Gravel, 7.5YR6/4 (light brown), dense, and moist.	
19.0	19.7	Gravel is subangular to angular chert with iron patina,	
		0.3- to 0.7-inch diameter	
19.7	20.0	Clayey Silt, 10YR7/2 (light gray), moderately hard,	
20.0	20.4	slightly plastic, and moist	
20.0		Silt with Sand. Sand is very fine quartz grains	
20.6	21.0	Clayey Silt as 19.7 to 20.0 ft	
		Silty Gravelly Sand, 7.5YR6/4 (light brown), dense,	
21.0	25.0	and moist. Sand is 80% fine quartz grains and 20%	
21.0	25.0	coarse, subrounded, chert grains. Gravel is subrounded	
		to subangular chert with iron patina, 0.3- to 0.7-inch	
		diameter Sand, 10YR8/2 (very pale brown), firm, and moist.	
25.0	26.5	Sand is very fine quartz grains	
		Sand with Gravel, 10YR8/2 (very pale brown), firm,	
		and moist Sand is very fine quartz grains. Gravel is	
26.5	27.0	subrounded chert with iron patina, 0.4- to 0.8-inch	
		diameter	
27.0	07.4	Sand, 7.5YR7/6 (reddish yellow), very firm, and moist.	
27.0	27.4	Sand is fine quartz grains	HU2
		Silt with little Sand, 10YR7/3 (very pale brown),	
27.4	28.0	moderately soft, moderately plastic, and moist. Sand is	
		coarse, rounded, chert grains	
		Sandy Gravel, 7.5YR7/4 (pink), dense, and moist.	
28.0	30.1	Gravel is subrounded to subangular chert with and	
		without iron patina, 0.3- to 0.7-inch diameter	
30.1	30.5	Sand, 7.5YR7/6 (reddish yellow), firm, and moist.	
		Sand is fine quartz grains	
		Sandy Gravel, 10YR7/4 (very pale brown), dense, and	
30.5	30.9	moist. Gravel is subrounded to rounded chert with and	
		without iron patina, 0.4- to 0.8-inch diameter	
			I

Plant North -2094.976, Plant East -5216.53

10/1/2012

· · · · ·		1 Iant North -2094.976, 1 Iant East -3210.33	10/1/2012
Start Depth (ft bgs)	(ft bgs)	Lithology	Hydrogeologic Unit
30.9	31.8	Sand as 30.1 to 30.5 ft	
31.8	32.5	Sandy Gravel, 10YR6/6 (brownish yellow), dense, and moist. Gravel is subrounded to subangular chert, 0.3- to 0.8-inch diameter. Sand is 90% fine quartz grains and 10% coarse, rounded, chert grains	
32.5	34.3	Sand, 7.5YR7/6 (reddish yellow), firm, and moist. Sand is fine quartz grains	
34.3	35.3	Sandy Gravel as 31.8 to 32.5 ft	
35.3	35.5	Sand as 32.5 to 34.3 ft	
35.5	35.8	Sandy Gravel as 31.8 to 32.5 ft	
35.8	42.4	Silt, 10YR8/2 (very pale brown) with few 10YR7/6 (yellow) laminations, soft, nonplastic to slightly plastic, and moist	
42.4	44.4	Silt with Sand, 10YR8/2 (very pale brown) with few 7.5YR7/6 (reddish yellow) laminations, soft, nonplastic, and moist. Sand is very fine quartz grains	
44.4	48.3	Sand, 10YR8/2 (very pale brown) with few 7.5YR7/6 (reddish yellow) laminations, firm, and moist. Sand is very fine quartz grains	
48.3	53.3	Sand with Silt interbeds, 10YR8/3 (very pale brown) mottled with 10YR8/2 (very pale brown), soft, nonplastic to moderately plastic, and moist. Sand is very fine quartz grains	HU3
53.3	54.9	Sand, 10YR8/1 (white), firm, and moist. Sand is fine quartz grains	
54.9	57.5	Gravelly Sand, 10YR8/1 (white) with 2.5YR8/3 (pink) mottling, firm, and moist. Sand is fine quartz grains. Gravel is subangular to rounded chert without iron patina, 0.3- to 1.0-inch diameter	
57.5	57.9	Sand, 10YR8/3 (very pale brown), firm, and moist. Sand is very fine quartz grains	
57.9	61.6	Slightly Clayey Silt, 7.5YR8/1 (white) with 7.5YR7/4 (pink) laminations, soft, moderately plastic, and moist	
61.6	64.1	Sand, 10YR8/3 (very pale brown), loose, and wet. Sand is very fine quartz grains	
64.1	65.1	Silt, 10YR8/1 (white), soft, plastic, and moist	HU4
65.1	66.8	Sand, 10YR8/1 (white), loose, and wet. Sand is fine quartz grains	
66.8	67.5	Sandy Gravel, 10YR7/4 (very pale brown), loose, and moist. Gravel is subangular to subrounded chert with	HU5

# Plant North -2105.517, Plant East -5240.028

10/2/2012

~ T		Thank 1401th 2103.317, Thank East 3210.020	
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	0.5	Silt, 10YR5/2 (grayish brown), soft, nonplastic, and moist. Zone of roots and humic material	
0.5	1.8	Silty Gravel, 10YR4/1 (dark gray), loose, and moist. Gravel is subangular limestone (0.3- to 0.8-inch diameter (dense gravel aggregate/DGA)	Fill
1.8	3.5	Silt, 10YR7/2 (light gray) with some 7.5YR7/6 (reddish yellow) mottling, soft, nonplastic, and moist	
3.5	5.1	Silt, 10YR8/2 (very pale brown), hard, nonplastic, and dry	
5.1	12.6	Silt, 10YR7/1 (light gray) with some 7.5YR7/6 (reddish yellow) mottling, soft, nonplastic, and moist	HU1
12.6	14.0	nonplastic, and moist	
14.0	15.5	Silt with Sand, 10YR8/1 (white), moderately hard to hard, nonplastic, and dry. Sand is very fine quartz grains	
15.5	18.6	Sand with some Gravel, 7.5YR6/6 (reddish yellow), lightly consolidated, and moist. Sand is fine quartz grains. Gravel is rounded chert without iron patina, 0.8- to 1.0-inch diameter	
18.6	23.5	Silt with Clay and some Gravel, 10YR7/1 (light gray),	
23.5	24.3	Gravelly Sand, 7.5YR7/6 (reddish yellow), dense, and moist. Sand is 90% fine quartz grains and 10% coarse, rounded, chert grains. Gravel is subangular to subrounded chert with iron patina, 0.3- to 0.4-inch diameter	
24.3	26.4	Silty Sand with some Gravel, 10YR7/3 (very pale brown), firm to dense, and moist. Sand is very fine quartz grains. Gravel is subrounded to subangular chert without iron patina, 0.3- to 0.4-inch diameter	
26.4	26.9	Gravelly Sand, 7.5YR6/6 (reddish yellow), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert without iron patina, 0.3- to 0.4-inch diameter	
26.9	27.4	Sand, 7.5YR7/6 (reddish yellow), firm, and moist. Sand is fine quartz grains	
27.4	27.9	Clayey Silt with Sand, 10YR7/3 (very pale brown) mottled with 7.5YR7/4 (pink), moderately hard, moderately to slightly plastic, and moist. Sand is fine quartz grains	HU2
27.9	28.2	Silt with Clay and some Gravel as at 18.6 to 23.5 ft	
28.2	28.4	Gravelly Sand as at 26.4 to 26.9 ft	
28.4	28.7	Silty Sand with some Gravel as at 24.3 to 26.4 ft	

# Plant North -2105.517, Plant East -5240.028

10/2/2012

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
28.7	29.7	Silt with some Sand, 10YR7/6 (yellow) mottled with 10YR8/1 (white), soft, nonplastic, and moist. Sand is very fine quartz grains	
29.7	30.9	Gravelly Sand, 7.5YR7/6 (reddish yellow), dense, and moist. Sand is 80% fine quartz grains and 20% coarse, subrounded, chert grains. Gravel is subrounded to rounded chert without iron patina, 0.3- to 0.4-inch diameter	
30.9	32.2	Sand, 10YR7/4 (very pale brown) finely mottled with 10YR8/1 (white), firm, and moist. Sand is fine quartz grains	
32.2	34.5	Silty Sandy Gravel, 7.5YR6/4 (light brown), dense, and moist. Gravel is subrounded to rounded chert without iron patina, 0.3- to 0.8-inch diameter. Sand is 70% fine quartz grains and 30% coarse, rounded, chert grains	
34.5	35.2	Gravelly Sand, 7.5YR6/6 (reddish yellow), dense, and moist. Sand is 80% fine quartz grains and 20% coarse, subangular, chert grains. Gravel is subrounded chert without iron patina, 0.4- to 1.0-inch diameter	
35.2	43.2	Silt, 7.5YR8/1 (white) mottled with 7.5YR6/6 (reddish yellow) GRADING DOWN to 10YR7/3 (very pale brown), soft, nonplastic, and moist	
43.2	49.4	Sand, 10YR8/2 (very pale brown) with some 10YR7/6 (yellow) staining, firm, and moist. Sand is very fine quartz grains	
49.4	49.9	Sand, 10YR7/6 (yellow) mottled with 10YR8/1 (white), firm, and moist. Sand is fine quartz grains	
49.9	50.3	Sand, 10YR8/3 (very pale brown) GRADING DOWN to 10YR8/6 (yellow), firm, and moist. Sand is very fine quartz grains	
50.3	51.6	Silt with Sand, 10YR8/1 (white) GRADING DOWN to 10YR7/8 (yellow), soft, nonplastic, and moist. Sand is very fine quartz grains	
51.6	54.7	Clay, 7.5YR7/4 (pink) GRADING DOWN to 10YR7/3 (very pale brown), soft, plastic, and moist	11112
54.7	55.0	Silty Sand with some Gravel, 10YR7/3 (very pale brown), firm, and moist. Sand is 90% fine quartz grains and 10% coarse, subrounded, chert grains. Gravel is subrounded chert without iron patina, 0.3- to 0.5-inch diameter	HU3
55.0	55.4	Sand is the quartz grants	
55.4	57.0	Gravelly Sand, 10YR8/2 (very pale brown), dense, and moist. Sand is fine quartz grains. Gravel is rounded to subrounded chert without iron patina, 0.3- to 0.5-inch diameter	

211-A-035

#### Plant North -2105.517, Plant East -5240.028

10/2/2012

		Fight 100101 2105.517, Fight East 5210.020	10/2/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
57.0	58.3	Sand, 7.5YR8/6 (reddish yellow), loose, and wet. Sand is very fine quartz grains	
58.3	63.0	Silt, 10YR8/1 (white) with 10YR7/6 (yellow) laminations GRADING DOWN to massive 10YR8/1 (white), soft, plastic, and moist	
63.0	65.3	Sand, 10YR8/3 (very pale brown), lightly consolidated, and very moist. Sand is very fine quartz grains	
65.3	66.3	Silt, 10YR8/2 (very pale brown) with some 10YR7/6 (yellow) laminations, soft, plastic, and moist	HU4
66.3	66.5	Sand, 7.5YR7/8 (reddish yellow), firm, and moist. Sand is very fine quartz grains	

#### Plant North -2051.946, Plant East -5261.363

10/3/2012

		Plant North -2051.940, Plant East -5201.305	10/3/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	0.6	Silt, 10YR3/1 (very dark gray), soft, nonplastic, and moist. Zone of roots and humic material	
0.6	1.8	Silt, 10YR6/3 (pale brown), moderately hard, slightly plastic, and moist	
1.8	4.6	10YR <sup>7</sup> /6 (yellow), hard, nonplastic, and dry	
4.6	14.5	Silt, 10YR7/2 (light gray) with little 10YR7/6 (yellow) mottling, soft, nonplastic, and moist	
14.5	14.8	Sand, 10YR7/8 (yellow), firm to dense, and moist. Sand is very fine quartz grains	HU1
14.8	16.5	Silt as 4.6 to 14.5 ft	ner
16.5	18.1	Silt with thin Sand interbeds, 10YR8/2 (very pale brown) GRADING DOWN to 7.5YR6/6 (reddish yellow). Silt is moderately soft, slightly plastic, and moist. Sand is fine quartz grains, firm, and moist	
18.1	20.1	Silt, 7.5YR7/4 (pink), soft, slightly plastic, and moist	
20.1	20.3	Silt with some Sand, 10YR7/3 (very pale brown), hard, nonplastic, and dry. Sand is very fine quartz grains	
20.3	25.5	Sand with Gravel and some Silt, 7.5YR7/3 (pink) with some 7.5YR3/1 (very dark gray) staining (manganese?), dense, and moist. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 0.3- to 0.4-inch diameter	
25.5	25.8	Sand, 10YR8/2 (very pale brown), firm, and moist. Sand is fine quartz grains	
25.8	26.1	Sand with Gravel and some Silt as 20.3 to 25.5 ft	
26.1	26.7	Sand, 10YR7/4 (very pale brown), firm, and moist. Sand is fine quartz grains	
26.7	27.1	Silty Sand with some Gravel, 10YR7/4 (very pale brown), firm, and moist. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 4 mm- to 0.4-inch diameter	HU2
27.1	30.0	Silt, 10YR7/3 (very pale brown), mottled with 10YR8/1 (white), soft, plastic, and moist	
30.0	32.5	Disturbed soil (Sandy Silt with some Gravel)	
32.5		Gravelly Sand, 10YR5/6 (yellowish brown), firm, and moist. Sand is 80% fine quartz grains and 20% coarse, subangular to subrounded, chert grains. Gravel is subrounded chert with iron patina(?), 0.3- to 1.0-inch diameter	
35.5	42.9	Silt, 7.5YR8/1 (white) mottled with 7.5YR6/6 (reddish yellow) and 7.5YR8/6 (reddish yellow), soft, moderately plastic, and moist	
42.9	43.7	Sandy Silt, 10YR8/2 (very pale brown) with 10YR7/6 (yellow) laminations, soft, nonplastic, and moist. Sand is very fine quartz grains	

#### Plant North -2051.946, Plant East -5261.363

10/3/2012

		Plant North -2051.940, Plant East -5201.303	10/3/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
43.7	47.4	Clayey Silt, 10YR8/2 (very pale brown) with 7.5YR7/4 (pink) laminations, moderately hard, plastic, and moist	
47.4	49.9	Silt, 10YR8/2 (very pale brown) mottled with 7.5YR6/4 (light brown) and with slight 2.5YR7/6 (light red) staining, soft, plastic, and moist	
49.9		Sand, 10YR8/1 (very pale brown) with 10YR7/6 (yellow) laminations, firm, and moist. Sand is very fine quartz grains	HU3
52.1	53.2	Silt, 10YR7/3 (very pale brown), soft to moderately soft, plastic, and moist	
53.2	55.0	Sand, 10YR8/3 (very pale brown), firm, and moist. Sand is fine quartz grains	
55.0	56.0	Sand with Gravel, 10YR7/8 (yellow), firm, and moist. Sand is 80% fine quartz grains and 20% coarse-to-very- coarse, subrounded, chert grains. Gravel is subrounded chert without iron patina, 4 mm- to 0.4-inch diameter	
56.0	60.9	Interbedded Silt, 10YR8/1 (white), soft, moderately plastic, and moist AND very fine quartz Sand, 10YR8/1 (white) with few 10YR7/6 (yellow) laminations, lightly consolidated, and moist-to-wet	
60.9	62.3	Sand, 10YR8/1 (white), tinged with 10YR7/6 (yellow) at base, firm, and moist. Sand is very fine quartz grains	
62.3	62.5	Sand with Gravel, 10YR7/6 (yellow), loose, and wet. Sand is fine to medium, rounded, quartz grains. Gravel is subrounded chert with iron patina, 0.4- to 0.8-inch diameter	HU4

Plant North -2607.698, Plant East -5240.899

10/9/2012

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Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	4.0	Gravelly Sand, 2.5YR6/6 (light red), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert with iron patina, 0.3- to 0.7-inch diameter	FILL
4.0	5.0	Silt, 10YR7/2 (light gray), soft, nonplastic, and moist	HU1
5.0	8.0	Permeameter sample - no description	NO DESCRIPTION
8.0	10.3	Silt as 4.0 to 5.0 ft	
10.3	13.7	fine quartz grains	HU1
13.7	15.0	Silt with little Clay and Gravel, 10YR7/2 (light gray) stained with 5YR5/4 (reddish brown), moderately hard, slightly plastic, and moist	
15.0	18.0	Permeameter sample - no description	NO DESCRIPTION
18.0	19.0	Gravelly Sand, 10YR7/4 (very pale brown), dense, and moist. Sand is fine quartz grains. Gravel is subangular to subrounded chert without(?) iron patina, 0.3- to 0.7-inch diameter	
19.0	20.0	Gravelly Sand with Silt, 10YR7/4 (very pale brown), dense, and moist. Sand is fine quartz grains. Gravel is	
20.0	23.1	Silt with some Sand and Gravel, 10YR6/4 (light yellowish brown), moderately hard, nonplastic, and moist. Sand is fine quartz grains. Gravel is subrounded chert without iron patina, 0.3- to 1.0-inch diameter	
23.1	25.1	Gravelly Sand, 10YR6/4 (light yellowish brown), dense and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert	HU2
25.1	28.4	Silt, 10YR8/3 (very pale brown) mottled with 10YR8/1 (white), soft, nonplastic to slightly plastic, and moist	
28.4	33.0	Gravelly Sand, 10YR7/3 (very pale brown), dense, and moist. Sand is fine quartz grains. Gravel is subangular to subrounded chert with and without iron patina, 0.3- to 0.9-inch diameter	
33.0	33.4	Sand with little Gravel, firm, and moist. Sand is fine quartz grains. Gravel is subrounded chert without(?) iron patina, 0.3- to 0.5-inch diameter	
33.4	35.0	Gravelly Sand, 10YR7/6 (yellow), dense, and moist.	
35.0	38.0	Permeameter sample - no description	NO DESCRIPTION
38.0		Silt, 10YR7/1 (light gray), soft, nonplastic, and moist	

211-B-001

#### Plant North -2607.698, Plant East -5240.899

10/9/2012

		Flaint North -2007.098, Flaint East -5240.899	10/9/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
39.0	40.0	Silt with Sand, 10YR7/4 (very pale brown), moderately soft, nonplastic, and moist. Sand is very fine quartz grains	
40.0	47.0	Silt, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white) GRADING DOWN to 10YR7/4 (very pale brown), moderately soft, moderately plastic, and moist	HU3
47.0	52.4	Silt with little Sand, soft, nonplastic to slightly plastic, and moist. Sand is very fine quartz grains	nes
52.4	56.5	Silt with little Clay, 7.5YR7/3 (pink) mottled with 7.5YR8/1 (white), moderately hard, slightly plastic, and moist	
56.5	59.4	Silt with Sand, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white), soft, nonplastic, and moist. Sand is very fine quartz grains	
59.4	61.6	Sand, 10YR8/4 (very pale brown), firm, and moist. Sand is fine quartz grains	
61.6	62.3	Sand, 10YR8/2 (very pale brown), firm, and moist. Sand is fine quartz grains	HU4
62.3	62.5	Sand, 7.5YR6/8 (reddish yellow), firm, and moist. Sand is fine quartz grains	

Plant North -2608.457, Plant East -5201.467

Start Depth	-	Lithology	Hydrogeologic Unit
(ft bgs)	(ft bgs)		
0.0		Gravelly Sand, 2.5YR5/6 (red), dense, and moist. Sand is 85% fine quartz grains and 15% coarse, subrounded to subangular, chert grains. Gravel is subrounded to subangular chert with iron patina, 4-mm to 0.6-inch diameter	FILL
3.5	13.4	Silt, 10YR7/1 (light gray) with 10YR7/4 (very pale brown) mottling, soft, nonplastic, and moist	
13.4	14.1	Sand, 10YR7/3 (very pale brown), firm, and moist. Sand is fine quartz grains	
14.1	15.9	Silt with little Clay, 10YR7/3 (very pale brown) with little 10YR7/6 (yellow) mottling, moderately hard, slightly plastic, and moist	HU1
15.9	17.0	Silt with little Clay and Gravel, 10YR7/3 (very pale brown) GRADING DOWN to 7.5YR6/6 (reddish yellow), moderately hard, slightly plastic, and moist. Gravel is rounded to subrounded chert without iron patina, 0.4- to 0.6-inch diameter	пот
17.0	17.5	Silt with some Clay, 10YR7/2 (light gray), soft, moderately plastic, and moist	
17.5		Gravelly Sand, 7.5YR7/4 (pink), dense, and moist. Sand is 70% fine quartz grains and 30% coarse to very coarse, subrounded, chert grains. Gravel is subangular to subrounded chert with iron patina, 4-mm to 0.5-inch diameter	
19.1	19.5	Sand, 10YR7/6 (yellow), dense, and moist. Sand is fine quartz grains	
19.5	20.3	Gravelly Sand as 17.5 to 19.1 ft	
20.3	21.2	Silt with little Clay and Gravel as 15.9 to 17.0 ft	
21.2		Sand with some Gravel, 7.5YR6/4 (light brown), dense, and moist. Sand is 70% fine quartz grains and 30% coarse to very coarse, subrounded, chert grains. Gravel is subrounded chert with iron patina, 0.3- to 0.5-inch diameter	HU2
23.0	27.3	Silt with some Clay, 10YR7/1 (light gray) mottled with 10YR7/8 (yellow), soft, plastic, and moist	
27.3	28.4	Sand, 10YR7/8 (yellow), firm, and moist. Sand is fine quartz grains	
28.4	31.3	Silty Sand with Gravel, 7.5YR7/3 (pink), dense, and moist. Sand is fine to medium quartz grains. Gravel is subangular to subrounded chert with and without iron patina, 0.4- to 1.0-inch diameter	
31.3	33.3	Sand with some Gravel, 10YR7/4 (very pale brown) GRADING DOWN to 10YR8/1 (white), firm, and moist. Sand is fine to medium quartz grains. Gravel is subrounded chert without iron patina, 0.3- to 0.6-inch diameter	
33.3	38.5	Silt with Sand, 10YR8/3 (very pale brown), very soft, nonplastic, and moist. Sand is very fine quartz grains	

# Plant North -2608.457, Plant East -5201.467

		Plant North -2008.457, Plant East -5201.467	10/10/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
38.5	40.0	Silt with Sand, 10YR7/6 (yellow) mottled with 10YR8/1 (white), soft, nonplastic, and moist. Sand is fine quartz grains	
40.0	42.4	7 5YR7/4 (pink) soft moderately plastic and moist	
42.4	44.8	Silt, 10YR8/1 (white) mottled with 10YR7/8 (yellow), soft, nonplastic, and moist	
44.8	47.4	Silt with little Clay, 7.5YR7/4 (pink) with 7.5YR8/1 (white) mottling, moderately hard, moderately plastic, and moist	HU3
47.4	50.4	Silt with Clay, 10YR7/4 (very pale brown) mottled with 10YR8/2 (very pale brown), moderately hard, moderately plastic, and moist	
50.4	51.0	Sand, 10YR7/3 (very pale brown), firm, and moist. Sand is fine quartz grains	
51.0	52.5	Silt, 7.5YR8/1 (white) mottled with 7.5YR7/4 (pink), soft, moderately plastic, and moist	
52.5	56.0	Silt with little Clay, 7.5YR7/4 (pink) with little 7.5YR8/1 (white) mottling, moderately hard, slightly plastic, and moist	
56.0	59.0	Silt with some Clay, 7.5YR8/1 (white) mottled with 7.5YR7/3 (pink), soft, moderately plastic, and moist	
59.0	60.5	Sand, 10YR8/2 (very pale brown) with 10YR7/8 (yellow) laminations, lightly consolidated, and moist. Sand is very fine quartz grains	
60.5		Sand, 10YR8/2 (very pale brown) with some 2.5YR7/4 (light reddish brown) and 7.5YR7/8 (reddish yellow) laminations, firm, and moist. Sand is fine quartz grains	
63.0	64.5	Sand with little Gravel, 10YR8/2 (very pale brown), loose, and wet. Sand is fine quartz grains. Gravel is rounded chert without iron patina, 0.3- to 0.4-inch diameter	HU4
64.5	65.0	Sand, 10YR8/1 (white) with 7.5YR7/8 (reddish yellow) staining, loose, and wet. Sand is fine quartz grains	

Plant North -2607.365, Plant East -5181.15

<b>G</b> 4- 4	<b>D</b> . 1	Than 10101 2007.505, Than East 5101.15	10/10/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	3.0	Fill: Gravelly Sand, 2.5YR5/6 (red), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert with iron patina, 0.3- to 0.8-inch diameter	Fill
3.0	13.6	Silt, 10YR7/1 (light gray) with 10YR7/6 (yellow) mottling, soft, nonplastic, and moist	
13.6	15.9	Silt with little Clay and little Gravel, 10YR7/2 (light gray), moderately hard, slightly plastic, and moist. Gravel is subrounded chert without iron patina, 0.4- to 0.5-inch diameter	HU1
15.9	16.9	Sandy Gravel with little Silt, 7.5YR7/2 (pinkish gray), dense, and moist. Gravel is subangular to rounded chert with and without iron patina, 4 mm- to 0.7-inch diameter. Sand is fine quartz grains	
16.9	17.8	Sand with little Gravel, 10YR7/3 (very pale brown), firm, and moist. Sand is fine quartz grains. Gravel is subangular to subrounded chert without(?) iron patina, 0.4- to 0.6-inch diameter	
17.8	20.1	Sandy Silt with little Gravel and little Clay, 10YR7/2 (light gray), moderately hard, nonplastic, and moist. Sand is fine quartz grains. Gravel is subangular to angular chert without iron patina, 0.4- to 0.8-inch diameter	
20.1	22.3	Gravelly Sand with little Silt, 7.5YR6/4 (light brown), dense, and moist. Sand is fine quartz grains. Gravel is subrounded chert without(?) iron patina, 0.3- to 0.6-inch diameter	
22.3	22.9	Sand, 10YR7/8 (yellow), firm, and moist. Sand is fine quartz grains	
22.9	27.0	Silt with Sand, 10YR8/4 (very pale brown) mottled with 10YR8/1 (white), soft, nonplastic, and moist. Sand is very fine quartz grains	HU2
27.0	27.4	Sand, 10YR7/6 (yellow), firm, and moist. Sand is fine quartz grains	
27.4	28.9	Sand with little Gravel, 10YR7/4 (very pale brown) GRADING DOWN to 10YR8/1 (white), firm, and moist. Sand is fine quartz grains. Gravel is subrounded to rounded chert with and without iron patina, 0.3- to 0.8-inch diameter	
28.9	30.4	Sand with Gravel, 10YR7/3 (very pale brown), dense, and moist. Sand is 75% fine quartz grains and 25% coarse, subrounded, chert grains. Gravel is subrounded to subangular chert without(?) iron patina, 0.3- to 0.4- inch diameter	
30.4	31.4	Sand, 10YR7/6 (yellow), firm to dense, and moist. Sand is fine quartz grains	

#### Plant North -2607.365, Plant East -5181.15

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
31.4	33.0	Sand with Gravel, 7.5YR6/4 (light brown), dense, and moist. Sand is fine to medium quartz grains. Gravel is subrounded to subangular chert with iron patina, 0.3- to 0.4-inch diameter	
33.0	35.9	Silt, 7.5YR7/3 (pink) GRADING DOWN to 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white), soft, nonplastic, and moist	
35.9	36.7	Silt with Sand, 7.5YR7/4 (pink), soft, nonplastic, and moist. Sand is very fine quartz grains	HU3
36.7	38.8	Sand, 10YR7/4 (very pale brown), firm, and moist. Sand is very fine quartz grains	
38.8	40.1	Sand, 10YR7/6 (yellow), firm, and moist. Sand is fine quartz grains	
40.1	42.5	Silt with little Clay, 7.5YR7/4 (pink) with 7.5YR8/1 (white) mottling, moderately soft, moderately plastic, and moist	
42.5	47.0	Silt with some Clay, 7.5YR7/3 (pink) mottled with 7.5YR8/1 (white) GRADING DOWN to 7.5YR7/4 (pink), moderately hard, slightly plastic, and moist	
47.0	51.0	Silt with Sand, 10YR7/4 (very pale brown) with some 7.5YR8/1 (white) mottling, soft, nonplastic, and moist. Sand is very fine quartz grains	
51.0	54.0	Silt with little Clay, 7.5YR8/1 (white) mottled with 7.5YR7/4 (pink), soft to moderately soft, moderately plastic, and moist	
54.0	56.3	Silt, 7.5YR6/6 (reddish yellow) mottled with 7.5YR8/1 (white), moderately hard, nonplastic, and moist	
56.3	58.5	Silt with Sand, 10YR8/2 (very pale brown) with 10YR7/6 (yellow) laminations, moderately soft, nonplastic, and moist. Sand is very fine quartz grains	
58.5	60.0	Sand, 10YR8/2 (very pale brown) GRADING DOWN to 7.5YR8/4 (pink), firm, and moist. Sand is very fine quartz grains	HU4

Plant North -2607.187, Plant East -5143.33

10/11/2012

		1 Iant North -2007.187, 1 Iant East -5145.55	10/11/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	3.6	Fill: Gravelly Sand, 2.5YR5/6 (red), dense, and moist. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 0.3- to 0.5-inch diameter	Fill
3.6	7.5	Silt, 10YR7/1 (light gray) with some 10YR7/6 (yellow) mottling, soft, nonplastic, and moist	
7.5	10.0	Permeameter Sample - No Description	
10.0	12.5	Silt as 3.6 to 7.5 ft	
12.5	13.3	Sand, 10YR8/4 (very pale brown), dense, and moist. Sand is very fine quartz grains	
13.3	14.7	Silt, 10YR7/4 (very pale brown), soft, slightly plastic, and moist	
14.7	15.0	Silt with little Gravel and little Clay, 10YR7/2 (light gray) mottled with 7.5YR6/6 (reddish yellow), moderately hard, slightly to moderately plastic, and moist. Gravel is subangular chert without iron patina, 0.3-inch diameter	HU1
15.0	15.5	Slough: Silt, 10YR7/2 (light gay), very soft, nonplastic, and moist	
15.5	17.2	Silt with little Clay and little Gravel, 7.5YR7/2 (pinkish gray) with 7.5YR7/6 (reddish yellow) staining, moderately hard, moderately plastic, and moist. Gravel is subrounded to subangular chert without iron patina, 0.3- to 1.0-inch diameter	
17.2	17.5	Sand with Gravel, 7.5YR7/4 (pink), firm, and moist. Sand is fine quartz grains. Gravel is subrounded chert with(?) iron patina, 0.4- to 0.6-inch diameter	
17.5	20.0	Permeameter Sample - No Description - Appeared	
20.0	21.1	Silt with little Clay and little Gravel as 15.5 to 17.2 ft	
21.1	23.8	Sand with Gravel, 7.5YR7/4 (pink), dense, and moist. Sand is fine quartz grains. Gravel is subangular to subrounded chert without(?) iron patina, 0.3- to 0.5-inch diameter	
23.8	24.2	Sand, 7.5YR7/4 (pink), firm, and moist. Sand is fine to medium quartz grains	
24.2	24.6	Silt with some Gravel, 10YR7/1 (light gray) with 7 5YR7/6 (reddish vellow) staining soft plastic and	
24.6	26.0	Sand, 10YR8/2 (very pale brown) GRADING DOWN to 10YR8/4 (very pale brown), dense, and moist. Sand is fine quartz grains	HU2
26.0	26.5	Gravelly Sand with Silt, 10YR7/6 (yellow), dense, and moist. Sand is fine quartz grains. Gravel is subrounded chert without iron patina, 0.3- to 0.6-inch diameter	

Plant North -2607.187, Plant East -5143.33

10/11/2012

		F failt Noftil -2007.187, F failt East -5145.55	10/11/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
26.5	28.5	Silt with Sand, 10YR7/4 (very pale brown) mottled with 10YR8/1 (white), soft, nonplastic, and moist. Sand is fine quartz grains	
28.5	30.0	Sand with Gravel, 10YR8/3 (very pale brown), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert without iron patina, 4 mm- to 0.6-inch diameter	
30.0	31.9	Sand with Gravel and some Silt, 7.5YR6/6 (reddish yellow). Sand is 80% fine to medium quartz grains and 20% coarse, subrounded, chert grains. Gravel is subrounded to subangular chert without(?) iron patina, 4 mm- to 0.5-inch diameter	
31.9	32.7	Silt with Clay, 7.5YR6/6 (reddish yellow), moderately soft, plastic, and moist	
32.7	42.4	Silt, 7.5YR6/6 (reddish yellow) GRADING DOWN to 10YR7/6 (yellow) and then to 10YR8/3 (very pale brown), soft, slightly plastic, and moist	
42.4	50.0	Silt with little Clay, 7.5YR8/4 (pink) with some 7.5YR7/6 (reddish yellow) mottling, moderately soft, plastic, and moist	
50.0	52.1	Silt with Sand, 10YR8/1 (white) with 10YR8/6 (yellow) laminations, soft, nonplastic, and moist. Sand is fine quartz grains	
52.1	54.6	Silt with Sand, 5YR8/2 (pinkish white), soft, nonplastic, and moist. Sand is very fine quartz grains	HU3
54.6	55.4	Sand, 10YR8/3 (very pale brown), firm, and moist. Sand is very fine to fine quartz grains	
55.4	56.8	Silt with Sand, 10YR7/6 (yellow) mottled with 10YR8/1 (white), soft, nonplastic, and moist. Sand is fine quartz grains	
56.8	57.5	Silt with some Clay, 7.5YR7/3 (pink) mottled with 7.5YR8/1 (white), moderately hard, slightly plastic, and moist	
57.5	61.0	Silt with Sand, 7.5YR8/1 (white) mottled with 5YR6/6 (reddish yellow), soft, nonplastic, and moist. Sand is fine quartz grains	
61.0	64.6	Sand 10YR8/3 (very nale brown) loose and wet Sand	HU4
64.6	65.0	Sand with Gravel, 10YR8/2 (very pale brown), firm and moist. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 0.3- to 1.0-inch diameter	HU5

# Plant North -2606.307, Plant East -5129.596

Г		1 Iant Worth 2000.307, 1 Iant East 5123.330	10/15/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	1.2	Fill: Gravelly Sand, 2.5YR5/6 (red), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to rounded chert with iron patina, 0.4- to 0.7-inch diameter	Fill
1.2	2.5	Silt with Gravel, 5YR7/3 (pink), soft, plastic, and moist. Gravel is rounded to subrounded chert with iron patina, 0.3- to 0.8-inch diameter	
2.5	13.1	Silt, 10YR7/1 (light gray) GRADING DOWN to 10YR7/4 (very pale brown) mottled with 10YR7/1 (light gray), soft, nonplastic, and moist	HU1
13.1	13.7	Sand, 10YR8/2 (very pale brown), dense, and moist. Sand is very fine quartz grains	
13.7	14.4	Silt with little Clay, 10YR6/4 (light yellowish brown), GRADING DOWN to 10YR7/1 (light gray), moderately hard, moderately plastic, and moist	
14.4	17.3	Sand with Gravel and little Silt, 10YR8/1 (white) mottled with 10YR7/6 (yellow), firm, and moist. Sand is very fine quartz grains. Gravel is subrounded chert with iron patina, 0.3- to 1.0-inch diameter	
17.3	18.2	Sand with Gravel, 10YR7/4 (very pale brown), dense, and moist. Sand is 70% fine quartz grains and 30% coarse to very coarse, subrounded, chert grains. Gravel is subrounded to subangular chert with iron patina, 0.3- to 0.4-inch diameter	
18.2	19.7	Silt, 10YR7/6 (yellow) mottled with 10YR8/1 (white), moderately soft, slightly plastic, and moist	
19.7	23.3	Sand with Gravel, 10YR6/6 (brownish yellow), dense, and moist. Sand is 80% fine quartz grains and 20% coarse, subrounded, chert grains. Gravel is subrounded to subangular chert with iron patina, 0.3- to 0.8-inch diameter	HU2
23.3	24.1	Sand, 10YR8/3 (very pale brown), firm, and moist. Sand is fine quartz grains	
24.1	26.7	Silt, 10YR8/4 (very pale brown) GRADING DOWN to 10YR8/4 (very pale brown) mottled with 10YR8/1 (white), soft, plastic, and moist	
26.7	29.2	Sand, 10YR8/2 (very pale brown) mottled with 10YR7/6 (yellow), firm, and moist. Sand is fine quartz grains	
29.2	30.6	Sand with some Gravel, 10YR8/3 (very pale brown), firm and moist Sand is fine quartz grains. Gravel is	

#### Plant North -2606.307, Plant East -5129.596

		1 Iant North -2000.307, 1 Iant East -3129.390	10/13/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
30.6	31.7	Gravelly Sand with little Silt, 10YR7/4 (very pale brown), dense, and moist. Sand is 60% fine to medium quartz grains and 40% coarse to very coarse, subrounded, chert grains. Gravel is subrounded chert with(?) iron patina, 0.3- to 0.5-inch diameter	
31.7	35.5	Silt, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white), soft, moderately plastic, and moist	
35.5	39.2	Silt with Sand, 10YR8/6 (yellow) mottled with 10YR8/1 (white), soft, nonplastic, and moist. Sand is very fine quartz grains	
39.2	43.1	Silt with little Clay, 7.5YR7/6 (reddish yellow) mottled with 7.5YR8/1 (white), soft, plastic, and moist	
43.1	46.6	Silt with little Clay as above but moderately hard and slightly plastic	
46.6	48.6	Sand, 10YR8/1 (white) with some 10YR7/4 (very pale brown) mottling, firm, and moist. Sand is fine quartz grains	
48.6	49.6	Silt with Sand, 10YR8/2 (very pale brown) GRADING DOWN to 10YR7/6 (yellow), soft to moderately soft, moderately plastic, and moist. Sand is very fine quartz grains	HU3
49.6	52.3	Sand with little Silt, 10YR6/6 (brownish yellow), firm, and moist. Sand is very fine to fine sand	
52.3	53.1	Silt, 10YR8/3 (very pale brown), soft, nonplastic, and moist	
53.1	54.5	Sand, 10YR8/2 (very pale brown) with 10YR6/6 (brownish yellow) laminations, firm, and moist. Sand is very fine quartz grains	
54.5	57.5	Silt with little Clay, 7.5YR8/1 (white) mottled with 7.5YR7/6 (reddish yellow), moderately hard, slightly plastic, and moist	
57.5	59.4	Interbedded Sand and Silt, 7.5YR7/3 (pink). Sand is fine quartz grains, firm and moist. Silt is soft, plastic, and moist	
59.4	62.3	Sand, 7.5YR7/4 (pink), firm to loose, and very moist to wet. Sand is fine quartz grains	
62.3	62.5	Silt, 10YR8/3 (pink), soft, moderately plastic, and moist	HU4
62.5	64.6	Sand with little Gravel, 10YR7/6 (yellow), firm, and moist. Sand is fine quartz grains. Gravel is rounded to subrounded chert without iron patina, 0.7- to 1.0-inch diameter	
64.6	65.0	Sand, 10YR8/1 (white), firm, and very moist. Sand is very fine quartz grains	

## Plant North -2611.28, Plant East -5085.431

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	3.2	Fill: Gravelly Sand, 2.5YR5/6 (red), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert with iron patina, 0.4- to 0.6-inch diameter	Fill
3.2	12.4	Silt, 10YR7/1 (light gray) with some 10YR7/4 (very pale brown) mottling GRADING DOWN to 10YR7/4 (very pale brown) with 10YR7/1 (light gray) mottling, soft, nonplastic, and moist	HU1
12.4	16.4	Sand with little Gravel, 10YR8/2 (very pale brown) mottled with 10YR6/4 (light yellowing brown), firm to dense, and moist. Sand is very fine quartz grains. Gravel is subrounded chert with iron patina, 0.3- to 0.4-inch diameter	
16.4	18.8	Silt with little Clay and little Gravel, 10YR7/1 (light gray) with 10YR7/4 (very pale brown) mottling, moderately hard, slightly to moderately plastic, and moist. Gravel is subrounded to subangular chert without iron patina, 0.3- to 0.7-inch diameter	
18.8	20.3	Sand with Gravel, 10YR7/4 (very pale brown), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert (and trace of feldspar)without iron patina, 0.3- to 0.4-inch diameter.	
20.3	20.9	Silt with Sand and little Gravel, 10YR7/2 (light gray), moderately hard, nonplastic, and moist. Sand is fine quartz grains	HU2
20.9	21.7	Sand with Gravel as 18.8 to 20.3 ft	
21.7	24.5	Silt, 7.5YR7/6 (reddish yellow) mottled with 7.5YR8/1 (white), moderately soft, moderately plastic, and moist	
24.5	27.2	Silt with Sand, 7.5YR7/6 (reddish yellow) mottled with 7.5YR8/1 (white), soft, nonplastic, and moist. Sand is very fine quartz grains	
27.2	34.0	Gravelly Sand (85% fine quartz grains and 15% coarse, subrounded, chert grains) with 0.3- to 0.4-ft interbeds of fine Sand, 10YR7/4 (very pale brown); dense, and moist. Gravel is subrounded to rounded chert with and without iron patina, 0.3- to 0.7-inch diameter	
34.0	35.2	Silt with Clay, 7.5YR7/4 (pink), moderately hard, slightly plastic, and moist	
35.2	36.2	Silt, 10YR8/2 (very pale brown), soft, nonplastic, and moist	
36.2	37.7	Silty Sand, 10YR8/2 (very pale brown), firm, and moist. Sand is very fine quartz grains	
37.7	38.2	Sand, 10YR8/2 (very pale brown) mottled with 10YR7/6 (yellow), firm, and moist. Sand is very fine quartz grains	

#### Plant North -2611.28, Plant East -5085.431

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
38.2	40.0	Silt, 10YR8/3 (very pale brown) with 5YR7/8 (light red) laminations, soft to moderately soft, nonplastic, and moist	
40.0	44.9	Silt, 7.5YR6/2 (pinkish gray) mottled with 7.5YR7/6 (reddish yellow) GRADING DOWN to 7.5YR7/2 (pinkish gray) with 7.5YR7/4 (pink) mottling, moderately hard, moderately plastic, and moist	HU3
44.9	48.0	Silty Sand GRADING DOWN to Sand, 10YR7/3 (very pale brown) with 10YR7/4 (very pale brown) laminations/mottling, firm, and moist. Sand is very fine quartz grains	
48.0	49.4	Sand, 10YR8/2 (very pale brown) mottled with 10YR7/6 (yellow), firm, and moist. Sand is fine quartz grains	
49.4	55.5	Silt with little Clay, 7.5YR8/2 (pinkish white) mottled with 7.5YR7/6 (reddish yellow), moderately soft, plastic to moderately plastic, and moist	
55.5	58.0	Silt with little Clay, 7.5YR7/4 (pink) with little 7.5YR8/1 (white) mottling, moderately hard, slightly plastic, and moist	
58.0	58.5	Silt with little Clay as 55.5 to 58.0 ft but colored 7.5YR8/2 (pinkish white)	
58.5	61.7	Sand with some Silt blebs, 10YR7/6 (yellow) and dense, GRADING DOWN to 10YR8/2 (very pale brown) and lightly consolidated; and moist. Sand is very fine quartz grains	
61.7	62.3	Sand, 10YR8/3 (very pale brown), firm, and moist. Sand is fine quartz grains	HU4
62.3	62.5	Sand with Gravel, 10YR7/3 (very pale brown), firm, and moist. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 0.3- to 0.5-inch diameter	

Plant North -2611.717, Plant East -5056.859

10/16/2012

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	2.6	Gravelly Sand, 2.5YR6/6 (red), dense, and moist. Sand is 80% fine quartz grains and 20% coarse, subrounded, chert grains. Gravel is subangular to subrounded chert with iron patina, 0.3- to 0.5-inch diameter	Fill
2.6	3.2	Silty Sand with Gravel, 5YR7/4 (pink), firm, and moist. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 0.3- to 1.0-inch diameter	
3.2	14.4	Silt, 10YR8/2 (very pale brown) with little 10YR7/6 (yellow) mottling GRADING DOWN to 10YR7/4 (very pale brown), soft, nonplastic, and moist	
14.4	15.0	Silt GRADING DOWN to Sand, 10YR8/1 (white) GRADING DOWN to 10YR8/4 (very pale brown), moderately soft/firm, nonplastic, and moist. Sand is very fine quartz grains	
15.0	19.6	Silt with Clay and some Gravel, 10YR7/1 (light gray) with little 10YR7/4 (very pale brown) mottling, moderately soft/stiff, slightly to moderately plastic, and moist. Gravel is rounded to subrounded chert without iron patina, 0.3- to 0.4-inch diameter	HU1
19.6	20.0	Silt with Sand, 10YR7/6 (yellow), moderately soft, nonplastic, and moist. Sand is fine quartz grains	
20.0	20.3	Silt with Clay and some Gravel as 15.0 to 19.6 ft	
20.3	23.0	Sand with Gravel, 7.5YR7/6 (reddish yellow), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert with iron patina, 0.3- to 0.5-inch diameter	
23.0	24.9	Silty Sand, 10YR8/6 (yellow) mottled with 10YR8/1 (white), firm, and moist. Sand is very fine quartz grains	
24.9	25.1	Sand, 7.5YR7/8 (reddish yellow), firm, and moist. Sand is fine quartz grains	
25.1	26.4	Silty Sand as 23.0 to 24.9 ft	HU2
26.4	32.0	Gravelly Sand, 7.5YR7/4 (pink), dense, and moist. Sand is fine quartz grains. Gravel is subangular to subrounded chert with iron patina, 0.3- to 0.5-inch diameter	
32.0	34.6	Gravelly Sand with little Silt, 7.5YR7/6 (reddish yellow), dense, and moist. Sand is fine quartz grains. Gravel is subangular to subrounded chert with iron patina, 0.3- to 0.5-inch diameter	
34.6	35.5	Sand, 7.5YR7/6 (reddish yellow), firm, and moist. Sand is very fine to fine quartz grains	
35.5	45.0	Silt, 7.5YR8/4 (pink) with 7.5YR7/6 (reddish yellow) laminations GRADING DOWN to 7.5YR8/2 (pinkish white) with 7.5YR7/6 (reddish yellow) laminations, very soft, nonplastic, and moist	

#### Plant North -2611.717, Plant East -5056.859

10/16/2012

		1 Iant North -2011.717, 1 Iant East -5050.057	 10/10/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
45.0	46.4	Silty Sand, GRADING DOWN to Sand, 10YR8/2 (very pale brown) with 10YR7/6 (yellow) laminations/mottling, firm, and moist. Sand is very fine quartz grains	
46.4	48.2	Sand, 7.5YR8/1 (white) with 7.5YR7/6 (reddish yellow) mottling and staining, firm, and moist. Sand is fine quartz grains	
48.2	49.6	Gravelly Sand, 10YR7/3 (very pale brown), dense, and moist. Sand is 85% fine quartz grains and 15% coarse, subrounded, chert grains. Gravel is subangular to subrounded chert with iron patina, 0.3- to 0.6-inch diameter	HU3
49.6	50.0	Silt with little Clay, 7.5YR7/6 (reddish yellow), moderately hard, slightly plastic, and moist	
50.0	51.4	Silt, 7.5YR8/4 (pink) with 7.5YR8/1 (white) mottling, soft, plastic, and moist	
51.4	54.5	Silt with Sand, 7.5YR8/1 (white) mottled with 7.5YR7/6 (reddish yellow), soft, nonplastic, and moist. Sand is very fine quartz grains	
54.5	58.6	Silt with little Clay, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white), soft, moderately plastic to plastic, and moist	
58.6	61.0	Silty Sand, 10YR8/2 (very pale brown) with 10YR7/6 (yellow) and 5YR7/6 (reddish yellow) laminations, firm, and moist. Sand is very fine quartz grains	
61.0	64.7	Sand with few Silt blebs, 10YR8/1 (white) GRADING DOWN to 10YR8/4 (very pale brown), firm to loose, and moist to wet. Sand is fine quartz grains	HU4
64.7	65.0	Sand, 7.5YR7/6 (reddish yellow), lightly consolidated, and wet. Sand is fine quartz grains	

## Plant North -2642.029, Plant East -5211.033

10/9/2012

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	2.7	Sand with Gravel/Gravelly Sand, 2.5YR5/6 (red), dense, and moist. Sand is 90% fine quartz grains and 10% coarse, subrounded, chert grains. Gravel is subrounded chert with iron patina, 0.3- to 0.5-inch diameter	Fill
2.7	13.1	Silt, 10YR7/1 (light gray) with some 10YR7/6 (yellow) mottling, soft, nonplastic, and moist	
13.1	14.8	Interbedded fine Sand, 7.5YR6/6 (reddish yellow) and very fine Sand (7.5YR8/1 (white), firm, and moist. Sand is quartz grains	
14.8	17.0	Gravelly Sand, 7.5YR5/6 (strong brown), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert with iron patina, 4 mm- to 0.6-inch diameter	
17.0	17.7	Sand, 7.5YR7/6 (reddish yellow), dense, and moist. Sand is fine quartz grains	HU1
17.7	21.3	Gravelly Sand as 14.8 to 17.0 ft	
21.3	21.7	Sand with Gravel, 10YR8/3 (very pale brown), firm, and moist. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 0.3- to 0.6-inch diameter	
21.7	22.3	Sand, 10YR8/3 (very pale brown), firm, and moist. Sand is fine quartz grains	
22.3	26.0	Silt, 10YR8/4 (Very pale brown) mottled with 10YR8/1 (white), soft, plastic to moderately plastic, and moist	
26.0	27.1	Sand with little Gravel, 10YR7/6 (yellow), firm, and moist. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 0.3- to 0.5-inch diameter	
27.1	28.0	Gravelly Sand, 10YR8/1 (white) mottled with 10YR8/4 (very pale brown), dense, and moist. Sand is fine quartz grains. Gravel is subangular to subrounded chert with iron patina, 4 mm- to 0.4-inch diameter	HU2
28.0	28.8	Sand, 10YR7/6 (yellow), firm, and moist. Sand is fine quartz grains	
28.8	30.0	Sandy Gravel, 10YR8/2 (very pale brown), dense, and moist. Gravel is subrounded to subangular chert with iron patina, 0.3- to 0.6-inch diameter	
30.0	30.8	Sandy Gravel as 28.8 to 30.0 ft but with Silt	
30.8	32.4	Sandy Gravel as 28.8 to 30.0 ft	
32.4	37.0	(pinkish white), soft, plastic to moderately plastic, and moist	
37.0	40.8	Silt with Clay, 7.5YR7/3 (pink) mottled with 7.5YR8/1 (white), soft, plastic, and moist	

## Plant North -2642.029, Plant East -5211.033

10/9/2012

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology		Hydrogeologic Unit
40.8	41.7	Silt with Clay as 37.0 to 40.8 ft but very soft	Ī	
41.7	43.0	Silt with Clay, 7.5YR7/3 (pink) mottled with 7.5YR8/1 (white) GRADING DOWN to 10YR8/2 (very pale brown), moderately hard, moderately plastic, and moist		
43.0	47.4	Silt with Clay, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white), moderately soft with blebs of both moderately hard and soft, slightly to moderately plastic, and moist		HU3
47.4	49.5	Sand, 10YR7/4 (very pale brown), firm, and moist. Sand is fine quartz grains. Note: 49.2 to 49.5 ft contains some chert gravel with iron patina, subrounded, 0.3-inch diameter		
49.5	55.1	Silt with Clay, 7.5YR6/6 (reddish yellow) mottled with 7.5YR8/1 (white), moderately hard, slightly plastic, and moist		
55.1	58.0	Silt with Sand, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white) GRADING DOWN to 10YR8/3 (very pale brown), soft, slightly plastic, and moist. Sand is fine quartz grains		
58.0	58.5	Sand, 10YR8/6 (yellow), firm, and moist. Sand is very fine quartz grains		
58.5	60.2	Sand, 10YR8/4 (very pale brown), firm, and moist. Sand is fine quartz grains		
60.2	60.5	Sand with Silt and Gravel, 10YR7/6 (yellow), firm, and moist. Sand is fine quartz grains. Gravel is rounded chert without iron patina, 0.3-inch diameter		HU4
60.5	62.0	Sand with a few Silt interbeds, 10YR8/2 (very pale brown), lightly consolidated to firm, and moist. Sand is fine quartz grains		
62.0	62.1	Sandy Gravel, 10YR7/4 (very pale brown), loose, and moist. Gravel is subrounded chert with iron patina, 0.3- inch diameter. Sand is fine quartz grains		
62.1	62.5	Sand with a few Silt interbeds as 60.5 to 62.0 ft		

## Plant North -2642.058, Plant East -5180.914

10/8/2012

~ 1	_	Than 10111 2042.030, Than East 5100.914	10/0/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	2.4	Gravelly Sand with little Silt, 2.5YR5/6 (red), dense, and moist. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 0.3- to 0.8-inch diameter	FILL
2.4	14.2	Silt, 10YR8/2 (very pale brown) mottled with 10YR7/6 (yellow), soft, nonplastic, and moist	HU2
14.2	15.2	Clayey Silt, 10YR7/2 (light gray), moderately hard, moderately plastic, and moist	
15.2	16.7	Silty Sand, 10YR7/1 (light gray), firm, and moist. Sand is very fine quartz grains	
16.7	20.1	Gravelly Sand with little Silt, 10YR6/4 (light yellowish brown), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert with and without iron patina, 0.3 - to 0.6-inch diameter	
20.1	21.2	Silty Sand with Gravel, 10YR7/1 (light gray), firm, and moist. Sand is very fine quartz grains. Gravel is subrounded chert without iron patina, 0.5- to 0.8-inch diameter	
21.2	23.5	Gravelly Sand with little Silt, 10YR6/6 (brownish yellow), dense, and moist. Sand is 90% fine quartz grains and 10% subrounded, coarse, chert grains. Gravel is subrounded chert with and without iron patina, 0.3- to 0.5-inch diameter	
23.5	26.7	Sand, 10YR8/1 (white) with 10YR7/6 (yellow) mottling, firm, and moist. Sand is very fine quartz grains	HU2
26.7	29.5	Gravelly Sand, 10YR8/2 (very pale brown) GRADING DOWN to 10YR7/6 (yellow), dense, and moist. Sand is 90% fine quartz grains and 10% coarse, subrounded, chert grains. Gravel is subrounded chert with and without iron patina, 4-mm to 0.6-inch diameter	
29.5	30.2	Gravelly Sand with Silt, 7.5YR7/1 (light gray), dense, and moist. Sand is 90% fine quartz grains and 10% coarse, subrounded, chert grains. Gravel is subrounded chert with and without iron patina, 4-mm to 0.6-inch diameter	
30.2	31.0	Sand, 10YR8/3 (very pale brown), firm, and moist. Sand is fine quartz grains	
31.0	34.0	Gravelly Sand as 26.7 to 29.5 ft	
34.0	35.0	Silty Clay, 7.5YR7/4 (pink) with 7.5YR8/1 (white) mottling, soft, plastic, and moist	
35.0	37.6	Silt with Sand, 10YR7/2 (light gray) with little 10YR7/6 (yellow) mottling, soft, nonplastic, and moist. Sand is very fine quartz grains	
37.6	39.1	Silt with little Clay, 7.5YR8/1 (white) mottled with 7.5YR7/6 (reddish yellow), soft, plastic, and moist	

#### Plant North -2642.058, Plant East -5180.914

10/8/2012

-		1 Iant North -2042.050, 1 Iant East -5100.514	10/8/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
39.1	42.7	Silt with little Clay as 37.6 to 39.1 ft interbedded with Clay with Silt, 10YR7/6 (reddish yellow) mottled with 7.5YR8/1 (white) and 7.5YR7/4 (pink), soft, plastic, and moist	
42.7	45.5	Silt, 7.5YR7/6 (reddish yellow), moderately soft, nonplastic, and moist	
45.5	46.7	Silt with some Clay, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white) and 7.5YR6/1 (gray), soft to moderately soft, plastic, and moist	HU3
46.7	52.3	Silt with Sand, 10YR7/6 (yellow) mottled with 10YR8/1 (white), soft, nonplastic, and moist. Sand is very fine quartz grains	
52.3	54.5	Silt with little Clay, 7.5YR6/6 (reddish yellow) with some 7.5YR8/1 (white) mottling, moderately soft, slightly plastic, and moist	
54.5	55.0	Silt with little Clay, 7.5YR6/6 (reddish yellow) with some 7.5YR8/1 (white) mottling, soft, plastic, and moist	
55.0	59.1	Silt with Sand, 10YR8/2 (very pale brown) with 10YR7/6 (yellow)-GRADING-DOWN-to-7.5YR7/4 (pink) laminations, soft, nonplastic, and moist. Sand is fine quartz grains	
59.1	60.3	Sand, 10YR8/4 (very pale brown), firm, and moist. Sand is very fine quartz grains	
60.3	62.5	Sand, 10YR8/2 (very pale brown), lightly consolidated, and moist. Sand is very fine quartz grains	
62.5	63.1	Sand with some Gravel, 10YR8/2 (very pale brown), firm, and moist. Sand is fine quartz grains. Gravel is subrounded to rounded chert without iron patina, 0.3- to 0.4-inch diameter	HU4
63.1	64.0	Sand, 7.5YR7/8 (reddish yellow), firm, and moist. Sand is fine quartz grains	
64.0	65.0	Sand with Gravel, 10YR8/2 (very pale brown), loose, and wet. Sand is fine quartz grains. Gravel is subrounded chert without iron patina, 0.3- to 0.8-inch diameter	

Plant North -2642.383, Plant East -5151.421

10/5/2012

-		Plant North -2042.383, Plant East -5151.421	10/5/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	2.5	Fill: Gravelly Sand, 2.5YR5/6 (red), dense, and moist. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 0.3- to 0.5-inch diameter	Fill
2.5	14.7	Silt, 10YR7/1 (light gray) with some 10YR7/4 (very pale brown) mottling, soft, nonplastic, and moist	
14.7	16.0	Clayey Silt with little Gravel, 10YR7/1 (light gray) with 10YR6/1 (gray) mottling, moderately hard, moderately plastic, and moist. Gravel is subrounded chert without iron patina, 0.3-inch diameter	HU1
16.0	16.5	Clayey Silt, 10YR7/1 (light gray) with 10YR6/1 (gray) mottling, moderately hard, moderately plastic, and moist0.3-inch diameter	
16.5	17.9	Sand with little Gravel, 7.5YR7/6 (reddish yellow), dense, and moist. Sand is 90% fine quartz grains and 10% coarse, rounded, chert grains. Gravel is rounded to subrounded chert with iron patina, 0.4- to 0.6-inch diameter	
17.9	19.0	Clayey Silt with little Gravel, 10YR7/1 (light gray) with 10YR6/1 (gray) mottling, moderately hard, moderately plastic, and moist. Gravel is subrounded chert without iron patina, 0.3- to 0.4-inch diameter	
19.0	20.0	Crushed sample sleeve: 19.0 to 19.6 = Clayey Silt with little Gravel as above and 19.6 to 20.0 ft = Sand with Gravel and little Silt as below	
20.0	20.6	Sand with Gravel and little Silt, 7.5YR6/6 (reddish yellow), dense, and moist. Sand is 80% fine quartz	HU2
20.6	21.2	Silt with Sand, 10YR8/2 (very pale brown), soft, nonplastic, and moist. Sand is fine quartz grains	
21.2	26.0	Silt with Sand as above but with little Gravel. Gravel is subrounded to rounded chert without(?) iron patina, 0.3-to 0.4-inch diameter	
26.0	31.5	Gravelly Sand with little Silt, 10YR7/6 (yellow) GRADING DOWN to 7.5YR7/4 (pink), dense, and very moist. Sand is 80% fine quartz grains and 20% coarse, subrounded, chert grains. Gravel is subangular to subrounded chert with iron patina, 4 mm- to 0.8-inch diameter	
31.5	37.0	Silt with Sand, 7.5YR8/4 (pink) mottled with 7.5YR8/1 (white), very soft, nonplastic to slightly plastic, and moist. Sand is very fine quartz grains	

#### Plant North -2642.383, Plant East -5151.421

10/5/2012

		Flaint North -2042.385, Flaint East -3151.421	10/3/2012
Start	End		
Depth	Depth	Lithology	Hydrogeologic Unit
(ft bgs)	(ft bgs)		
37.0	45.0	Silt, 7.5YR7/6 (reddish yellow) with 7.5YR8/1 (white) mottling GRADING DOWN to 7.5YR8/1 (white) with 7.5YR7/4 (pink) mottling, soft, slightly plastic, and moist	
45.0	47.2	Silty Sand, 10YR7/4 (very pale brown), firm, and moist. Sand is very fine quartz grains	
47.2	49.9	Silt with little Clay and some Gravel, 10YR7/4 (very pale brown) mottled with 10YR8/1 (white), moderately soft, plastic, and moist. Gravel is subrounded to subangular chert without iron patina, 0.4- to 0.8-inch diameter	HU3
49.9	50.2	Sand with some Gravel, 10YR6/6 (brownish yellow), firm, and moist. Sand is fine quartz grains	
50.2	54.0	Silt, 10YR7/4 (very pale brown) mottled with 10YR8/1 (white) GRADING DOWN to 7.5YR8/1 (white) mottled with 7.5YR7/4 (pink), soft, moderately plastic, and moist	
54.0	55.0	Clay 7 5VR7/4 (nink) with some 7 5VR8/1 (white)	
55.0	56.1	Clay as above	
56.1	59.5	Silt with Sand, 7.5YR7/4 (pink) GRADING DOWN to 7.5YR8/1 (white), soft, nonplastic, and moist. Sand is very fine quartz grains	
59.5	60.0	Sand, 10YR8/3 (very pale brown), lightly consolidated, and moist. Sand is very fine quartz grains	
60.0	60.9	Sand as above but colored 7.5YR7/4 (pink)	
60.9	62.5	Sand as 59.5 to 60.0 ft but colored 7.5YR8/2 (pinkish white) GRADING DOWN to 7.5YR8/1 (white)	
62.5	64.2	Sand with some Gravel, 10YR8/1 (white) GRADING DOWN to 10YR8/3 (very pale brown), firm, and wet. Sand is 90% very fine quartz grains and 10% coarse, subrounded, chert grains. Gravel is subangular to subrounded chert without iron patina, 4 mm- to 0.4-inch diameter	HU4
64.2	65.0	Sand, 10YR8/3 (very pale brown), firm, and moist. Sand is very fine quartz grains	

Plant North -2642.307, Plant East -5120.984

10/8/2012

· · · · · ·		1 Iant North -2042.307, 1 Iant East -3120.984	10/8/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	2.1	Fill: Gravelly Sand, 2.5YR5/6 (red), dense, and moist. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 0.3- to 0.5-inch diameter	Fill
2.1	13.7	Silt, 10YR7/1 (light gray) with 10YR7/4 (very pale brown) mottling, soft, nonplastic, and moist	
13.7	15.4	Silt with some Gravel and little Clay, 10YR7/2 (light gray), moderately soft, moderately plastic, and moist. Gravel is subrounded chert with iron patina, 0.3- to 0.5- inch diameter	
15.4	16.4	Sandy Gravel, 10YR6/3 (pale brown), dense, and moist. Gravel is subrounded chert with iron patina, 0.3- to 0.5- inch diameter. Sand is fine quartz grains	HU1
16.4	18.2	Silt with some Gravel and little Clay, 10YR7/2 (light gray), moderately soft, moderately plastic, and moist. Gravel is subangular chert without iron patina, 0.4- to 0.5-inch diameter	
18.2	21.9	Gravelly Sand with little Silt, 7.5YR7/4 (pink), dense, and moist. Sand is 80% fine quartz grains and 20% coarse, subrounded, chert grains. Gravel is subrounded to rounded chert with and without iron patina, 0.3- to 0.6-inch diameter	
21.9	22.4	Sand, 10YR7/6 (yellow), firm, and moist. Sand is very fine quartz grains	
22.4	24.6	Silt, 10YR8/6 (yellow) mottled with 10YR8/1 (white), soft, slightly plastic, and moist	
24.6	29.2	Sandy Silt with little Gravel, 10YR7/3 (very pale brown), moderately soft, nonplastic, and moist. Gravel is subrounded chert without iron patina, 0.6- to 1.0-inch diameter	HU2
29.2	31.6	Sandy Gravel with little Silt, 7.5YR7/4 (pink) with some 7.5YR5/1 (gray) staining (manganese?), dense, and moist. Gravel is subangular to subrounded chert without(?) iron patina, 0.3- to 1.0-inch diameter. Sand is 75% fine quartz grains and 25% coarse to very coarse, subrounded to rounded, chert grains	
31.6	32.2	Sand, 7.5YR7/8 (reddish yellow), firm, and moist. Sand is fine quartz grains	
32.2	34.3	Silt with little Clay, 7.5YR7/6 (reddish yellow) with little 7.5YR8/1 (white) mottling, soft, nonplastic, and moist	
34.3	40.0	Silt, 10YR7/4 (very pale brown) mottled with 10YR8/1 (white), very soft, nonplastic, and moist	
40.0	40.8	Silt with little Clay 7 5VR7/ $A$ (pink) mottled with	
40.8	42.0	Silt as 34.3 to 40.0 ft	

#### Plant North -2642.307, Plant East -5120.984

10/8/2012

		Flain Notul -2042.307, Flain East -3120.964	10/8/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
42.0	42.4	Silt with little Clay, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white) and 2.5YR6/8 (light red), moderately soft, slightly plastic, and moist	
42.4	45.9	Silt, 7.5YR7/4 (pink) GRADING DOWN to 7.5YR8/1 (white) mottled with 7.5YR7/4 (pink), soft, nonplastic, to slightly plastic, and moist	
45.9	50.1	Silt with Sand, 7.5YR7/6 (reddish yellow) mottled with 7.5YR8/1 (white), soft, nonplastic to slightly plastic, and moist. Sand is very fine quartz grains	HU3
50.1	51.6	Sand, 10YR8/1 (white) GRADING DOWN to 10YR7/6 (yellow), firm, and moist. Sand is very fine quartz grains	
51.6	52.8	Sand, 10YR7/6 (yellow), firm, and moist. Sand is fine quartz grains	
52.8	54.4	Sandy Silt, 7.5YR7/3 (pink), soft, nonplastic, and moist	
54.4	58.0	Silt with Clay, 7.5YR7/4 (pink) with 7.5YR8/1 (white) mottling, moderately hard, moderately plastic, and moist	
58.0	60.3	Silt with Sand, 10YR8/2 (very pale brown) GRADING DOWN to 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white), soft, nonplastic, and moist. Sand is very fine quartz grains	
60.3	62.5	Sand, 10YR8/1 (white), lightly consolidated, and moist. Sand is very fine quartz grains	
62.5	62.7	Gravel with Sand and Silt, 10YR7/8 (yellow), firm, and moist. Gravel is subrounded chert with(?) iron patina, 0.6- to 1.0-inch diameter. Sand is very fine quartz sand	
62.7	63.1	Sand, 10YR8/1 (white), loosely consolidated, and moist. Sand is fine quartz grains	HU4
63.1	63.3	Silty Clay, 10YR7/3 (very pale brown), soft, plastic, and moist	
63.3	67.5	Sand, 10YR8/2 (very pale brown) with 7.5YR7/8 (reddish yellow) laminations, firm, and moist. Sand is fine quartz grains	

#### Plant North -2642.287, Plant East -5091.257

		1 Iant 101th -2042.207, 1 Iant East -5091.257	10/4/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	3.1	Fill: Gravelly Sand, 2.5YR5/6 (red), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert with iron patina, 4 mm- to 0.5-inch diameter	Fill
3.1	15.2	Silt, 10YR7/2 (light gray) mottled with 10YR7/4 (very pale brown), soft, nonplastic to slightly plastic, and moist	
15.2	18.6	Silt with little Clay and little Gravel, 10YR7/2 (light gray) with some 10YR7/3 (very pale brown) mottling, moderately hard, moderately plastic, and moist. Gravel is rounded to subangular chert without iron patina, 0.3-inch diameter	HU1
18.6	18.9	Gravelly Sand with little Silt, 10YR5/4 (yellowish	
18.9	19.9	is subrounded to subangular chert without iron patina, 0.3- to 0.4-inch diameter	
19.9	21.4	Silty Sand with little Gravel, 7.5YR7/2 (pinkish gray), firm, and moist. Sand consists of 70% fine quartz grains and 30% very coarse, subrounded, chert grains. Gravel is subrounded chert without(?) iron patina, 4 mm- to 0.3- inch diameter	
21.4	22.6	Sand, 7.5YR7/6 (reddish yellow) GRADING DOWN to 10YR7/6 (yellow) mottled with 10YR8/1 (white), firm, and moist. Sand is very fine quartz grains	
22.6	23.6	Gravelly Sand with Silt, 10YR6/6 (brownish yellow), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert without iron patina, 0.4- to 0.8-inch diameter	HU2
23.6	25.1	Sand, 7.5YR7/6 (reddish yellow), firm, and moist. Sand is fine quartz grains	
25.1	25.9	Silt with Sand, 7.5YR7/6 (reddish yellow) mottled with 7.5YR8/1 (white), soft, slightly plastic, and moist. Sand is fine quartz grains	
25.9	28.1	Sand with Gravel, 7.5YR6/8 (reddish yellow) with some 7.5YR8/1 (white) mottling, firm to dense, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert without iron patina, 4 mm- to 0.8-inch diameter	
28.1	29.1	Sand, 10YR7/3 (very pale brown), firm, and moist. Sand is fine quartz grains	
29.1	30.0	Sand with Gravel as 25.9 to 28.1 ft	

#### Plant North -2642.287, Plant East -5091.257

r		Plant North -2642.287, Plant East -5091.257	10/4/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
30.0	32.1	Sand with Gravel, 10YR6/4 (light yellowish brown), firm to dense, and moist. Sand is 80% fine quartz grains and 20% coarse, subrounded, chert grains. Gravel is subrounded chert with(?) iron patina, 0.3- to 0.9-inch diameter	
32.1	35.6	Silt, 7.5YR7/4 (pink), soft, moderately plastic, and moist	
35.6	37.5	Silt with Sand, 10YR8/3 (very pale brown), soft, nonplastic, and moist. Sand is very fine quartz grains	
37.5	44.9	Silt GRADING DOWN to Silt with a little Clay, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white), soft, moderately plastic to plastic, and moist	
44.9	48.1	Silt, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white), very soft, moderately plastic, and moist	
48.1	48.6	Silty Sand 7 5VR7/6 (reddish vellow) firm and moist	
48.6	50.1	Silt as 44.9 to 48.1 ft	HU3
50.1	50.8	Sand, 10YR7/4 (very pale brown), firm, and moist. Sand is fine quartz grains	
50.8	51.2	Clay, 7.5YR6/4 (light brown) mottled with 7.5YR8/1 (white), moderately hard, plastic, and moist	
51.2	54.6	Silt with Clay, 7.5YR8/1 (white) with 7.5YR7/6 (reddish yellow) mottling, moderately soft, moderately plastic, and moist	
54.6	55.6	Clay as 50.8 to 51.2 ft	
55.6	57.4	Silt with some Sand, 10YR8/3 (very pale brown), soft, slightly plastic, and moist. Sand is fine quartz grains	
57.4	62.7	Sand, 10YR8/3 (very pale brown), firm, and wet. Sand is fine quartz grains	
62.7	65.0	Sand with Gravel, 10YR8/3 (very pale brown), firm, and wet. Sand is 80% fine quartz grains and 20% coarse, rounded, chert grains. Gravel is rounded to subrounded chert without iron patina, 4 mm- to 0.5-inch diameter	HU4

#### Plant North -2642.137, Plant East -5057.047

1		Flaint Norui -2042.137, Flaint East -3037.047	10/4/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	2.5	Gravely Sand with some Silt, 2.5YR6/6 (light red), dense, and moist. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 0.3- to 1.0-inch diameter (common fill material at PGDP)	Fill
2.5	13.5	Silt, 10YR7/1 (light gray) with some 10YR6/6 (brownish yellow) mottling, soft, nonplastic to slightly plastic, and moist	
13.5	16.5	Silt with little Clay and with little Gravel, 10YR7/2 (light gray), hard, slightly plastic, and slightly moist. Gravel is subrounded chert without iron patina, 0.3-inch diameter	HU1
16.5	17.5	Sandy Gravel with Silt, 7.5YR7/2 (light gray), dens, and moist. Gravel is subrounded chert without iron patina, 0.3- to 0.4-inch diameter. Sand is fine grained	HU2
17.5	20.0	No recovery	No Recovery
20.0	21.3	Sand with some Gravel, 7.5YR7/6 (reddish yellow), dense, and moist. Sand is fine quartz grains. Gravel is subangular to subrounded chert with (?) iron patina, 4- mm to 1.0-inch diameter	
21.3	21.7	Silt, 7.5YR8/4 (pink), moderately hard, moderately plastic, and moist	
21.7	21.8	Sand, 7.5YR8/4 (pink), firm, and moist. Sand is very fine quartz grains.	
21.8	23.7	Silt with little Clay, 7.5YR7/6 (reddish yellow) with 7.5YR7/1 (light gray) mottling, soft, moderately plastic, and moist	
23.7	25.0	Silt, 7.5YR8/3 (pink) with 7.5YR8/1 (white) mottling, soft, plastic, and moist	
25.0	25.9	Silty Sand, 10YR7/4 (very pale brown) with little 10YR8/1 (white) mottling, firm, and moist. Sand is very fine quartz grains	
25.9	26.7	Sand with some Gravel, 10YR7/4 (very pale brown), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert without (?) iron patina, 4-mm to 0.3-inch diameter	HU2
26.7	27.6	Silty Sand, 10YR8/2 (very pale brown) mottled with 10YR7/6 (yellow), soft, nonplastic, and moist. Sand is very fine quartz grains	
27.6	27.9	Gravelly Medium Sand, 7.5YR6/6 (reddish yellow), loose, and moist. Gravel is subrounded chert without iron patina, 0.3-inch diameter	
27.9	28.5	Silt, 10YR7/3 (very pale brown), moderately hard, moderately plastic, and moist	
28.5	29.7	Silty Sand, 10YR8/2 (very pale brown) mottled with 10YR7/6 (yellow), firm, and moist. Sand is very fine quartz grains	

#### Plant North -2642.137, Plant East -5057.047

		Plaint North -2042.157, Plaint East -3057.047	10/4/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
29.7	32.1	Gravel with Silt, 10YR8/2 (very pale brown), dense, and moist. Gravel is subrounded to subangular chert without iron patina, 0.3- to 1.0-inch diameter	
32.1	33.1	Sand with blebs of Silt, 10YR7/3 (very pale brown), firm, and moist. Sand is very fine quartz grains	
33.1	33.8	Sand with Gravel, 10YR8/2 (very pale brown), firm, and moist. Sand is fine quartz grains. Gravel is rounded to subrounded chert without iron patina, 4-mm to 0.4- inch diameter	
33.8	34.5	Sand, 10YR8/2 (very pale brown), lightly consolidate, and moist. Sand is fine quartz grains	
34.5	34.9	Gravelly Sand as 27.6 to 27.9 ft but colored 7.5VR7/4	
34.9	35.4	Sand, 10YR8/2 (very pale brown), firm, and moist. Sand is very fine quartz grains	
35.4	36.0	Sand with Gravel as 33.1 to 33.8 ft	
36.0	36.8	Sandy Silt with some Gravel, 10YR7/3 (very pale brown) with little 2.5YR7/8 (light red) staining, soft, nonplastic, and moist. Sand is fine grained. Gravel is rounded to subrounded chert without iron patina, 0.5- to 1.0-inch diameter	
36.8	37.4	Sand with Gravel as 33.1 to 33.8 ft	
37.4	42.4	Silt, 10YR8/2 (very pale brown) with some 2.5YR7/8 (light red) staining, soft, nonplastic to slightly plastic, and moist	HU3
42.4	43.8	Silt with little Clay, 7.5YR7/3 (pink) mottled with 7.5YR7/1 (light gray), soft, moderately plastic, and moist	
43.8	47.6	Silt, 10YR8/2 (very pale brown) with laminations of 10YR7/6 (yellow) and 7.5YR7/6 (reddish yellow), moderately soft, moderately plastic, and moist	
47.6	48.2	Sand, 10YR8/2 (very pale brown) GRADING DOWN to 5YR7/6 (reddish yellow), firm, and moist. Sand is very fine quartz grains	
48.2	50.0	Silt with little Clay, 7.5YR7/4 (pink) mottled with 7.5YR7/1 (light gray), soft, moderately plastic, and moist	
50.0	52.4	Sand, 10YR8/2 (very pale brown) with 7.5YR7/6 (reddish yellow) staining, firm, and moist. Sand is very fine quartz grains	
52.4	59.5	Slightly Clayey Silt, 7.5YR8/4 (pink) with 7.5YR8/1 (white) mottling, soft, moderately plastic, and moist	
59.5	62.9	Sand, 5YR7/6 (reddish yellow), lightly consolidated, and very moist. Sand is very fine quartz grains	

Plant North -2642.137, Plant East -5057.047

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
62.9	65.0	Sandy Gravel, 7.5YR7/6 (reddish yellow), loose, and wet. Gravel is subrounded to subangular chert with iron patina, 0.3- to 1.0-inch diameter. Sand consists of 80% fine grains and 20% of coarse to very coarse, rounded, chert grains	HU4

## Plant North -2607.931, Plant East -5163.515

10/16/2012

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	3.7	Gravelly Sand, 2.5YR5/6 (red), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert with iron patina, 0.4- to 1.0-inch diameter	Fill
3.7	13.7	Silt, 10YR7/1 (light gray) with little 10YR7/6 (yellow) mottling, GRADING DOWN to 10YR7/6 (yellow) with 10YR7/1 (light gray) mottling and streaks of 10YR3/1 (very dark gray) (manganese?), soft, nonplastic, and moist	HU1
13.7	17.0	Silt with Clay and little Gravel, 10YR7/1 (light gray), moderately soft to moderately hard, slightly plastic, and moist. Gravel is subrounded to rounded chert without iron patina, 0.4- to 0.5-inch diameter	
17.0	17.4	Sand with Gravel, 7.5YR7/3 (pink), dense, and moist. Sand is 80% fine quartz grains and 20% coarse, subrounded, chert grains. Gravel is subrounded to subangular chert with iron patina, 0.3- to 0.4-inch diameter	
17.4	17.7	Sand, 10YR7/3 (very pale brown), firm, and moist. Sand is fine quartz grains	
17.7	18.0	Sand with Gravel as 17.0 to 17.4 ft	
18.0	18.3	Silt with Clay and little Gravel as 13.7 to 17.0 ft	
18.3	21.5	Sand with Gravel and little Silt, 10YR6/4 (light yellowish brown), dense, and moist. Sand is fine quartz grains. Gravel is subangular to subrounded chert with and without iron patina, 0.3- to 0.8-inch diameter	
21.5	22.4	Sand, 10YR7/6 (yellow) GRADING DOWN to 10YR8/1 (white), dense GRADING DOWN to firm, and moist. Sand is fine quartz grains	HU2
22.4	23.9	Sand with Gravel and little Silt as 18.3 to 21.5 ft	
23.9	24.5	Sand, 10YR7/6 (yellow), firm, and moist. Sand is fine quartz grains	
24.5	29.5	Silty Sand, 10YR8/1 (white) mottled with 10YR7/6 (yellow), firm, and moist. Sand is very fine quartz grains	
29.5	31.8	Sand with Gravel, 10YR6/6 (brownish yellow), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert with(?) iron patina, 0.3- to 0.6-inch diameter	
31.8	32.6	Sand with Gravel and little Silt, , 10YR6/6 (brownish yellow), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert with(?) iron patina, 0.3- to 0.6-inch diameter	
32.6	33.8	Silt with little Clay, 7.5YR7/4 (pink), very soft, moderately plastic, and moist	

# Plant North -2607.931, Plant East -5163.515

10/16/2012

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
33.8	35.7	Silt with little Clay, 7.5YR7/4 (pink) with some 7.5YR8/1 (white) mottling, soft, plastic, and moist	
35.7	39.0	Silt with Sand, 7.5YR7/6 (reddish yellow) with some 7.5YR8/1 (white) mottling, moderately soft, nonplastic, and moist. Sand is very fine quartz grains	
39.0	41.0	Silt, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white), moderately hard to moderately soft, moderately plastic, and moist	
41.0	42.5	Silt, 10YR8/2 (very pale brown) mottled with 10YR7/6 (yellow), moderately hard to moderately soft, moderately plastic, and moist	
42.5	45.0	Silt, 7.5YR6/6 (reddish yellow) with some 7.5YR8/1 (white) mottling, hard, nonplastic, and moist	
45.0	50.0	Silt with Sand, 10YR7/4 (very pale brown) with some 10YR8/1 (white) mottling, moderately hard, nonplastic, and moist. Sand is very fine quartz grains	HU3
50.0	52.0	Silt, 10YR8/2 (very pale brown) mottled with 10YR7/6 (yellow), moderately soft, slightly plastic, and moist	
52.0	52.5	Sand, 10YR8/2 (very pale brown) with 10YR7/6 (yellow) mottling, firm, and moist. Sand is very fine quartz grains	
52.5	57.7	Silt, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white), moderately hard GRADING DOWN to hard, nonplastic, and moist	
57.7	59.8	Silt with Sand, 7.5YR7/3 (pink) mottled with 7.5YR8/1 (white), soft, moderately plastic, and moist. Sand is very fine quartz grains	
59.8	62.1	Interbedded Very Fine Sand [10YR8/1 (white), firm, and moist] AND Silt with Very Fine Sand [7.5YR7/4 (pink), soft, moderately plastic, and moist]	
62.1	62.5	Sand, 10YR8/1 (white), firm, and moist. Sand is fine quartz grains	HU4

Plant North -2624.624, Plant East -5148.039

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	2.5	Gravelly Sand, 2.5YR5/6 (red), dense, and moist. Sand is fine quartz grains. Gravel is chert with iron patina, 0.3- to 1.0-inch diameter	Fill
2.5	12.9	Silt, 10YR7/2 (light gray) with little 10YR7/4 (very pale brown) mottling GRADING DOWN to 10YR6/3 (pale brown), soft, nonplastic, and moist	
12.9	13.6	Sand, 10YR8/3 (very pale brown), dense, and moist. Sand is very fine quartz grains	
13.6	15.2	Silt with Clay and some Gravel, 10YR7/4 (very pale brown) GRADING DOWN to 10YR7/2 (light gray), moderately hard/stiff, slightly plastic, and moist	HU1
15.2	16.0	Gravelly Sand, 10YR6/4 (light yellowish brown), dense, and moist. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 4 mm- to 0.4-inch diameter	
16.0	18.8	Silt with little Clay and little Gravel, 10YR7/1 (light gray), moderately soft, slightly plastic, and moist. Gravel is subrounded chert without iron patina, 0.3- to 0.7-inch diameter	
18.8	20.2	Gravelly Sand with Silt, 10YR7/3 (very pale brown), dense, and moist. Sand is fine quartz grains. Gravel is subrounded chert without iron patina, 0.7- to 1.2-inch diameter AND subangular to subrounded chert with iron patina, 0.3- to 0.7-inch diameter	
20.2	21.5	Sand with Gravel, 7.5YR7/4 (pink), dense, and moist. Sand is 70% fine quartz grains and 30% coarse-to-very- coarse, subrounded chert grains. Gravel is subangular to subrounded chert with(?) iron patina, 0.3-inch diameter	
21.5	22.6	Sand, 10YR8/2 (very pale brown) with 10YR7/6 (yellow) mottling, firm, and moist. Sand is fine quartz	
22.6	23.4	grains Sand with Gravel, 10YR7/4 (very pale brown), dense and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert with and without iron patina, 0.3-inch diameter	
23.4	23.8	Sand, 10YR8/2 (very pale brown), firm, and moist. Sand is fine quartz grains	HU2
23.8	24.1	Sandy Gravel, 10YR8/2 (very pale brown), dense, and moist. Gravel is subrounded chert with and without iron patina, 0.4-inch diameter. Sand is fine quartz grains	
24.1	29.0	Silt with Sand (very fine quartz grains), GRADING DOWN to Sand (very fine quartz grains), 10YR8/2 (very pale brown) with 10YR7/6 (yellow) and 7.5YR7/6 (reddish yellow) laminations, soft to moderately firm, nonplastic, and moist	

Plant North -2624.624, Plant East -5148.039

		Plaint North -2024.024, Plaint East -5148.059	10/17/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
29.0	31.4	Sandy Gravel GRADING DOWN to Sandy Gravel with little Silt, 7.5YR6/4 (light brown), dense, and moist. Gravel is subrounded to subangular chert with iron patina, 0.3- to 1.0-inch diameter. Sand is 80% fine quartz grains and 20% coarse-to-very-coarse, subrounded chert grains	
31.4	36.3	Silt, 7.5YR7/4 (pink) with some 7.5YR8/1 (white) mottling GRADING DOWN to 10YR7/4 (very pale brown) with some 10YR8/1 (white) mottling, very soft to soft, nonplastic to moderately plastic, and moist	
36.3	39.3	Silt, 10YR7/4 (very pale brown) with 10YR8/1 (white) mottling GRADING DOWN to 10YR8/2 (very pale brown) with 7.5YR7/4 (pink) mottling, moderately soft, nonplastic, and moist	
39.3	40.6	Silty Sand, 10YR7/3 (very pale brown) GRADING DOWN to 10YR7/6 (yellow) with 10YR8/1 (white) mottling, firm, and moist. Sand is very fine quartz grains	
40.6	41.0	Sand, 7.5YR7/6 (reddish yellow), firm and moist. Sand is fine quartz grains	
41.0	45.6	Clayey Silt, 7.5YR7/4 (pink) with 7.5YR8/1 (white) mottling, moderately hard, plastic, and moist	
45.6	47.4	Silt with Sand, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white), soft, nonplastic, and moist. Sand is very fine quartz grains. Contains trace rounded chert gravel (without iron patina), 0.6- to 1.2-inch diameter	HU3
47.4	48.0	Sand, 7.5YR7/6 (reddish yellow), dense, and moist. Sand is fine quartz grains	
48.0	51.5	Silt with little Clay, 7.5YR8/1 (white) with 7.5YR7/4 (pink) mottling, moderately soft, moderately plastic, and moist	
51.5	53.4	Silt with Sand, 7.5YR8/1 (white) mottled with 7.5YR7/4 (pink), soft, slightly plastic, and moist. Sand is very fine quartz grains	
53.4	58.5	Silt with little Clay, 7.5YR7/6 (reddish yellow) with 7.5YR8/1 (white) mottling, moderately hard, slightly plastic, and moist	
58.5	62.3	Silt with Sand (very fine quartz grains) interbedded with Silty Sand (very fine quartz grains), 7.5YR8/1 (white) with 7.5YR7/7 (reddish yellow) laminations and mottling, soft/firm, nonplastic to slightly plastic, and moist	
62.3	63.9	Sand, 10YR8/1 (white), firm, moist to loose, and wet. Sand is fine quartz grains	

Plant North -2624.624, Plant East -5148.039

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Start Depth (ft bgs)	End Depth (ft bgs)	Lithology		Hydrogeologic Unit
63.9	64.2	Sandy Gravel, 10YR8/2 (very pale brown), loose, and wet. Gravel is subrounded to subangular chert with and without iron patina, 4 mm- to 0.5-inch diameter. Sand is fine quartz grains		HU4
64.2	65.0	Sand with some Gravel and blebs of Silt, 10YR8/1 (white) with an interbed of 10YR7/6 (yellow), firm, and moist. Sand is fine quartz grains. Gravel is subrounded chert without iron patina, 0.3- to 0.5-inch diameter		

## Plant North -2607.459, Plant East -5258.754

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
(IL Ugs)	(IL DES)	Gravely Sand, 5YR6/6 (reddish yellow), dense, and	
0.0	1.8	moist. Sand is fine grained quartz. Gravel is subangular to subrounded chert with iron patina, 0.3- to 0.7-inch diameter	
1.8	2.2	Sandy Gravel, 10YR7/1 (light gray), dense, and moist. Gravel is subrounded limestone, 4mm- to 0.5-inch diameter (dense gravel aggregate/DGA). Sand is coarse, subangular limestone	Fill
2.2	4.1	Gravelly Sand as 0.0 to 1.8 ft	
4.1	10.3	Silt, 10YR7/2 (light gray) with little 10YR7/4 (very pale brown) mottling, soft, nonplastic, and moist	
10.3	11.5	Sand, 10YR6/6 (brownish yellow), dense, and moist. Sand is very fine quartz grains	
11.5	12.7	Gravelly Sand, 7.5YR6/4 (light brown), dense, and moist. Sand is 90% fine quartz grains and 10% coarse, subrounded, chert grains. Gravel is subrounded chert without (?) iron patina, 0.3- to 1.0-inch diameter	HU1
12.7	15.2	Silt with little Clay and little Gravel, 10YR7/3 (very pale brown), moderately hard, nonplastic, and moist. Gravel is subrounded chert without iron patina	
15.2	17.6	Silt with Gravel and little Clay, 10YR7/3 (very pale brown) GRADING DOWN to 10YR7/1 (light gray), moderately hard, nonplastic, and moist. Gravel is subrounded chert without iron patina, 0.3- to 1.0-inch diameter	
17.6	18.1	Sand, 10YR7/4 (very pale brown), firm and moist. Sand is fine to medium, subrounded, quartz grains	
18.1	18.6	Sand 10YR7/4 (very pale brown) firm and moist Sand	
18.6	19.1	Sand with some Gravel, 10YR7/4 (very pale brown), firm, and moist. Sand is fine quartz grains. Gravel is subrounded chert without (?) iron patina, 0.3- to 0.4- inch diameter	
19.1	21.8	Sand with some Gravel, 10YR8/2 (very pale brown), firm and moist Sand is fine quartz grains. Gravel is	
21.8	22.5	Sand with some Gravel, 7.5YR6/4 (light brown), dense, and moist. Sand is 70% fine quartz grains and 30% coarse-to-very-coarse, subrounded chert grains. Gravel is subrounded to rounded chert without (?) iron patina, 0.3- to 0.4-inch diameter	
22.5	24.9	Sand with little Gravel, 10YR7/1 (light gray) mottled with 10YR7/3 (very pale brown), firm, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert, with and without iron patina, 4 mm- to 0.6-inch diameter	HU2

## Plant North -2607.459, Plant East -5258.754

<u>г</u>			
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
24.9	25.8	Sand, 7.5YR7/6 (reddish yellow), firm, and moist. Sand is fine quartz grains	
25.8	27.0	Silt, 10YR8/2 (very pale brown) with 7.5YR7/6 (reddish yellow) laminations, moderately soft, nonplastic, and moist	
27.0		Sand, 10YR8/2 (very pale brown), lightly consolidated, and moist. Sand is 90% fine quartz grains and 10% coarse, rounded, chert grains	
28.1	28.8	Silt as 25.8 to 27.0 ft	
28.8	29.5	Sand, 10YR8/2 (very pale brown), firm, and moist. Sand is very fine quartz grains	
29.5	31.0	Gravelly Sand, 10YR7/3 (very pale brown), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert with iron patina, 0.3- to 0.6-inch diameter	
31.0	31.5	Silt, 10YR8/2 (very pale brown), soft, plastic, and moist	
31.5	36.4	Gravelly Sand as 29.5 to 31.0 ft	
36.4		Silty Sand, 10YR8/2 (very pale brown) with some 7.5YR7/6 (reddish yellow) laminations, firm, and moist. Sand is very fine quartz grains	
39.0	40.2	Silt with little Clay, 10YR7/2 (light gray) mottled with 10YR7/4 (very pale brown), moderately soft, moderately plastic, and moist	
40.2	47.0	Silt with some Clay, 7.5YR7/4 (pink) with some 7.5YR8/1 (white) mottling, moderately hard, slightly plastic, and moist	
47.0	53.9	Silt, 7.5YR8/1 (white) mottled with 7.5YR7/6 (reddish yellow), moderately hard, slightly plastic, and moist	HU3
53.9	56.7	Silt, 7.5YR6/8 (reddish yellow), hard, nonplastic, and moist	
56.7	58.2	Silt, 7.5YR8/1 (white), moderately hard, nonplastic, and moist	
58.2	59.0	Silt with Sand, 10YR8/3 (very pale brown) with 7.5YR7/6 (reddish yellow) mottling, soft, nonplastic, and moist. Sand is fine quartz grains	
59.0	62.5	Sand with a few blebs of Silt, 10YR8/2 (very pale brown) with some 7.5YR7/6 (reddish yellow) staining and mottling, firm and moist. Sand is fine quartz grains. Silt blebs are 10YR8/2 (very pale brown), soft, plastic, and moist.	HU4

## Plant North -2630.55, Plant East -5241.133

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	1.4	Gravelly Sand with little Silt, 2.5YR6/6 (light red), dense, and moist. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 4-mm to 0.4-inch diameter	
1.4	2.0	Gravel, 10YR7/1 (light gray), dense, and moist. Gravel is subangular limestone, 4-mm to 0.3-inch diameter: dense gravel aggregate/DGA	FILL
2.0	2.6	Gravelly Sand, 2.5YR6/6 (light red), dense, and moist. Sand is fine quartz grains. Gravel is subrounded chert with iron patina, 4-mm to 0.4-inch diameter	
2.6	12.1	Silt, 10YR7/1 (light gray) with little 10YR7/4 (very pale brown) mottling GRADING DOWN to 7.5YR7/6 (reddish yellow), soft, nonplastic, and moist	
12.1	12.7	Sand, 10YR8/2 (very pale brown), dense, and moist. Sand is very fine quartz grains	
12.7	14.0	Sand, 10YR7/6 (yellow), firm, and moist WITH thin Silt interbeds, 10YR8/2 (very pale brown), soft, plastic, and moist. Sand is fine quartz grains	
14.0	14.4	Sandy Silt with some Gravel, 7.5YR6/6 (reddish yellow), soft, nonplastic, and moist	HU1
14.4	17.5	Silt with little Clay and Gravel, 10YR7/3 (very pale brown), moderately soft, plastic, and moist. Gravel is subrounded chert without iron patina, 0.4-inch diameter	
17.5	18.6	Silt with Sand and Gravel, 10YR7/1 (light gray), soft, nonplastic, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert with and without iron patina, 0.3- to 0.6-inch diameter	
18.6	23.9	Sand with Gravel and little Silt, 7.5YR7/6 (reddish yellow), dense, and moist. Sand is 70% fine quartz grains and 30% coarse, subrounded, chert grains. Gravel is subrounded to subangular chert with iron patina, 0.3-to 0.8-iinch diameter	
23.9	25.8	Sand, 10YR8/4 (very pale brown), firm-to-lightly- consolidated, and moist. Sand is fine quartz grains	
25.8	26.8	Silt with little Sand, 10YR7/6 (yellow) mottled with 10YR8/1 (white), soft, moderately plastic, and moist. Sand is fine quartz grains	
26.8	27.4	Gravelly Sand, 10YR8/2 (very pale brown), dense, and moist. Sand is fine quartz grains. Gravel is subangular to subrounded chert with(?) iron patina, 0.5- to 0.6-inch diameter	HU2
27.4	27.6	Sand, 10YR8/1 (white), firm, and moist. Sand is fine quartz grains	
27.6	30.3	Gravelly Sand as 26.8 to 27.4 ft	

#### Plant North -2630.55, Plant East -5241.133

		Flaint North -2050.55, Flaint East -5241.155	10/18/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
30.3	31.5	Sand, 10YR8/1 (white), firm, and moist. Sand is fine quartz grains	
31.5	32.4	Sand with Gravel, 10YR8/1 (white), firm, and moist. Sand is fine quartz grains. Gravel is subrounded to rounded chert without iron patina, 0.3- to 0.5-inch diameter	
32.4		Silt with some Sand, 10YR8/1 (white), soft, nonplastic to moderately plastic, and moist. Sand is very fine quartz grains	
39.0	43.2	Silt with some Clay, 10YR8/1 (white) mottled with 10YR7/6 (yellow), soft, plastic, and moist	
43.2	51.6	Silt with some Clay, 7.5YR7/4 (pink) mottled with 7.5YR8/1 (white), moderately soft, moderately plastic, and moist	
51.6	52.5	Silt with Sand (soft, moderately plastic, and moist) GRADING DOWN to Sand (firm and moist), 7.5YR6/6 (reddish yellow) mottled with 7.5YR8/1 (white). Sand is very fine quartz grains	HU3
52.5	55.5	Silt with little Clay, 7.5YR6/6 (reddish yellow) with little 7.5YR8/1 (white) mottling, moderately hard/stiff, nonplastic to slightly plastic, and moist	
55.5	58.7	Silty Sand, 10YR8/2 (very pale brown) with 10YR7/76 (yellow) laminations, firm, and moist. Sand is very fine quartz grains	
58.7	62.5	Sand, 10YR8/4 (very pale brown), firm and moist to loose and wet. Sand is fine quartz grains but for interval of coarse, rounded, quartz grains at 62.0 to 62.1 ft	HU4

# Plant North -2603.36, Plant East -5105.973

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	2.2	subrounded to subangular chert with iron patina, 4 mm- to 0.5-inch diameter	
2.2	15.2	Silt, 10YR7/1 (light gray) with little 10YR7/4 (very pale brown) GRADING DOWN to 10YR7/3 (very pale brown), soft, nonplastic, and moist	HU1
15.2	18.3	Silt with little Clay and little Gravel, 10YR7/1 (light gray) mottled with 10YR7/4 (very pale brown), moderately hard, slightly plastic, and moist. Gravel is subrounded to subangular chert without iron patina, 0.3- to 0.9-inch diameter	
18.3	19.1	Sand with Gravel, 10YR7/4 (very pale brown), dense, and moist. Sand is 70% fine quartz grains and 30% coarse, subrounded, chert grains. Gravel is subrounded chert without iron patina, 0.3- to 0.5-inch diameter	
19.1	20.0	Sand with trace of Gravel, 7.5YR7/6 (reddish yellow), dense, and moist. Sand is 85% fine quartz grains and 15% coarse, subrounded, chert grains. Gravel is chert, 0.3- to 0.5-inch diameter	
20.0	20.9	Sand with Gravel as 18.3 to 19.1 ft	
20.9	21.3	Silt with Sand, 10YR7/1 (light gray), moderately hard, nonplastic, and moist. Sand is very fine quartz grains	HU2
21.3	22.5	Sand with Gravel as 18.3 to 19.1 ft	
22.5	27.5	Silty Sand, firm, and moist; interbedded with Silt with little Clay, moderately hard, slightly plastic, and moist; 10YR7/1 (light gray) mottled with 7.5YR7/6 (reddish yellow). Sand is very fine quartz grains	
27.5	28.2	Silty Sand with Gravel, 10YR7/1 (light gray) mottled with 7.5YR7/6 (reddish yellow), firm, and moist. Sand is very fine quartz grains. Gravel is subrounded chert without iron patina, 0.3- to 0.8-inch diameter	
28.2	28.5	Silt with Sand, 10YR7/1 (light gray), moderately soft, moderately plastic, and moist. Sand is very fine quartz grains	
28.5	32.0	Sand with Gravel and with little Silt, 7.5YR7/4 (pink), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert without iron patina, 0.3- to 0.4-inch diameter (and trace 1.0-inch diameter)	
32.0	42.3	Silt, 10YR7/3 (very pale brown) GRADING DOWN to 10YR8/2 (very pale brown) with 10YR7/6 (yellow) laminations, soft to moderately soft, nonplastic to slightly plastic, and moist	

#### Plant North -2603.36, Plant East -5105.973

-		Plant North -2003.30, Plant East -5105.973	10/18/2012
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
42.3	45.5	Silt with little Clay, 7.5YR7/4 (pink) mottled with 7.5YR7/1 (white), moderately hard, slightly to moderately plastic, and moist	
45.5	46.5	Silty Sand, 7.5YR6/6 (reddish yellow) with some 7.5YR8/1 (white) mottling, firm, and moist. Sand is very fine quartz grains	
46.5	48.5	Sand with trace of Gravel, 7.5YR6/6 (reddish yellow) mottled with 7.5YR8/1 (white), firm, and moist. Sand is fine quartz grains. Gravel is subrounded chert without iron patina, 0.3- to 0.7-inch diameter	HU3
48.5	50.3	Silt, 10YR7/4 (very pale brown) mottled with 10YR8/1 (white), moderately hard, nonplastic, and moist	
50.3	52.2	Silt, 10YR7/3 (very pale brown) mottled with 7.5YR7/6 (reddish yellow), soft, moderately plastic, and moist	
52.2	53.6	Silty Sand, 10YR8/2 (very pale brown) mottled with 10YR7/6 (yellow), firm, and moist. Sand is very fine quartz grains	
53.6	57.7	Silt, 7.5YR7/6 (reddish yellow) mottled with 7.5YR8/1 (white), moderately soft, moderately plastic, and moist	
57.7	59.0	Silty Sand, 10YR8/4 (very pale brown) mottled with 10YR8/1 (white), firm, and moist. Sand is very fine quartz grains	
59.0	59.6	Silt with Sand, 10YR7/6 (yellow), soft, nonplastic, and moist. Sand is very fine quartz grains	
59.6	67.5	Sand, 10YR8/4 (very pale brown), lightly consolidated and moist TO loose and wet WITH a few blebs of Clay, 10YR8/2 (very pale brown), soft, plastic, and moist. Sand is fine quartz grains	HU4

## Plant North -2627.587, Plant East -5106.145

10/19/2012

Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
0.0	1.3	Fill: Sand with Gravel and little Silt, 2.5YR6/6 (light red), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to rounded chert with iron patina, 0.3-inch diameter	
1.3	1.5	Fill: Gravel, 10YR7/2 (light gray), loose, and moist. Gravel is subangular to subrounded limestone, 4 mm- to 0.5-inch diameter (dense gravel aggregate/DGA)	Fill
1.5	2.6	Fill: Sand with Gravel, 2.5YR6/6 (light red), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to rounded chert with iron patina, 0.3-inch diameter	
2.6	14.5	Silt, 10YR7/1 (light gray) mottled with 10YR7/6 (yellow) GRADING DOWN at 13.1 ft to 10YR7/6 (yellow) mottled with 10YR5/4 (yellowish brown) and 10YR7/1 (light gray), soft, nonplastic, and moist	
14.5	16.7	Silt with little Clay and little Gravel, 10YR7/1 (light gray), moderately soft, moderately plastic, and moist. Gravel is subrounded to subangular chert without iron patina, 4 mm- to 0.3-inch diameter	
16.7	18.3	Silt with Gravel and little Clay, 10YR7/1 (light gray) mottled with 7.5YR7/4 (pink), moderately soft, moderately plastic, and moist. Gravel is subrounded chert without iron patina, 0.5- to 1.1 inch diameter	
18.3	20.0	subangular to subrounded chert without iron patina, 0.3- to 0.5-inch diameter	HU2
20.0	20.2	Gravelly Sand, 7.5YR6/4 (light brown), dense, and moist. Sand is 65% fine quartz grains and 35% coarse, subrounded, chert grains. Gravel is subrounded to subangular chert without iron patina, 0.3- to 0.5-inch diameter	
20.2	22.0	Silt with Sand, 10YR8/2 (very pale brown) with some 10YR7/6 (yellow) mottling, soft, nonplastic, and moist. Sand is very fine quartz grains	
22.0	22.4	Silt with Gravel and little Clay as at 16.7 to 18.3 ft but colored 7.5YR6/2 (pinkish gray)	
22.4	23.0	Gravelly Sand as 20.0 to 20.2 ft	
23.0	24.2	Silt, 10YR8/1 (white) mottled with 10YR8/3 (very pale brown), soft, nonplastic, and moist	
24.2	25.3	Sand, 10YR8/1 (white) with 10YR7/4 (very pale brown) mottling, firm, and moist. Sand is fine quartz grains	

# Plant North -2627.587, Plant East -5106.145

10/19/2012

1		,	
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
25.3	30.0	Sand with some Gravel, 10YR8/2 (very pale brown) GRADING DOWN to 10YR6/6 (brownish yellow), dense, and moist. Sand is 85% fine quartz grains and 15% coarse to very coarse, subrounded, chert grains. Gravel is subrounded to subangular chert without iron patina, 0.3- to 0.4-inch diameter	HU3
30.0	30.5	Sand, 10YR8/3 (very pale brown), firm, and moist. Sand is fine quartz grains	HU3
30.5	31.9	Gravelly Sand, 10YR7/4 (very pale brown), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert with and without iron patina, 4 mm- to 0.8-inch diameter (poorly sorted)	
31.9	32.2	is fine quartz grains	
32.2	37.5	Silt with Sand, 7.5YR8/6 (reddish yellow), soft, nonplastic, and moist. Sand is fine quartz grains	
37.5	42.2	Silt, 10YR7/4 (pink) with some 10YR8/1 (white) mottling, soft, nonplastic to moderately plastic, and moist	
42.2	44.2	Silt with little Clay, 7.5YR7/4 (pink) with some 7.5YR6/6 (reddish yellow) mottling, moderately soft GRADING DOWN to soft, moderately plastic, and moist	
44.2	45.9	Silt 7 5VP7/6 (reddish vellow) with little 7 5VP8/1	
45.9	47.9	Silt with Sand, 7.5YR7/6 (reddish yellow) mottled with 7.5YR8/1 (white), soft, nonplastic, and moist. Sand is very fine quartz grains	
47.9	50.6	Sand 10VR8/2 (very nale brown) firm and moist Sand	HU3
50.6	51.4	Silt with Sand, 10YR8/2 (very pale brown), soft, slightly plastic, and moist. Sand is very fine quartz grains	
51.4	52.3	Silt with Clay, 7.5YR8/2 (pinkish white) mottled with 7.5YR7/4 (pink), soft, plastic, and moist	
52.3	52.9	Silt with Sand, 10YR8/2 (very pale brown), soft, slightly plastic, and moist. Sand is very fine quartz grains	
52.9	53.6	is fine quartz grains	
53.6	57.6	Silt, 7.5YR8/2 (pinkish white) with 7.5YR7/4 (pink) mottling, soft, plastic, and moist	
57.6	59.7	Sand (fine quartz grains), 10YR8/6 (yellow), firm, and moist interbedded with Silt, 10YR8/3 (very pale brown), soft, nonplastic, and moist	
59.7	62.4	Sand 10YR7/6 (vellow) firm and moist Sand is fine	

Plant North -2627.587, Plant East -5106.145

10/19/2012

		,	
Start Depth (ft bgs)	End Depth (ft bgs)	Lithology	Hydrogeologic Unit
62.4	62.7	Gravelly Sand, 10YR8/1 (white), dense, and moist. Sand is fine quartz grains. Gravel is subrounded to subangular chert with iron patina, 0.4- to 0.5-inch diameter	HU4
62.7	65.0	Sand, 10YR8/2 (very pale brown), firm and moist to loose and wet. Sand is fine quartz grains	

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**APPENDIX E** 

SUMMARY OF SOILS VOC DATA FOR SWMU 211-A

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## SWMU 211-A VOC Analyes

Station	Date Collected	Sample Depth [ft bls]	TCI [µg/k		1,1-DC [µg/kg		<i>cis</i> -1,2 DCE [µg/kg	1	trans-1, DCE [µg/kg		VC [µg/k	g]
			75		137		619		5290		570	
		0.5	0.44	U	1.8	U	0.67	U	1.1	U	0.48	U
		7.5	0.42	U	1.7	U	0.65	U	1	U	0.46	U
		10.1	0.39	U	1.6	U	0.61	U	0.95	U	0.43	U
		(10.1)DUP	0.38	U	1.6	U	0.58	U	0.91	U	0.42	U
		19.9	9.7		1.4	U	0.54	U	0.84	U	0.39	U
		24.9	4	J	1.5	U	0.55	U	0.86	U	0.39	U
211-A-	8/29/2012	25.5	14		1.2	U	0.46	U	0.72	U	0.33	U
001		34.5	3.1	J	1.4	U	0.52	U	0.81	U	0.37	U
		35.5	0.45	J	1.3	U	0.5	U	0.78	U	0.36	U
		44.5	0.36	U	1.5	U	0.56	U	0.88	U	0.4	U
		46.5	0.36	U	1.5	U	0.55	U	0.86	U	0.39	U
		50.1	0.37	U	1.5	U	0.57	U	0.89	U	0.41	U
		59	11		1.7	U	0.63	U	0.99	U	0.45	U
		Average	3.4		***		***		***		***	
		4.5	2.1	J	1.8	U	0.69	J	1	U	0.47	U
		6	23		1.6	U	9.4	J	0.93	U	0.43	U
		11	12		1.6	U	3.2	J	0.92	U	0.42	U
		16	0.34	U	1.4	U	0.52	U	0.82	U	0.37	U
		21	9.5		1.5	U	2	J	0.88	U	0.4	U
		25.5	0.47	J	1.5	U	0.55	U	0.85	U	0.39	U
	8/30/2012	32.5	10		1.6	U	0.92	J	0.93	U	0.42	U
211-A- 002		(32.5)DUP	2.4	J	1.4	U	0.53	U	0.83	U	0.38	U
002		36.5	1,100		27	U	11	U	8.9	U	30	U
		40.5	880		22	U	9.6	U	7.5	U	26	U
		45.5	140		1.5	U	0.58	U	0.9	U	0.41	U
		50.1	2.5	J	1.6	U	0.6	U	0.93	U	0.43	U
		59.9	65		2	J	0.61	U	0.96	U	0.44	U
	8/31/2012	62.5	8.7	J	1.6	U	0.58	U	0.91	U	0.42	U
		Average	161		2.5		2.0		***		***	

Station	Date Collected	Sample Depth [ft bls]	TCI [µg/k		1,1-DC [µg/kg		<i>cis</i> -1,2 DCE [µg/kg		trans-1, DCE [µg/kg		VC [µg/k	g]
			75		137		619		5290		570	
		4	0.39	U	1.6	U	0.6	U	0.94	U	0.43	U
		9	0.38	U	1.6	U	0.58	U	0.91	U	0.42	U
		14	0.39	U	1.6	U	0.6	U	0.94	U	0.43	U
		19	0.38	U	1.6	U	0.58	U	0.91	U	0.42	U
		(21.5)DUP	0.34	U	1.4	U	0.52	U	0.81	U	0.37	U
		21.5	0.34	U	1.4	U	0.52	U	0.81	U	0.37	U
	9/12/2012	28.5	0.31	U	1.3	U	0.48	U	0.75	U	0.34	U
211-A-003	9/12/2012	34.9	8.7	J	1.6	U	0.6	U	0.95	U	0.43	U
		39.5	110		17		1.8	J	0.83	U	0.38	U
		40.1	80		19		0.85	J	0.94	U	0.43	U
		48	52		12		1.2	J	0.89	U	0.41	U
		54	4.4	J	1.5	U	0.56	U	0.87	U	0.4	U
		59	0.39	U	1.6	U	0.59	U	0.93	U	0.43	U
		64	0.36	U	1.9	J	0.56	U	0.87	U	0.4	U
		Average	18		4.1		0.5		***		***	
		4	0.39	U	1.6	U	0.59	U	0.93	U	0.42	U
		9	0.38	U	1.6	U	0.59	U	0.92	U	0.42	U
		14	0.36	U	1.6	J	0.56	U	0.87	U	0.4	U
		16.5	0.33	U	18		0.5	U	0.79	U	0.36	U
	8/31/2012	24.9	1,700		1,600		9.6	U	7.5	U	26	U
		27	960		970		9.4	J	7.3	U	25	U
211 4 004		30.1	620		900		20	J	6.2	U	21	U
211-A-004		35.1	1,200		1,400		20	J	8.1	U	28	U
		40.1	2,400		4,400		29	J	8.3	U	28	U
		48.5	17	U	480		9.9	U	7.7	U	26	U
	9/4/2012	53.5	33	J	110	J	10	U	8.2	U	28	U
	9/4/2012	59.9	97		12		10	J	1.1	U	0.51	U
		61	160		23		14		1.1	U	0.49	U
		Average	552		763		9.1		***		***	

Station	Date Collected	Sample Depth [ft bls]	TCI [µg/k		1,1-DC [µg/kg		<i>cis</i> -1,2 DCE [µg/kg		trans-1, DCE [µg/kg		VC [µg/kậ	g]
			75		137		619		5290		570	
		4	19	U	26	U	11	U	8.8	U	30	U
		6	1,700		24	U	15	J	8.2	U	28	U
		14	88		1.5	U	11		0.88	U	7.6	J
		15.1	35		1.6	U	4.7	J	0.92	U	1.5	J
		(15.1)DUP	42		1.5	U	6.4	J	0.9	U	2	J
		23.5	17		9.3		2	J	0.81	U	0.37	U
	9/4/2012	26	13		1.3	U	2.2	J	0.75	U	0.35	U
211-A-005	9/4/2012	34.9	54		130		1.4	J	0.88	U	0.4	U
		35.5	190	J	840		11	U	8.4	U	29	U
		43.5	96	J	690		10	U	7.9	U	27	U
		45.5	71	J	550		10	U	7.8	U	27	U
		53	11		8.8	J	0.6	J	0.86	U	0.4	U
		55.5	6.5	J	3.2	J	0.84	J	0.95	U	0.43	U
		60.5	120		24		7.1	J	0.9	U	0.41	U
		Average	175		163		5.2		***		5.9	
		4	0.39	U	1.6	U	0.6	U	0.94	U	0.43	U
		(4)DUP	1.8	J	1.7	U	0.65	J	0.98	U	0.45	U
		9	0.43	U	1.8	U	0.66	U	1	U	0.47	U
		14	0.38	U	1.6	U	0.59	U	0.93	U	0.42	U
		18.5	0.41	U	1.7	U	0.63	U	0.99	U	0.45	U
		23.5	0.32	U	1.3	U	0.49	U	0.77	U	0.35	U
	0/06/0010	29	0.36	U	1.5	U	0.56	U	0.88	U	0.4	U
211-A-006	9/26/2012	32	1.1	J	1.3	U	0.49	U	0.77	U	0.35	U
		39	13		32		0.83	J	0.97	U	0.44	U
		40.5	8	J	22		0.59	U	0.92	U	0.42	U
		49	8.7		17		0.51	U	0.8	U	0.37	U
		51	7.1	J	9.5	J	0.6	U	0.94	U	0.43	U
		59.5	24		7.2	J	1	J	1	U	0.48	U
		61	52		9.4	J	2.9	J	1.1	U	0.51	U
		Average	8.3		7.4		0.6		***		***	

Station	Date Collected	Sample Depth [ft bls]	TCI [µg/k		1,1-DC [µg/kg		<i>cis</i> -1,2 DCE [µg/kg		trans-1, DCE [µg/kg		VC [µg/kş	g]
			75		137		619		5290		570	
		4	0.39	U	1.6	U	0.6	U	0.94	U	0.43	U
		(9)DUP	0.54	U	2.2	U	0.83	U	1.3	U	0.6	U
		9	0.49	U	2	U	0.75	U	1.2	U	0.54	U
		13.5	0.43	U	1.8	U	0.66	U	1	U	0.47	U
		19	0.38	U	1.6	U	0.59	U	0.92	U	0.42	U
		24.9	0.45	U	1.9	U	0.69	U	1.1	U	0.5	U
	9/20/2012	29	0.4	U	1.6	U	0.61	U	0.96	U	0.44	U
211-A-008	9/20/2012	33.5	0.37	U	1.5	U	0.56	U	0.88	U	0.4	U
		39	0.36	U	1.5	U	0.56	U	0.87	U	0.4	U
		41	0.38	U	1.6	U	0.58	U	0.91	U	0.42	U
		49.9	0.37	U	1.5	U	0.56	U	0.88	U	0.4	U
		53.5	5.3	J	1.5	U	0.58	U	0.9	U	0.41	U
		59	34		6.5	J	0.67	U	1	U	0.48	U
		61.5	130		78		4.2	J	1.1	U	0.52	U
		Average	12		6.8		0.6		***		***	
		4	0.43	U	1.8	U	0.66	U	1	U	0.48	U
		9	0.44	U	1.8	U	0.68	U	1.1	U	0.49	U
		14	0.43	U	1.8	U	0.66	U	1	U	0.47	U
		19	8.7	J	1.7	U	0.62	U	0.98	U	0.45	U
		22.5	1.7	J	1.7	U	0.64	U	1	U	0.46	U
		(29)DUP	13		1.5	U	0.55	U	0.87	U	0.4	U
	9/20/2012	29	11		1.6	U	0.6	U	0.94	U	0.43	U
211-A-009	9/20/2012	34	2.4	J	2.5	J	0.57	U	0.89	U	0.41	U
		39.5	160	J	25	U	11	U	8.5	U	29	U
		40.1	110		1.5	U	0.54	U	0.85	U	0.39	U
		49	1.8	J	1.8	U	0.68	U	1.1	U	0.48	U
		54	32		3.6	J	0.56	U	0.88	U	0.4	U
		59.9	<b>190</b>		38		1.9	J	0.92	U	0.42	U
		60.1	33		3.3	J	0.64	J	0.93	U	0.43	U
		Average	40		4.8		0.8		***		***	

Station	Date Collected	Sample Depth [ft bls]	TCI [µg/k		1,1-DC [µg/kg		<i>cis</i> -1,2 DCE [µg/kg		trans-1, DCE [µg/kg		VC [µg/kş	g]
			75		137		619		5290		570	
		4	0.39	U	1.6	U	0.6	U	0.95	U	0.43	U
	8/16/2012	9.5	0.46	J	1.6	U	0.6	U	0.94	U	0.43	U
	8/10/2012	14.5	0.42	U	1.7	U	0.64	U	1	U	0.46	U
		19.9	14		1.4	U	11		0.8	U	0.37	U
		24	2.7	J	1.4	U	0.51	U	0.81	U	0.37	U
		26	25		1.5	U	0.91	J	0.89	U	0.41	U
211-A-010		33	<mark>790</mark>		22	U	9.5	U	7.4	U	25	U
211-A-010	9/13/2012	38.5	500		26	U	11	U	8.6	U	29	U
		40.1	280		22	U	9.6	U	7.5	U	25	U
		48	1.4	J	1.5	U	0.57	U	0.9	U	0.41	U
		52	0.32	U	1.3	U	0.49	U	0.76	U	0.35	U
	9/17/2012	59	15		1.6	U	0.61	U	0.96	U	0.44	U
	9/17/2012	60.5	120		2.2	J	1.3	J	1.1	U	0.52	U
		Average	135		3.4		2.3		***		***	
		4	0.39	U	1.6	U	0.6	U	0.93	U	0.43	U
		9	0.42	U	1.7	U	0.64	U	1	U	0.46	U
		(11)DUP	0.39	U	1.6	U	0.6	U	0.95	U	0.43	U
		11	0.39	U	1.6	U	0.6	U	0.94	U	0.43	U
		19.5	0.39	U	1.6	U	0.59	U	0.93	U	0.43	U
		20.1	0.39	U	1.6	U	0.6	U	0.94	U	0.43	U
	8/17/2012	27.5	0.34	U	1.4	U	0.52	U	0.82	U	0.37	U
211-A-011	0/17/2012	30.5	0.35	U	1.5	U	0.54	U	0.85	U	0.39	U
		36.5	60		17		0.86	J	1.2	U	0.55	U
		40.1	76		20		0.64	U	1	U	0.46	U
		49.5	11		2.9	J	0.67	U	1	U	0.48	U
		51.5	3.2	J	1.5	U	0.55	U	0.86	U	0.39	U
		59.9	8.3	J	19		0.68	U	1.1	U	0.49	U
		62.5	8.6	J	28		0.6	U	0.94	U	0.43	U
		Average	12		6.7		0.3		***		***	

Station	Date Collected	Sample Depth [ft bls]	TCF [µg/k		1,1-DC [µg/kg		cis-1,2 DCE [µg/kş		trans-1, DCE [µg/kg		VC [µg/kş	g]
			75		137		619		5290		570	
		4	0.46	U	1.9	U	0.7	U	1.1	U	0.5	U
		9	0.4	U	1.6	U	0.61	U	0.96	U	0.44	U
		14	0.41	U	1.7	U	0.63	U	0.99	U	0.45	U
		(19)DUP	0.39	U	1.6	U	0.59	U	0.93	U	0.43	U
		19	0.39	U	1.6	U	0.6	U	0.94	U	0.43	U
		20.5	0.36	U	1.5	U	0.55	U	0.86	U	0.39	U
	9/17/2012	26.5	0.34	U	1.4	U	0.52	U	0.81	U	0.37	U
211-A-012	9/17/2012	31	0.44	U	1.8	U	0.67	U	1.1	U	0.48	U
		36.5	0.35	U	1.4	U	0.53	U	0.84	U	0.38	U
		40.1	20		23		0.88	J	0.97	U	0.45	U
		49	16		11		1.5	J	0.86	U	0.39	U
		54	5.1	J	1.6	J	0.55	U	0.86	U	0.39	U
		59	12		50		1.2	J	1	U	0.46	U
		64.5	14		55		1.3	J	0.94	U	0.43	U
		Average	4.9		11		0.6		***		***	
		4.9	0.34	U	1.4	U	0.52	U	0.81	U	0.37	U
		6.5	5.7	J	1.6	U	12		0.96	U	0.44	U
		14	42		1.6	U	22		0.93	U	3	J
		18.5	0.37	U	1.5	U	0.57	U	0.9	U	0.41	U
	9/4/2012	20.5	9.3		1.4	U	2.1	J	0.84	U	0.38	U
		26.5	3.3	J	1.4	U	0.92	J	0.81	U	0.37	U
211 A 012		30.1	22		7.8	J	2.9	J	0.81	U	0.39	J
211-A-013		35.5	29		5.1	J	1.3	J	0.87	U	0.4	U
		44.5	170	J	350		9.4	U	7.4	U	25	U
		47.5	78	J	180	J	9.7	U	7.6	U	26	U
	9/5/2012	53.5	13		11		0.7	J	0.99	U	0.45	U
	9/3/2012	55.1	13		12		0.76	J	0.91	U	0.42	U
		64	56		13		4.8	J	0.99	U	0.45	U
		Average	34		45		4.4		***		2.4	

Station	Date Collected	Sample Depth [ft bls]	TCI [µg/k		1,1-DC [µg/kg		<i>cis</i> -1,2 DCE [µg/kg		trans-1, DCE [µg/kg		VC [µg/kậ	g]
			75		137		619		5290		570	
		4	0.39	U	1.6	U	0.6	U	0.93	U	0.43	U
		9	0.4	U	24		0.61	U	0.96	U	0.44	U
		14	0.41	U	6.1	J	0.63	U	0.98	U	0.45	U
		19	0.33	U	1.4	U	0.51	U	0.8	U	0.36	U
		24.5	0.34	U	1.4	U	0.52	U	0.81	U	0.37	U
		29.5	0.31	U	1.7	J	0.48	U	0.75	U	0.35	U
	9/5/2012	34.5	18		22		1.1	J	0.88	U	0.4	U
211-A-014	)/5/2012	(36.5)DUP	28		43		1.6	J	0.81	U	0.37	U
		36.5	0.35	U	1.5	U	0.54	U	0.85	U	0.39	U
		42	59		140		3.5	J	0.84	U	0.38	U
		45.1	24		57		0.93	J	0.78	U	0.36	U
		50.5	26		34		0.6	J	0.87	U	0.4	U
		56	2.4	J	1.4	U	0.53	U	0.83	U	0.38	U
		63.5	16		7.6	J	1.7	J	0.95	U	0.44	U
		Average	12		24		0.8		***		***	
		4.5	0.41	U	1.7	U	0.63	U	0.99	U	0.45	U
		6	0.41	U	1.7	U	0.64	U	1	U	0.46	U
		14	0.38	U	1.6	U	0.58	U	0.91	U	0.42	U
		19	0.37	U	1.5	U	0.56	U	0.88	U	0.4	U
		24	0.31	U	1.3	U	0.48	U	0.75	U	0.34	U
		25.5	0.35	U	1.4	U	0.53	U	0.84	U	0.38	U
211-A-015	9/6/2012	34	20		30		1	J	0.83	U	0.38	U
211-A-013		39	51		83		1.4	J	0.86	U	0.39	U
		44.9	47		22		0.54	U	0.85	U	0.39	U
		46.5	120		24		0.71	J	0.84	U	0.39	U
		50.1	130		5.9	J	0.56	U	0.88	U	0.4	U
		59.9	57		47		1.9	J	0.91	U	0.42	U
		63	36		25		3.3	J	1	U	0.46	U
		Average	36		19		0.8		***		***	

Station	Date Collected	Sample Depth [ft bls]	TCI [µg/k		1,1-DC [µg/kg		cis-1,2 DCE [µg/kş	1	trans-1, DCE [µg/kg		VC [µg/kş	g]
			75		137		619		5290		570	
		0.1	0.39	U	1.6	U	0.6	U	0.94	U	0.43	U
		6	1.7	J	1.7	U	1.1	J	0.97	U	0.45	U
		14	0.48	U	2	U	0.74	U	1.2	U	0.53	U
		16.5	2.1	J	1.7	U	0.63	U	0.99	U	0.45	U
		23.5	0.38	U	1.6	U	0.59	U	0.92	U	0.42	U
		(29.9)DUP	34		3.7	J	0.52	U	0.82	U	0.37	U
	0/07/0010	29.9	33		4.4	J	0.48	U	0.75	U	0.34	U
211-A-016	9/27/2012	30.5	86		18		0.56	U	0.88	U	0.4	U
		35.1	6.4	J	4.8	J	0.64	U	1	U	0.46	U
		43	26	J	26	U	11	U	8.7	U	29	U
		46.5	300		22	U	9.5	U	7.4	U	25	U
		54	150		8.6		0.54	J	0.81	U	0.37	U
		55.1	89	J	25	U	11	U	8.3	U	28	U
		62.5	90		110		4.1	J	1.3	U	0.58	U
		Average	58		14		1.7		***		***	
		1	0.48	U	2	U	0.74	U	1.2	U	0.53	U
		9	2.4	J	1.9	U	6.4	J	1.1	U	0.5	U
		14	2.2	J	1.6	U	21		0.94	U	0.59	J
		18	79		1.4	U	9.5		0.83	U	0.38	U
		(22.5)DUP	31		1.8	U	7.7	J	1.1	U	0.49	U
		22.5	29		1.4	U	7.2	J	0.84	U	0.38	U
	0/01/0010	29.5	1,500		26	U	11	U	8.8	U	30	U
211-A-017	9/21/2012	30.1	1,600		22	U	9.6	U	7.5	U	25	U
		39	190		1.8	U	3	J	1.1	U	0.48	U
		41.5	64		1.5	U	0.86	J	0.87	U	0.4	U
		49	9	J	1.5	U	0.57	U	0.89	U	0.41	U
		52.5	23		1.5	U	0.71	J	0.85	U	0.39	U
		59	180	J	29	U	12	U	9.7	U	33	U
		61.5	150	J	23	U	10	U	7.9	U	27	U
		Average	276		***		5.6		***		4.3	

Station	Date Collected	Sample Depth [ft bls]	TCI [µg/k		1,1-DC [µg/kg		<i>cis-</i> 1,2 DCE [µg/kg		trans-1 DCE [µg/kg		VC [µg/kậ	g]
			75		137		619		5290		570	
		0.5	0.4	U	1.7	U	0.62	U	0.97	U	0.44	U
		6.5	0.42	U	1.7	U	0.64	U	1	U	0.46	U
		(11)DUP	0.4	U	1.7	U	0.62	U	0.97	U	0.45	U
		11	0.36	U	1.5	U	0.55	U	0.87	U	0.4	U
		19.9	0.34	U	1.4	U	0.52	U	0.81	U	0.37	U
		21	0.36	U	1.5	U	0.56	U	0.88	U	0.4	U
	9/11/2012	28.5	0.32	U	1.3	U	0.5	U	0.78	U	0.36	U
211-A-018		33	0.35	U	1.5	U	0.54	U	0.85	U	0.39	U
		36	1.1	J	1.6	U	0.59	U	0.93	U	0.42	U
		44.9	7.7	J	4.6	J	0.52	U	0.81	U	0.37	U
		48	49		15		0.57	U	0.89	U	0.41	U
		53.5	81		23		0.61	U	0.96	U	0.44	U
		56.5	66		20		0.62	U	0.97	U	0.44	U
	9/12/2012	62	440		24	U	10	U	8.1	U	28	U
		Average	46		5.8		***		***		***	
		0.5	0.36	U	1.5	U	0.55	U	0.86	U	0.39	U
		9	0.37	U	1.5	U	0.57	U	0.9	U	0.41	U
		14	0.39	U	1.6	U	0.6	U	0.94	U	0.43	U
		19	0.32	U	1.3	U	0.49	U	0.77	U	0.35	U
		23	0.34	U	1.4	U	0.52	U	0.82	U	0.37	U
		29.5	0.34	U	1.4	U	0.52	U	0.81	U	0.37	U
211-A-019	9/12/2012	33.5	0.36	U	1.5	U	0.55	U	0.86	U	0.39	U
211-A-019		39	0.36	U	4.4	J	0.55	U	0.86	U	0.39	U
		44	0.35	U	2.4	J	0.54	U	0.85	U	0.39	U
		47	0.35	U	4.5	J	0.54	U	0.84	U	0.38	U
		54	2	J	26		0.56	U	0.88	U	0.4	U
		59	2.4	J	35		0.57	U	0.89	U	0.41	U
		64	11		59		3	J	0.93	U	0.42	U
		Average	1.3		10		0.5		***		***	

Station	Date Collected	Sample Depth [ft bls]	TCI [µg/k		1,1-DC [µg/kg		cis-1,2 DCE [µg/kg		trans-1, DCE [µg/kg		VC [µg/k	g]
			75		137		619		5290		570	
		4.5	0.43	U	1.8	U	0.67	U	1	U	0.48	U
		9	9.9	J	1.7	U	1.8	J	1	U	0.46	U
		(9)DUP	6.7	J	1.6	U	1.3	J	0.95	U	0.43	U
		11	3.9	J	1.8	U	0.7	J	1	U	0.47	U
		19	23		1.5	U	5.4	J	0.88	U	0.4	U
		20.1	12		1.9	U	3.3	J	1.1	U	0.51	U
		25.9	710		24	U	10	U	8	U	27	U
211-A-020	9/24/2012	32	210		1.9	U	4.3	J	1.1	U	0.49	U
211-A-020		35.5	<b>470</b>		25	U	11	U	8.3	U	28	U
		40.1	770		23	U	9.8	U	7.7	U	26	U
		48	800		23	U	9.8	U	7.6	U	26	U
		53.5	300		22	U	9.4	U	7.3	U	25	U
		57	800		25	U	11	U	8.5	U	29	U
		62	<b>180</b>		6.7	J	3.1	J	0.95	U	0.44	U
		65.1	160		17		4.3	J	1.1	U	0.5	U
		Average	<mark>297</mark>		6.7		3.7		***		***	
		0.1	0.36	U	1.5	U	0.56	U	0.88	U	0.4	U
		6.5	0.4	U	1.7	U	0.74	J	0.97	U	0.44	U
		14	0.38	U	1.6	U	1.2	J	0.92	U	0.42	U
		18.5	0.34	U	1.4	U	0.54	J	0.81	U	0.37	U
		24	0.33	U	1.4	U	0.51	U	0.79	U	0.36	U
		29.5	15		22		1.6	J	0.91	U	0.42	U
	9/6/2012	30.5	7.7	J	7.5	J	0.73	J	0.78	U	0.36	U
211-A-021	9/0/2012	39	46		84		3.6	J	0.89	U	0.41	U
		(44)DUP	59		110		3.8	J	0.87	U	0.47	J
		44	50		95		3.5	J	0.9	U	0.41	U
		49	46		82		3.1	J	0.81	U	0.37	U
		54	30		29		3.3	J	0.86	U	0.39	U
		55.1	7.5	J	6.2	J	1.2	J	0.93	U	0.43	U
		64	6.2	J	3.4	J	0.82	J	0.99	U	0.45	U
		Average	19		32		1.8		***		0.2	

Station	Date Collected	Sample Depth [ft bls]	TCI [µg/k		1,1-DC [µg/kg		<i>cis</i> -1,2 DCE [µg/kg		trans-1, DCE [µg/kg		VC [µg/kậ	g]
			75		137		619		5290		570	
		0.5	0.43	U	1.8	U	0.66	U	1	U	0.47	U
		6	2.7	J	1.7	U	0.7	J	0.97	U	0.44	U
		14	3.2	J	1.6	U	0.69	J	0.94	U	0.43	U
		18.5	1.6	J	1.5	U	0.54	U	0.85	U	0.39	U
		24.9	0.37	U	1.5	U	0.56	U	0.88	U	0.4	U
		27.5	0.36	U	1.5	U	0.56	U	0.88	U	0.4	U
211-A-022	9/27/2012	33.5	0.36	U	1.5	U	0.55	U	0.87	U	0.4	U
211-A-022		35.1	8.5	J	6.7	J	0.85	J	0.83	U	0.38	U
		44	10		12		1	J	0.86	U	0.39	U
		49.5	6.7	J	5	J	0.68	U	1.1	U	0.49	U
		54.5	13		17		0.79	J	1.1	U	0.52	U
		56	88		1.8	J	1	J	0.89	U	0.41	U
		62	27		5.3	J	1.2	J	1	U	0.46	U
		Average	12		4.1		0.6		***		***	
		1	0.4	U	1.7	U	0.62	U	0.97	U	0.44	U
		7	0.37	U	1.5	U	0.57	U	0.89	U	0.41	U
		14.9	0.36	U	1.5	U	0.56	U	0.88	U	0.4	U
		18	0.36	U	1.5	U	0.55	U	0.87	U	0.4	U
		20.1	0.33	U	1.6	J	0.51	U	0.81	U	0.37	U
		(20.1)DUP	0.36	U	7.2	J	0.56	U	0.88	U	0.4	U
	9/11/2012	25.5	0.33	U	3.9	J	0.5	U	0.78	U	0.36	U
211-A-023	9/11/2012	34.9	0.37	U	1.5	U	0.57	U	0.89	U	0.4	U
		36.5	0.43	U	1.8	U	0.66	U	1	U	0.47	U
		43	0.39	U	7.9	J	0.6	U	0.94	U	0.43	U
		49	1.4	J	9.9		0.55	U	0.86	U	0.39	U
		53	66		8.6	J	0.87	J	0.97	U	0.45	U
		55.1	130		6.9	J	1.5	J	0.94	U	0.43	U
		62	73		11		1	J	1	U	0.46	U
		Average	19		4.4		0.5		***		***	

Station	Date Collected	Sample Depth [ft bls]	TCE [µg/kậ		1,1-DC [µg/kg		<i>cis</i> -1,2 DCE [µg/kg		trans-1, DCE [µg/kg		VC [µg/k	g]
			75		137		619		5290		570	
		1	0.37	U	1.5	U	0.56	U	0.88	U	0.4	U
		9	0.42	U	1.7	U	0.64	U	1	U	0.46	U
		14	0.4	U	1.6	U	0.61	U	0.96	U	0.44	U
		19	2.2	J	1.6	U	0.61	U	0.95	U	0.43	U
		24	0.34	U	1.4	U	0.52	U	0.81	U	0.37	U
		26	1.8	J	1.2	U	0.46	U	0.71	U	0.33	U
211-A-024	9/10/2012	33	0.36	U	1.5	U	0.55	U	0.87	U	0.4	U
211-A-024		39	0.86	J	1.8	U	0.68	U	1.1	U	0.49	U
		44	1.3	J	1.5	U	0.57	U	0.9	U	0.41	U
		49	3.4	J	1.5	U	0.56	U	0.88	U	0.4	U
		52.5	76		1.5	U	0.73	J	0.86	U	0.39	U
		56	9.2	J	1.5	U	0.56	U	0.87	U	0.4	U
		64.5	25		1.8	U	0.91	J	1.1	U	0.49	U
		Average	9		***		0.4		***		***	
		3	71		1.7	U	13		0.97	U	0.45	U
		6.5	92		2.1	U	28		1.2	U	0.55	U
		11	80		1.6	U	23		0.94	U	0.43	U
		(15.5)DUP	33		1.7	U	9	J	0.97	U	0.44	U
		15.5	80		1.8	U	20		1.1	U	0.48	U
		22.5	54		1.5	U	14		0.88	U	0.4	U
	9/10/2012	25.5	45		1.4	U	1.2	J	0.82	U	0.38	U
211-A-025	9/10/2012	32.5	63		1.6	U	1.4	J	0.95	U	0.44	U
		39.5	420		23	U	10	U	7.9	U	27	U
		44.5	1,400		23	U	44	J	7.7	U	26	U
		49.9	540		27	U	24	J	9.1	U	31	U
		50.1	27		1.5	U	0.9	J	0.88	U	0.4	U
		56.5	7	J	1.9	U	0.72	U	1.1	U	0.52	U
		64	68		1.7	U	0.65	U	1	U	0.47	U
		Average	213		***		13		***		***	

Station	Date Collected	Sample Depth [ft bls]	TCI [µg/k		1,1-DC [µg/kg		cis-1,2 DCE [µg/kg		trans-1, DCE [µg/kg		VC [µg/kş	g]
			75		137		619		5290		570	
		4	0.43	U	1.8	U	0.66	U	1	U	0.47	U
		9	0.39	U	1.6	U	0.6	U	0.94	U	0.43	U
		14	0.41	U	1.7	U	0.62	U	0.98	U	0.45	U
		18.5	0.34	U	1.4	U	0.52	U	0.82	U	0.37	U
		24.9	0.35	U	1.5	U	0.55	U	0.85	U	0.39	U
		29	0.36	U	1.5	U	0.55	U	0.86	U	0.4	U
211-A-026	9/7/2012	30.5	0.41	J	1.4	U	0.51	U	0.8	U	0.37	U
211-A-020		36	12		15		2.3	J	0.99	U	0.45	U
		44	12		14		4.1	J	0.88	U	0.84	J
		47	14		20		3.9	J	0.88	U	1	J
		51	7.2	J	6.6	J	2.2	J	0.96	U	0.44	U
		55.5	14		1.6	U	0.65	J	0.92	U	0.42	U
		61.5	1.2	J	1.6	U	0.59	U	0.92	U	0.42	U
		Average	4.8		4.8		1.2		***		0.3	
	9/11/2012	2	0.43	U	1.8	U	0.66	U	1	U	0.47	U
	9/11/2012	8.5	0.53	U	2.2	U	0.81	U	1.3	U	0.58	U
		14	0.4	U	1.7	U	0.62	U	0.97	U	0.44	U
		(14)DUP	0.42	U	1.7	U	0.64	U	1	U	0.46	U
		16.5	0.35	U	1.5	U	0.55	U	0.85	U	0.39	U
		21	0.39	U	1.6	U	0.6	U	0.94	U	0.43	U
		28	0.35	U	1.4	U	0.54	U	0.84	U	0.39	U
211-A-027	9/18/2012	31.5	0.46	J	1.7	J	0.51	U	0.8	U	0.36	U
	9/10/2012	36.5	3.4	J	1.6	U	0.59	U	0.92	U	0.42	U
		44.5	47		1.4	U	0.53	U	0.83	U	0.38	U
		45.5	<b>620</b>		20	U	8.7	U	6.8	U	23	U
		51	51		1.7	U	0.63	U	0.99	U	0.45	U
		59	29		1.7	U	0.67	J	1	U	0.46	U
		66.5	17		1.9	J	0.86	J	1.1	U	0.48	U
		Average	55		1.6		0.7		***		***	

Station	Date Collected	Sample Depth [ft bls]	TCI [µg/k		1,1-DC [µg/kg		cis-1,2 DCE [µg/kg		trans-1 DCE [µg/kg		VC [µg/kş	
			75		137		619		5290		570	
		4	0.38	U	1.6	U	0.58	U	0.91	U	0.42	U
		9	0.43	U	1.8	U	0.66	U	1	U	0.48	U
		14	0.41	U	1.7	U	0.63	U	0.99	U	0.45	U
		19	0.76	J	55		0.57	U	0.89	U	0.41	U
		22.5	0.44	U	1.8	J	0.67	U	1.1	U	0.48	U
		26	210		<b>290</b>		0.92	U	1.4	U	0.66	U
211-A-028	9/24/2012	34	220	J	55	J	11	U	8.9	U	30	U
211-A-026		38.5	3,700		4,200		33	J	9.1	U	31	U
		42.5	2,800		3,800		28	J	7.8	U	27	U
		48	1,600		1,800		33	J	8.1	U	27	U
		50.5	1,700		1,400		38	J	8.3	U	28	U
		55.1	42		79		4.2	J	0.95	U	0.43	U
		61	180		66		16		1.3	U	0.58	U
		Average	804		904		12		***		***	
		4	0.4	U	1.7	U	0.62	U	0.97	U	0.44	U
		9	0.51	U	2.1	U	0.79	U	1.2	U	0.56	U
		14	0.4	U	1.7	U	0.62	U	0.98	U	0.45	U
		18	0.31	U	1.3	U	0.48	U	0.74	U	0.34	U
		24.9	23		18		0.54	U	0.85	U	0.39	U
		28.5	440		240		9	U	7	U	24	U
	9/25/2012	(32)DUP	110		77		2.5	J	1.4	U	0.65	U
211-A-029	9/23/2012	32	480		360		12	U	9.4	U	32	U
		38	2,600		2,900		62	J	9.2	U	31	U
		40.5	870		880		11	U	8.2	U	28	U
		48.5	270		350		11	U	8.6	U	29	U
		50.5	22		27		0.61	U	0.96	U	0.44	U
		55.1	4	J	4.4	J	0.86	J	1	U	0.46	U
		64	100		15		9.2	J	1.1	U	0.49	U
		Average	351		348		7.0		***		***	

Station	Date Collected	Sample Depth [ft bls]	TCI [µg/k	_	1,1-DC [µg/kg		cis-1,2 DCE [µg/kş		trans-1, DCE [µg/kg		VC [µg/kş	g]
			75		137		619		5290		570	
		9	0.39	U	1.6	U	0.61	U	0.95	U	0.43	U
		14	0.36	U	1.5	U	0.56	U	0.87	U	0.4	U
		19	0.36	U	30		0.56	U	0.87	U	0.4	U
		23.5	21	U	29	U	13	U	9.9	U	34	U
		29.9	0.51	U	2.1	U	0.78	U	1.2	U	0.56	U
	9/25/2012	32.5	97	J	61	J	11	U	8.9	U	30	U
211-A-030	9/23/2012	39	0.38	U	3.5	J	0.58	U	0.91	U	0.42	U
		40.1	0.38	U	1.6	U	0.59	U	0.92	U	0.42	U
		49	0.39	U	8.9	J	0.61	U	0.95	U	0.44	U
		54.5	4.8	J	2	J	0.76	J	0.91	U	0.41	U
		58	20		25		1.9	J	1	U	0.47	U
		61	12		15		1.5	J	0.93	U	0.42	U
		Average	12		14		1.5		***		***	
		0.1	0.46	U	1.9	U	0.71	U	1.1	U	0.51	U
		9	0.41	U	1.7	U	0.64	U	1	U	0.46	U
		(14)DUP	0.39	U	1.6	U	0.6	U	0.94	U	0.43	U
		14	0.35	U	1.4	U	0.53	U	0.83	U	0.38	U
		19	2.9	J	1.5	U	0.9	J	0.85	U	0.39	U
		23	1	J	1.6	U	0.61	U	0.95	U	0.44	U
	9/26/2012	28	7.8	J	1.5	U	0.57	U	0.9	U	0.41	U
211-A-031	9/20/2012	34.5	35		1.9	U	0.7	U	1.1	U	0.5	U
		35.5	310		22	U	9.5	U	7.4	U	25	U
		40.5	18	U	24	U	10	U	8.1	U	28	U
		49.5	42		1.6	U	0.64	J	0.93	U	0.43	U
		50.5	29		1.8	U	0.69	U	1.1	U	0.49	U
		56.5	5.8	J	1.6	U	0.62	J	0.96	U	0.44	U
		61.5	3.5	J	1.8	U	0.67	U	1	U	0.48	U
		Average	32		***		1.1		***		***	

Station	Date Collected	Sample Depth [ft bls]	TCI [µg/k	_	1,1-DC [µg/kg		<i>cis</i> -1,2 DCE [µg/kg	,	trans-1, DCE [µg/kg		VC [µg/kş	
			75		137		619		5290		570	
		1.3	0.38	U	1.6	U	0.59	U	0.93	U	0.42	U
		9	0.41	U	1.7	U	0.64	U	1	U	0.46	U
		14	0.37	U	1.5	U	0.58	U	0.9	U	0.41	U
		19	1.1	J	1.5	U	0.57	U	0.89	U	0.41	U
		24.9	4.7	J	1.8	U	2	J	1.1	U	0.49	U
	9/28/2012	26	6.6	J	1.5	U	1.7	J	0.9	U	0.41	U
211-A-032	9/20/2012	33	0.47	J	1.5	U	0.54	U	0.85	U	0.39	U
		38	33		1.8	U	0.68	U	1.1	U	0.48	U
		42.5	29		1.5	U	0.58	U	0.9	U	0.41	U
		49	3.3	J	1.5	U	0.57	U	0.9	U	0.41	U
		54.9	0.42	U	1.7	U	0.64	U	1	U	0.46	U
		58.5	0.34	U	1.4	U	0.52	U	0.81	U	0.37	U
		Average	6.6		***		0.6		***		***	
		4	0.42	U	1.7	U	0.64	U	1	U	0.46	U
		9	0.38	U	1.6	U	0.59	U	0.92	U	0.42	U
		14	0.37	U	1.5	U	0.58	U	0.9	U	0.41	U
		19	0.35	U	1.5	U	0.55	U	0.85	U	0.39	U
		21.5	0.33	U	1.4	U	0.51	U	0.8	U	0.37	U
		29.9	3.6	J	2.4	J	0.64	U	1	U	0.46	U
	10/1/2012	(34)DUP	12		1.9	J	0.84	J	0.8	U	0.36	U
211-A-033	10/1/2012	34	60		16		2.1	J	0.84	U	0.38	U
		36	1,100		1,100		46	J	8	U	27	U
		44.5	700		540		29	J	7.4	U	25	U
		49.5	300		240		9.3	U	7.3	U	25	U
		50.5	130	J	58	J	12	U	9.7	U	33	U
		56.5	0.48	J	1.7	U	0.64	U	1	U	0.46	U
		62	14		3.6	J	8.4	J	0.89	U	0.41	U
		Average	166		140		7.1		***		***	

Station	Date Collected	Sample Depth [ft bls]	TCI [µg/k		1,1-DC [µg/kg		cis-1,2 DCE [µg/kş	1	trans-1, DCE [µg/kg		VC [µg/k	
			75		137		619		5290		570	
		1.9	0.4	U	1.7	U	0.62	U	0.97	U	0.44	U
		8.6	0.39	U	1.6	U	0.61	U	0.95	U	0.44	U
		13.4	0.38	U	2.5	J	3.6	J	0.9	U	0.41	U
		18.5	1.6	J	33		12		0.87	U	0.4	U
		24	7.6	J	30		6.9	J	0.89	U	0.41	U
		27	2.1	J	1.7	J	0.53	U	0.84	U	0.38	U
	10/2/2012	30.5	35		27		0.57	U	0.89	U	0.4	U
211-A-035	10/2/2012	37	580		<b>590</b>		11	U	8.3	U	28	U
		(41.5)DUP	420		350		11	U	8.2	U	28	U
		41.5	400		400		10	U	8	U	27	U
		49	210	J	26	J	11	U	8.4	U	29	U
		51.5	680		360		10	U	8.2	U	28	U
		55.5	17		1.7	U	2	J	1	U	0.46	U
		66.5	25		9.3	J	4	J	0.98	U	0.45	U
		Average	170		131		4		***		***	
		0.1	0.41	U	1.7	U	0.64	U	1	U	0.46	U
		9	0.47	U	1.9	U	0.73	U	1.1	U	0.52	U
		14.7	0.42	U	1.7	U	0.64	U	1	U	0.46	U
		19	0.67	J	2.1	J	0.57	U	0.89	U	0.41	U
		22	280	J	31	U	13	U	10	U	35	U
		26.5	810		340		9.9	U	7.8	U	26	U
211 A 026	10/3/2012	31.5	1,400		1,600		8.6	U	6.7	U	23	U
211-A-036		35.5	2,800		3,700		51	J	8.2	U	28	U
		44.5	3,800		3,900		110	J	7.6	U	28	J
		47.5	4,800		3,300		77	J	8	U	27	U
		50.1	1,300		690		12	U	9.1	U	31	U
		55.5	3	J	1.5	U	0.57	U	0.89	U	0.41	U
		61	33		12		4.1	J	0.99	U	0.45	U
		Average	1,171		1,043		20		***		9	

Station	Date Collected	Sample Depth [ft bls]	TCI [µg/k		1,1-DC [µg/kg		cis-1,2 DCE [µg/kg		trans-1, DCE [µg/kg		VC [µg/k	
			75		137		619		5290		570	
		4	0.4	U	1.6	U	0.61	U	0.96	U	0.44	U
		9	0.39	U	1.6	U	0.61	U	0.95	U	0.43	U
		14	0.42	U	1.7	U	0.65	U	1	U	0.47	U
		16	0.38	U	1.6	U	0.58	U	0.91	U	0.41	U
		24	0.47	U	1.9	U	0.72	U	1.1	U	0.51	U
		(24)Dup	0.53	U	2.2	U	0.81	U	1.3	U	0.58	U
	2/25/2013	25.5	0.36	U	1.5	U	0.55	U	0.87	U	0.4	U
211-A-037	2/25/2015	34	0.51	U	2.1	U	0.78	U	1.2	U	0.56	U
		35.5	0.54	U	2.2	U	0.84	U	1.3	U	0.6	U
		44	0.37	U	2.3	J	0.57	U	0.89	U	0.41	U
		49.5	0.37	U	1.5	U	0.57	U	0.89	U	0.41	U
		54.5	2.2	J	1.7	U	0.65	U	1	U	0.47	U
		56.5	1.4	J	2.5	U	0.93	U	1.5	U	0.67	U
		62	1.2	J	1.8	U	0.67	U	1	U	0.48	U
		Average	0.5		***		***		***		***	
		3	0.37	U	1.5	U	0.58	U	0.9	U	0.41	U
		7.5	20	U	27	U	12	U	9.2	U	31	U
		12	23	U	32	U	14	U	11	U	36	U
		15.5	0.41	U	1.7	U	0.64	U	1	U	0.46	U
		20.5	26		1.6	U	6.8	J	0.96	U	2.2	J
		28.5	0.36	U	1.5	U	0.55	U	0.86	U	0.39	U
211 4 029	2/25/2013	32.5	0.37	U	1.5	U	0.57	U	0.89	U	0.41	U
211-A-038		39	30		1.6	U	7.5	J	0.92	U	0.42	U
		43	61		2	J	10		0.91	U	0.42	U
		49.9	0.98	J	1.6	U	0.6	U	0.93	U	0.43	U
		54.5	6.6	J	1.5	U	1.2	J	0.89	U	0.4	U
		56	20		3.6	J	6.6	J	0.97	U	0.44	U
		62	11		1.8	J	4	J	0.89	U	0.41	U
		Average	14		3.3		3.9		***		2.9	

Station	Date Collected	Sample Depth [ft bls]	TCI [µg/k		1,1-DC [µg/kg		<i>cis</i> -1,2 DCE [µg/kg		trans-1 DCE [µg/kg		VC [µg/k	
			75		137		619		5290		570	
		9	0.41	U	1.7	U	0.62	U	0.98	U	0.45	U
		14	0.44	U	1.8	U	0.67	U	1.1	U	0.48	U
		(14)Dup	0.46	U	1.9	U	0.7	U	1.1	U	0.5	U
		19	0.36	U	1.5	U	0.55	U	0.86	U	0.4	U
		23	0.39	U	1.6	U	0.59	U	0.93	U	0.43	U
		27.5	0.44	U	1.8	U	0.68	U	1.1	U	0.49	U
211-A-039	2/26/2013	33	0.34	U	1.4	U	0.55	J	0.83	U	0.38	U
211-A-039		37	0.41	U	3.4	J	1.5	J	1	U	0.46	U
		42	0.38	U	15		1.8	J	0.92	U	0.42	U
		49.5	0.34	U	12		0.53	U	0.83	U	0.38	U
		51.5	0.39	U	57		0.66	J	0.93	U	0.43	U
		56	1	J	1.5	U	0.57	U	0.89	U	0.41	U
		64	4.5	J	2.3	U	0.86	U	1.3	U	0.61	U
		Average	0.6		7.3		0.57		***		***	
		3	0.4	U	1.6	U	0.61	U	0.96	U	0.44	U
		9	0.4	U	1.7	U	0.62	U	0.97	U	0.44	U
		14	0.38	U	1.6	U	0.59	U	0.92	U	0.42	U
		16.5	0.42	U	1.7	U	0.64	U	1	U	0.46	U
		22	0.53	U	2.2	U	0.82	U	1.3	U	0.59	U
		26	0.34	U	1.4	U	0.52	U	0.81	U	0.37	U
	2/26/2012	34.5	0.34	U	1.4	U	0.52	U	0.81	U	0.37	U
211-A-040	2/26/2013	36	0.41	U	1.7	U	0.63	U	0.99	U	0.45	U
		(36)Dup	0.35	U	1.5	U	0.54	U	0.85	U	0.39	U
		41.5	0.4	U	1.7	U	0.62	U	0.97	U	0.44	U
		48.5	0.37	U	2.4	J	0.56	U	0.88	U	0.4	U
		51.5	0.37	U	1.5	U	0.57	U	0.89	U	0.41	U
		56	0.36	U	21		0.55	U	0.86	U	0.39	U
		61	0.38	U	3.2	J	0.58	U	0.91	U	0.42	U
		Average	***		2.5		***		***		***	

Station	Date Collected	Sample Depth [ft bls]	TCI [µg/k		1,1-DC [µg/kg		cis-1,2 DCE [µg/kg		trans-1, DCE [µg/kg		VC [µg/kş	
			75		137		619		5290		570	
		4	0.39	U	1.6	U	0.61	U	0.95	U	0.44	U
		9	0.41	U	1.7	U	0.63	U	0.98	U	0.45	U
		14.5	0.41	U	1.7	U	0.63	U	0.99	U	0.45	U
		18.5	0.37	U	8.8	J	0.57	U	0.89	U	0.41	U
		(18.5)Dup	0.35	U	8.7	J	0.54	U	0.84	U	0.39	U
		24	0.53	U	2.2	U	0.82	U	1.3	U	0.59	U
	2/27/2012	27	0.34	U	1.4	U	0.53	U	0.83	U	0.38	U
211-A-041	2/27/2013	34.5	1.7	J	1.6	J	2.2	J	0.86	U	1.1	J
		39	71		120		14		1	U	6.5	J
		41	76		140		11		0.86	U	6.4	J
		49	33		170		8.5	J	0.84	U	0.72	J
		50.5	18		26		4.1	J	0.98	U	0.45	U
		55.1	27		2.2	J	2.8	J	1	U	0.46	U
		63	68		21		15		0.87	U	0.4	U
		Average	21		36		4.3		***		1.2	
		9	0.41	U	1.7	U	2.8	J	0.99	U	0.45	U
		14.5	0.39	U	1.6	U	0.6	U	0.94	U	0.43	U
		17	0.37	U	1.5	U	0.57	U	0.89	U	0.41	U
		22.5	0.33	U	1.4	U	0.52	U	0.81	U	0.37	U
		27.5	0.34	U	1.4	U	0.52	U	0.81	U	0.37	U
	2/27/2012	31	0.38	U	1.6	U	0.59	U	0.93	U	0.42	U
211-A-042	2/27/2013	39	61		68		9.6	J	0.95	U	2	J
		42	120		94		16		0.98	U	2.4	J
		48	82		40		9	J	0.92	U	0.6	J
		54.9	40		21		5.7	J	0.88	U	0.4	U
		57	0.38	U	1.6	U	0.58	U	0.91	U	0.41	U
		62.5	27		6.4	J	5.2	J	0.98	U	0.45	U
		Average	28		20		4.2		***		0.6	

Station	Date Collected	Sample Depth [ft bls]	TCI [µg/k		1,1-DC [µg/kg		<i>cis</i> -1,2 DCE [µg/kg		trans-1, DCE [µg/kg		VC [µg/kş	g]
			75		137		619		5290		570	
		3.5	0.34	U	1.4	U	0.52	U	0.81	U	0.37	U
		9	0.42	U	1.7	U	0.97	J	1	U	0.46	U
		14	0.39	U	1.6	U	0.6	U	0.93	U	0.43	U
		(14)Dup	0.4	U	1.6	U	0.61	U	0.96	U	0.44	U
		17.5	0.35	U	1.4	U	0.54	U	0.84	U	0.38	U
		22.5	0.32	U	1.3	U	1.2	J	0.78	U	0.36	U
	3/4/2013	29	2.7	J	1.7	U	8.3	J	0.98	U	0.45	U
211-A-043	3/4/2013	32.5	1.8	J	1.5	U	5.2	J	0.9	U	0.41	U
		36	9.2		2	J	28		0.86	U	0.39	U
		44.9	24		13		32		0.94	U	0.43	U
		49	39		6.7	J	34		0.81	U	0.37	U
		53.5	30		1.7	U	46		0.97	U	0.44	U
		55.1	42		5.1	J	48		0.84	U	0.39	U
		62	0.39	U	1.6	U	0.6	U	0.94	U	0.43	U
		Average	11		2.5		15		***		***	
		4	5.5	J	1.7	U	100		1	U	78	
		(4)Dup	4.2	J	1.7	U	49		1	U	62	
		6	20	U	28	U	630		9.4	U	32	U
		10.5	18	U	25	U	520		8.5	U	29	U
		18.5	0.46	U	1.9	U	1.2	J	1.1	U	0.5	U
		23	5	J	1.3	U	31		0.76	U	0.96	J
	3/6/2013	26	11		1.9	U	99		1.1	U	9.2	J
211-A-044	5/0/2015	33.5	8.5	J	1.7	U	64		1	U	3.2	J
		36.5	18		1.8	J	98		0.82	U	4.8	J
		44.5	42		2.6	J	130		0.88	U	9.9	
		49	76		9.6		110		0.85	U	0.77	J
		54.5	2.7	J	1.5	U	4.8	J	0.86	U	0.39	U
		55.5	2.5	J	1.9	U	1.7	J	1.1	U	0.52	U
		62.5	0.47	U	1.9	U	0.72	U	1.1	U	0.51	U
		Average	14		3.4		131		***		14	

#### Notes:

- Groundwater Protection Remediation Goals from Remedial Design Work Plan for Solid Waste Management Units 1, 211-A, and 211-B Volatile Organic Compound Sources for the Southwest Groundwater Plume at the Paducah Gaseous Diffusion Plant, Paducah, Kentucky, (DOE 2012a).
- 2. J—Indicates an estimated value.
- $3. \qquad U\mbox{--Compound analyzed for but not detected at or below the lowest concentration reported.}$
- 4. DUP-Indicated that a duplicate sample was taken for the interval given in parentheses.
- 5. Sample depth represents the discrete depth at which an EnCore® sample was taken.
- 6. For "U" qualified samples a value of one half the concentration reported was used in calculating the average borehole concentration.
- 7. \*\*\*-Indicates average concentration not calculated as all boring samples were "U" qualified for specific VOC.
- 8. Yellow shading and bold text indicate an exceedance of Groundwater Protection Remediation Goals.
- 9. Soil boring 211-A-007 was not collected.
- 10. Soil boring 211-A-034 was collected and archived. Boring was not logged or screened for VOC impacts.

**APPENDIX F** 

HYDRAULIC CONDUCTIVITY AND GRAIN SIZE TESTS

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Grain Size Analysis

# ASTM D422

Advanced Terra Testing

#### MECHANICAL ANALYSIS - SIEVE TEST DATA ASTM D 422

CLIENT LATA Kent	lucky	JOB NO. 2855-05	
BORING NO. DEPTH SAMPLE NO. SOIL DESCR. LOCATION	211-A-006 12-15.5' 211A006GRNSZ1 ERI12-SW-SWMU211A SW Plume RDSI Geotechnical	SAMPLED DATE TESTED WASH SIEVE DRY SIEVE	09/26/12 KD 10/10/12 JS Yes No
MOISTURE DATA		WASH SIEVE ANALY	SIS
HYGROSCOPIC	Yes	Wt. Total Sample	
NATURAL	No	Wet (g) Weight of + #10	1120.50
		Before Washing (g) Weight of + #10	0.92
Wt. Wet Soil & Pan (g)	40.14	After Washing (g)	0.87
Wt. Dry Soil & Pan (g)	39.59	Weight of - #10	
Wt. Lost Moisture (g)	0.55	Wet (g)	1119.58
Wt. of Pan Only (g)	3.07	Weight of - #10	
Wt. of Dry Soil (g)	36.52	Dry (g)	1103.02
Moisture Content %	1.5	Wt. Total Sample Dry (g)	1103.89
Wt. Hydrom. Sample W	/et (a) 62.50	Calc. Wt. "W" (g)	61.62
Wt. Hydrom. Sample D		Calc. Mass + #10	0.05
÷			

Sieve	Pan	Indiv.	Indiv.	Cum.	Cum.	%
Number	Weight	Wt. + Pan	Wt.	Wt.	%	Finer
(Size)	(g)	(g)	Retain.	Retain.	Retain.	By Wt.
3"	0.00	0.00	0.00	0.00	0.0	100.0
1 1/2"	0.00	0.00	0.00	0.00	0.0	100.0
3/4"	0.00	0.00	0.00	0.00	0.0	100.0
3/8"	0.00	0.00	0.00	0.00	0.0	100.0
#4	0.00	0.71	0.71	0.71	0.1	99.9
#10	0.00	0.16	0.16	0.87	0.1	99.9
#20	3.03	3.06	0.03	0.03	0.1	99.9
#40	3.11	3.19	0.08	0.10	0.2	99.8
#60	3.07	3.42	0.35	0.45	0.8	99.2
#100	3.01	4.84	1.83	2.28	3.8	96.2
#200	3.01	4.94	1.93	4.21	6.9	93.1

Data entered by: DAW Data checked by: <u>AU</u> FileName: LKH0NSZ1



#### HYDROMETER ANALYSIS - SEDIMENTATION DATA ASTM D 422

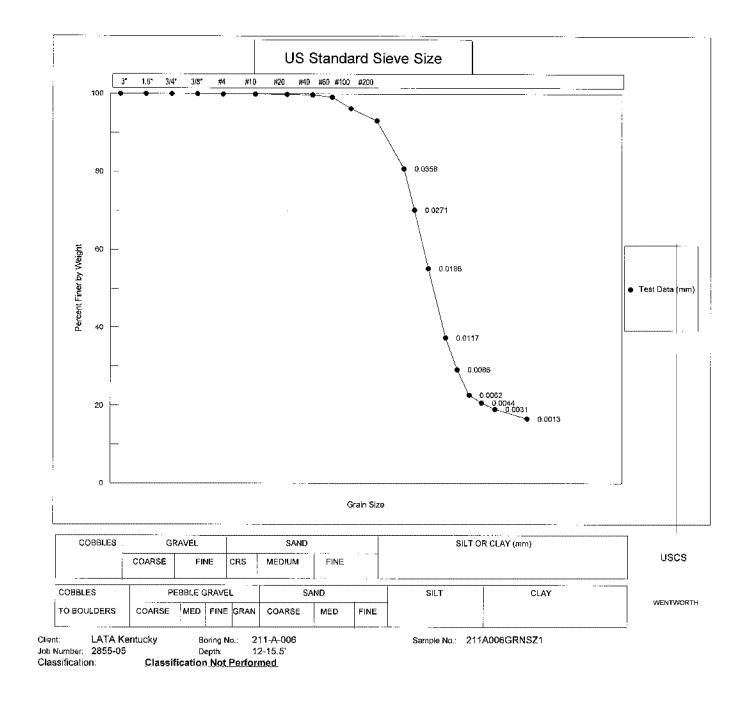
CLIENT LATA Ker	ntucky	JOB NO. 2855-05	
BORING NO. DEPTH SAMPLE NO. SOIL DESCR. LOCATION	211-A-006 12-15.5' 211A006GRNSZ1 ERI12-SW-SWMU211A SW Plume RDSI Geotechnical	SAMPLED DATE TESTED WASH SIEVE DRY SIEVE	09/26/12 KD 10/10/12 JS Yes No
Hydrometer # Sp. Gr. of Soil Value of "alpha" Deflocculant Defloc. Corr'n Meniscus Corr'n	ASTM 152 H 2.65 1.00 Sodium Hexametaphosphate 5.0 0.0	Temp., Deg. C Temp. Coef. K Wt. Dry Sample "W' % of Total Sample	22.5 0.01325 61.622 100.0

⊤ Elapsed Time (min)	Hydrometer Original	Reading Corrected "R"	100Ra/W	% Total Sample	Effective Depth L	Grain Diameter (mm)
0.0						
0.5						
1.0	54.75	49.75	80.7	80.7	7.31	0.0358
2.0	48.25	43.25	70.2	70.2	8.38	0.0271
5.0	39.00	34,00	55.2	55.2	9.89	0.0186
15.0	28.00	23.00	37.3	37.3	11.70	0.0117
30.0	23.00	18.00	29.2	29.2	12.52	0.0086
60.0	19.00	14.00	22.7	22.7	13.17	0.0062
120.0	17.75	12.75	20.7	20.7	13.38	0.0044
250.0	16.75	11.75	19.1	19.1	13.54	0.0031
1440.0	15.25	10.25	16.6	16.6	13.79	0.0013

Grain Diameter =  $K^{(SQRT(L/T))}$ 

Data entered by: DAW Data checked by: DAW FileName: LKH0NSZ1





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F-6

#### MECHANICAL ANALYSIS - SIEVE TEST DATA ASTM D 422

CLIENT LATA Kent	ucky	JOB NO. 2855-05	
BORING NO. DEPTH SAMPLE NO. SOIL DESCR. LOCATION	211-A-006 211A006GRNSZ2 ERI12-SW-SWMU211A SW Plume RDSI Geotechnical	SAMPLED DATE TESTED WASH SIEVE DRY SIEVE	09/26/12 KD 10/10/12 JS Yes No
MOISTURE DATA		WASH SIEVE ANALYS	SIS
HYGROSCOPIC	Yes	Wt. Total Sample	
NATURAL	Νο	Wet (g) Weight of + #10 Before Washing (g) Weight of + #10	929.90 494.76
Wt. Wet Soil & Pan (g) Wt. Dry Soil & Pan (g)	34.10 33.65	After Washing (g) Weight of - #10	470.13
Wt. Lost Moisture (g) Wt. of Pan Only (g)	0.45	Wet (g) Weight of - #10	435.14
Wt. of Dry Soil (g) Moisture Content %	31.23 1.4	Dry (g) Wt. Total Sample	453.24
		Dry (g)	923.37
Wt. Hydrom. Sample W Wt. Hydrom. Sample D		Calc. Wt. "W" (g) Calc. Mass + #10	173.72 88.45

Sieve Number (Size)	Pan Weight (g)	Indiv. Wt. + Pan (g)	Indiv. Wt. Retain.	Cum. Wt. Retain.	Cum. % Retain.	% Finer By Wt.
3"	0.00	0.00	0.00	0.00	0.0	400.0
-	0.00	0.00	0.00	0.00	0.0	100.0
1 1/2"	0.00	0.00	0.00	0.00	0.0	100.0
3/4"	0.00	42.14	42.14	42.14	4.6	95.4
3/8"	0.00	102.72	102.72	144.86	15.7	84.3
#4	0.00	174.75	174.75	319.61	34.6	65.4
#10	0.00	150.52	150.52	470.13	50.9	49.1
#20	3.05	18.15	15.10	15.10	59.6	40.4
#40	3.06	17.47	14.41	29.51	67.9	32.1
#60	3.05	15.15	12.10	41.62	74.9	25.1
#100	2.98	9.72	6.74	48.36	78.7	21.3
#200	3.08	6.90	3.82	52.17	80.9	19.1

Data entered by: DAW Data checked by: DAW FileName: LKH0NSZ2



#### HYDROMETER ANALYSIS - SEDIMENTATION DATA ASTM D 422

CLIENT	LATA Kent	ucky	JOB NO.	2855-05	
BORING NC DEPTH SAMPLE NC SOIL DESCI LOCATION	D.	211-A-006 211A006GRNSZ2 ERI12-SW-SWMU211A SW Plume RDSI Geotechnical	SAMPLED DATE TES WASH SIE DRY SIEVI	VE	09/26/12 KD 10/10/12 JS Yes No
Hydrometer Sp. Gr. of So Value of "alp Deflocculant Defloc. Corr'	oil oha" t	ASTM 152 H 2.65 1.00 Sodium Hexametaphosphate 5.0	Temp., Deg Temp. Coe Wt. Dry Sa % of Total :	f. K mple "W"	22.5 0.01325 173.718 100.0

T Elapsed Time (min)	Hydrometer Original	Reading Corrected "R"	100Ra/W	% Total Sample	Effective Depth L	Grain Diameter (mm)
0.0					. <b></b>	
0.5						
1.0	36.75	31.75	18.3	18.3	10.26	0.0424
2.0	36.00	31.00	17.8	17.8	10.39	0.0302
5.0	33.00	28.00	16.1	16.1	10.88	0.0195
15.0	30.25	25.25	14.5	14.5	11.33	0.0115
30.0	29.00	24.00	13.8	13.8	11.53	0.0082
60.0	28.00	23.00	13.2	13.2	11.70	0.0058
120.0	27.25	22.25	12.8	12.8	11.82	0.0042
250.0	27.00	22.00	12.7	12.7	11.86	0.0029
1440.0	26.00	21.00	12.1	12.1	12.03	0.0012

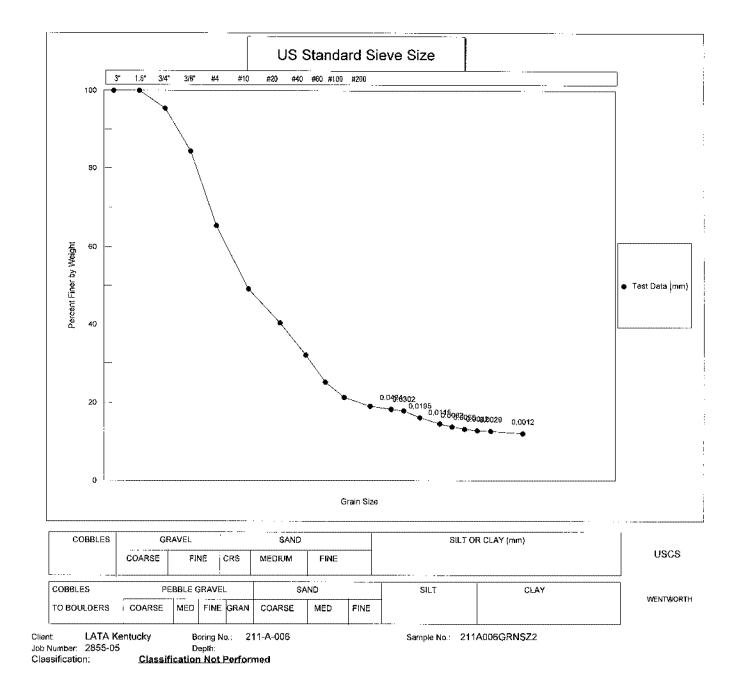
0.0

Grain Diameter = K\*(SQRT(L/T))

Meniscus Corr'n

Data entered by: DAW Data checked by: <u>Sub</u> FileName: LKH0NSZ2





#### MECHANICAL ANALYSIS - SIEVE TEST DATA ASTM D 422

CLIENT LATA Kent	ucky	JOB NO. 2855-05	
BORING NO. DEPTH SAMPLE NO. SOIL DESCR. LOCATION	211-A-006 211A006GRNSZ3 ERI12-SW-SWMU211A SW Plume RDSI Geotechnical	SAMPLED DATE TESTED WASH SIEVE DRY SIEVE	09/26/12 KD 10/10/12 JS Yes No
MOISTURE DATA		WASH SIEVE ANALY	SIS
HYGROSCOPIC	Yes	Wt. Total Sample	
NATURAL	No	Wet (g) Weight of + #10	1241.91
		Before Washing (g) Weight of + #10	19.21
Wt. Wet Soil & Pan (g) Wt. Dry Soil & Pan (g)	41.26 40.84	After Washing (g) Weight of - #10	18.33
Wt. Lost Moisture (g)	0.42	Wet (g) Weight of - #10	1222.70
Wt. of Pan Only (g) Wt. of Dry Soil (g) Moisture Content %	37.84 1.1	Dry (g) Wt. Total Sample	1210.15
		Dry (g)	1228.48
Wt. Hydrom. Sample W Wt. Hydrom. Sample D		Calc. Wt. "W" (g) Calc. Mass + #10	62.93 0.94

Sieve Number (Size)	Pan Weight (g)	Indiv. Wt. + Pan (g)	Indiv. Wt. Retain.	Cum. Wt. Retain.	Cum. % Retain.	% Finer By Wt.
3"	0.00	0.00	0.00	0.00	0.0	100.0
1 1/2"	0.00	0.00	0.00	0.00	0.0	100.0
3/4"	0.00	8.17	8.17	8.17	0.7	99.3
3/8"	0.00	4.84	4.84	13.01	1.1	98.9
#4	0.00	3.19	3.19	16.20	1.3	98.7
#10	0.00	2.13	2.13	18.33	1.5	98.5
#20	3.07	3.28	0.21	0.21	1.8	98.2
#40	3.32	4.38	1.06	1.26	3.5	96.5
#60	3.03	8.93	5.90	7.16	12.9	87.1
#100	3.08	13.97	10.89	18.06	30.2	69.8
#200	2.99	12.62	9.62	27.68	45.5	54.5

Data entered by: DAW Data checked by: DAW FileName: LKH0NSZ3



#### HYDROMETER ANALYSIS - SEDIMENTATION DATA ASTM D 422

CLIENT LA	ATA Kentucky	JOB NO. 2855-05	
BORING NO. DEPTH SAMPLE NO. SOIL DESCR. LOCATION	211-A-006 211A006GRNSZ3 ERI12-SW-SWMU211A SW Plume RDSI Geotechnical	SAMPLED DATE TESTED WASH SIEVE DRY SIEVE	09/26/12 KD 10/10/12 JS Yes No
Hydrometer # Sp. Gr. of Soil Value of "alpha Deflocculant	ASTM 152 H 2.65 a" 1.00 Sodium Hexametaphosphate	Temp., Deg. C Temp. Coef. K Wt. Dry Sample "W" % of Total Sample	22.6 0.01323 62.927 100.0

т						
Elapsed	Hydrometer	Reading		%	Effective	Grain
Time	Original	Corrected		Total	Depth	Diameter
(min)		"R"	100Ra/W	Sample	L	(mm)
0.0						-
0.5						
1.0	34.75	29.75	47.3	47.3	10.59	0.0431
2.0	33.00	28.00	44.5	44.5	10.88	0.0309
5.0	31.75	26.75	42.5	42.5	11.08	0.0197
15.0	28.25	23.25	36.9	36.9	11.66	0.0117
30.0	26.25	21.25	33.8	33.8	11.99	0.0084
60.0	24.50	19.50	31.0	31.0	12.27	0.0060
120.0	23.00	18.00	28.6	28.6	12.52	0.0043
250.0	21.50	16.50	26.2	26.2	12.76	0.0030
1440.0	20.00	15.00	23.8	23.8	13.01	0.0013

5.0

0.0

Grain Diameter =  $K^{(SQRT(L/T))}$ 

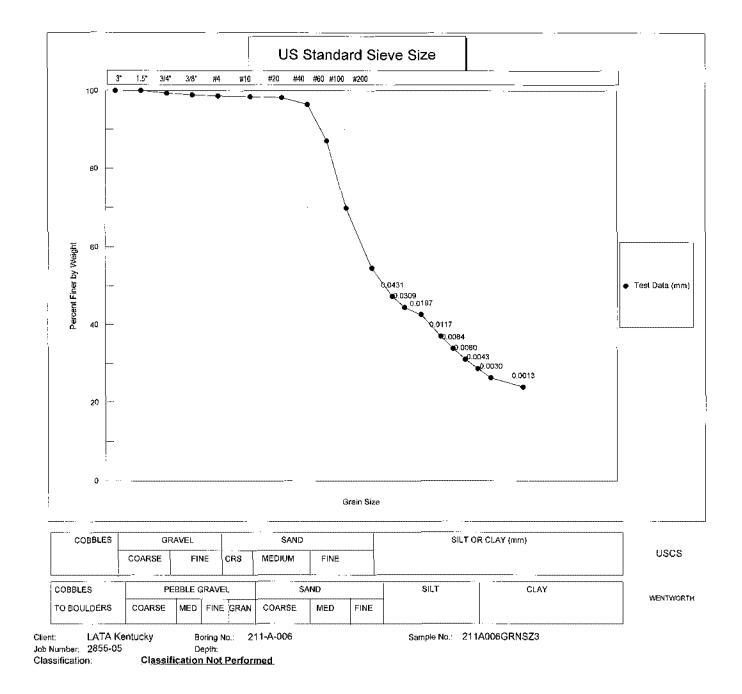
Defloc. Corr'n

Meniscus Corr'n

Data entered by: Data checked by: FileName: LKH0NSZ3 DAW

Date: 10/12/2012 Date: 10/12/12





F-12

CLIENT LATA Kent	ucky	JOB NO. 2855-2	
BORING NO. DEPTH SAMPLE NO. SOIL DESCR. LOCATION	211-A-002 9-13' 211A002GRNSZ1 ERI12-SW-SWMU211A SW Plume RDSI Geotechnical	SAMPLED DATE TESTED WASH SIEVE DRY SIEVE	8/30/12 KD 9/13/12 JS Yes No
MOISTURE DATA		WASH SIEVE ANALY	SIS
HYGROSCOPIC	Yes	Wt. Total Sample	1010 40
NATURAL	No	Wet (g) Weight of + #10	1213.18
		Before Washing (g) Weight of + #10	4.38
Wt. Wet Soil & Pan (g) Wt. Dry Soil & Pan (g)	38.74 37.31	After Washing (g) Weight of - #10	3.66
Wt. Lost Moisture (g) Wt. of Pan Only (g)	1.43 3.04	Wet (g) Weight of - #10	1208.80
Wt. of Dry Soil (g) Moisture Content %	34.27 4.2	Dry (g) Wt. Total Sample	1161.07
moisture content 76	4.2	Dry (g)	1164.73
Wt. Hydrom. Sample W Wt. Hydrom. Sample Dr		Calc. Wt. "W' (g) Calc. Mass + #10	74.25 0.23

Sieve Number (Size)	Pan Weight (g)	Indiv. Wt. + Pan (g)	Indiv. Wt. Retain.	Cum. Wt. Retain.	Cum. % Retain.	% Finer By Wt.
3"	0.00	0.00	0.00	0.00	0.0	100.0
1 1/2"	0.00	0.00	0.00	0.00	0.0	100.0
3/4"	0.00	0.00	0.00	0.00	0.0	100.0
3/8"	0.00	1.15	1.15	1.15	0.1	99.9
#4	0.00	0.83	0.83	1.98	0.2	99.8
#10	0.00	1.68	1.68	3.66	0.3	99.7
#20	2.99	2.00	0.09	0.09	0.4	99.6
#20		3.08			0.4	
#40	2.99	3.32	0.33	0.42	0.9	99.1
#60	3.03	4.00	0.97	1.39	2.2	97.8
#100	3.12	4.66	1.54	2.93	4.3	95.7
#200	3.04	4.30	1.26	4.19	6.0	94.0

Data entered by: MLM Data checked by: <u>SML</u> FileName: LKHYNS21

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Date: 09/17/2012 Date: <u>9/17/12</u>



CLIENT LATA Ken	tucky	JOB NO. 2855-2	
BORING NO. DEPTH SAMPLE NO. SOIL DESCR. LOCATION	211-A-002 9-13' 211A002GRNSZ1 ERI12-SW-SWMU211A SW Plume RDSI Geotechnical	SAMPLED DATE TESTED WASH SIEVE DRY SIEVE	8/30/12 KD 9/13/12 JS Yes No
Hydrometer # Sp. Gr. of Soil Value of "alpha" Deflocculant Defloc. Corr'n Meniscus Corr'n	ASTM 152 H 2.65 1.00 Sodium Hexametaphosphate 4.5 0.0	Temp., Deg. C Temp. Coef. K Wt. Dry Sample "W" % of Total Sample	23.3 0.01312 74.253 100.0

T Elapsed Time (min)	Hydrometer Original	Reading Corrected "R"	100Ra/W	% Total Sample	Effective Depth L	Grain Diameter (mm)
0.0						
0.5				_	·	
1.0	42.50	38.00	51.2	51.2	9.32	0.0401
2.0	39.50	35.00	47.1	47.1	9.81	0.0291
5.0	34.50	30.00	40.4	40.4	10.63	0.0191
15.0	26.50	22.00	29.6	29.6	11.94	0.0117
30.0	22.00	17.50	23.6	23.6	12.68	0.0085
60.0	19.00	14.50	19.5	19.5	13.17	0.0061
120.0	17.50	13.00	17.5	17.5	13.42	0.0044
250.0	15.25	10.75	14.5	14.5	13.79	0.0031
1440.0	13.00	8.50	11.4	11.4	14.16	0.0013

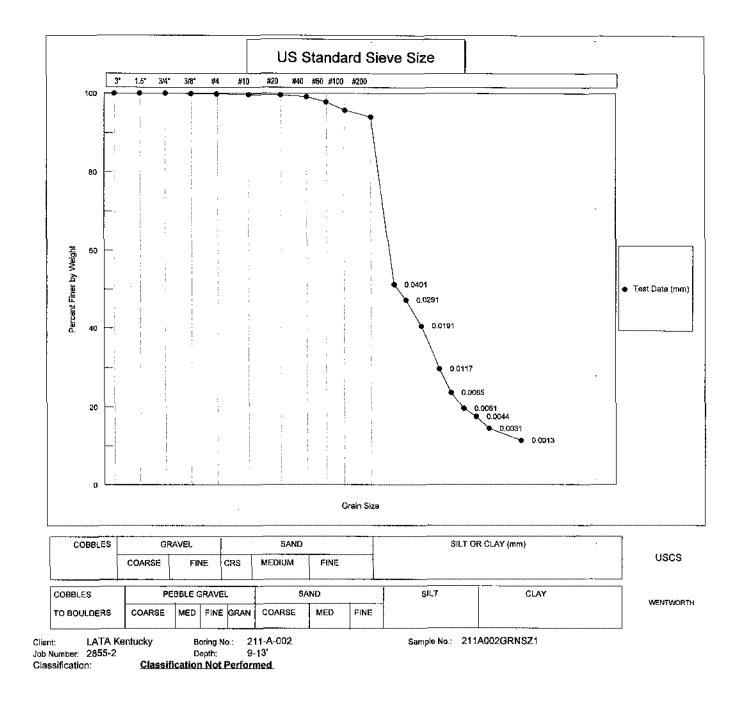
Grain Diameter =  $K^{(SQRT(L/T))}$ 

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Date: 09/17/2012 Date: <u>9/17/12</u>





Sec. 2

F-15

15

CLIENT LATA Ken	tucky	JOB NO. 2855-2	
BORING NO. DEPTH SAMPLE NO. SOIL DESCR. LOCATION	211-A-002 23-26' 211A002GRNSZ2 ERI12-SW-SWMU211A SW Plume RDSI Geotechnical	SAMPLED DATE TESTED WASH SIEVE DRY SIEVE	8/30/12 KD 9/13/12 JS Yes No
MOISTURE DATA		WASH SIEVE ANALY	SIS
HYGROSCOPIC	Yes	Wt. Total Sample Wet (g)	1087.63
NATURAL	No	Weight of + #10 Before Washing (g) Weight of + #10	562.03
Wt. Wet Soil & Pan (g) Wt. Dry Soil & Pan (g)		After Washing (g) Weight of - #10	502.46
Wt. Lost Moisture (g) Wt. of Pan Only (g)	0.48 3.15	َ Wet (g) Weight of - #10	525.60
Wt. of Dry Soil (g) Moisture Content %	34.85 1.4	Dry (g) Wt. Total Sample	577.22
		Dry (g)	1079.68
Wt. Hydrom. Sample V Wt. Hydrom. Sample D		Caic. Wt. "W" (g) Caic. Mass + #10	168.81 78.56

Sieve	Pan	Indiv.	Indiv.	Cum.	Cum.	%
Number	Weight	Wt. + Pan	Wt.	Wt.	%	Finer
(Size)	(g)	(g)	Retain.	Retain.	Retain.	By Wt.
3"	0.00	0.00	0.00	0.00	0.0	100.0
1 1/2"	0.00	0.00	0.00	0.00	0.0	100.0
3/4"	0.00	17.41	17.41	17,41	1.6	98.4
3/8"	0.00	121.64	121.64	139.05	12.9	87.1
#4	0,00	184.36	184.36	323.41	30.0	70.0
#10	0.00	179.05	179.05	502.46	46.5	53.5
#20	3.02	17.88	14.87	14.87	55.3	44.7
#40	3.11	16.68	13.56	28.43	63.4	36.6
#60	3.06	18.07	15.01	43.43	72.3	27.7
#100	2,99	14.19	11.20	54.64	78.9	21.1
#200	3.09	8.81	5.72	60.36	82.3	17.7

Data entered by: MLM Data checked by: MLM FileName: LKHYNS22

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Date: 09/17/2012 Date: 9/17/20



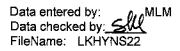
CLIENT L	ATA Kentucky	JOB NO. 2855-2	
BORING NO. DEPTH SAMPLE NO. SOIL DESCR LOCATION	23-26' 211A002GRNSZ2	SAMPLED DATE TESTED WASH SIEVE DRY SIEVE	8/30/12 KD 9/13/12 JS Yes No
Hydrometer # Sp. Gr. of Soi Value of "alph Deflocculant Defloc. Corr'n Meniscus Cor	l 2.65 na" 1.00 Sodium Hexametaphosphate a 4.5	Temp., Deg. C Temp. Coef. K Wt. Dry Sample "W" % of Total Sample	23.3 0.01312 168.807 100.0

T Elapsed Time (min)	Hydrometer Original	Reading Corrected "R"	100Ra/W	% Totai Sample	Effective Depth L	Grain Diameter (mm)
0.0						÷
0.5						
1.0	32.25	27,75	16.4	16.4	11.00	0.0435
2.0	30.00	25.50	15.1	15.1	11.37	0.0313
5.0	28.00	23.50	13.9	13.9	11.70	0.0201
15.0	25.25	20.75	12.3	12.3	12.15	0.0118
30.0	23.50	19.00	11.3	11.3	12.44	0.0084
60.0	22.00	17.50	10.4	10.4	12.68	0.0060
120.0	21.00	16.50	9.8	9.8	12.85	0.0043
250.0	20.25	15.75	9.3	9.3	12.97	0.0030
1440.0	19.00	14.50	8.6	8.6	13.17	0.0013

Grain Diameter = K\*(SQRT(L/T))

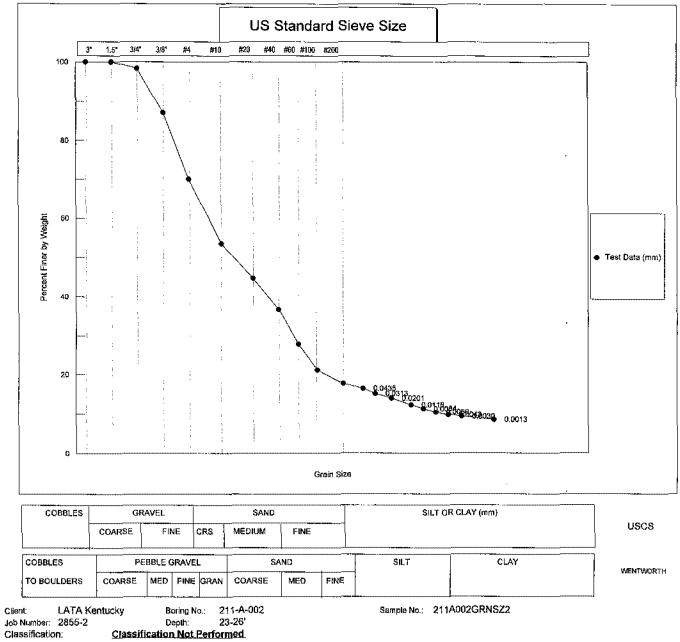
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Date: 09/17/2012 Date: 9/17 (2





F-18

Client: LATA Kentucky Job Number: 2855-2

CLIENT LATA Ken	tucky	JOB NO. 2855-2	
BORING NO. DEPTH SAMPLE NO. SOIL DESCR. LOCATION	211-A-002 37.4-39.0' 211A002GRNSZ3 ERI12-SW-SWMU211A SW Plume RDSI Geotechnical	SAMPLED DATE TESTED WASH SIEVE DRY SIEVE	8/30/12 KD 9/13/12 JS Yes No
MOISTURE DATA		WASH SIEVE ANALY	SIS
HYGROSCOPIC	Yes	Wt. Total Sample Wet (g)	842.64
NATURAL	No	Weight of + #10 Before Washing (g) Weight of + #10	1.54
Wt. Wet Soil & Pan (g) Wt. Dry Soil & Pan (g)		After Washing (g) Weight of - #10	1.36
Wt. Lost Moisture (g) Wt. of Pan Only (g)	0.71 2.98	Wet (g) Weight of - #10	841.10
Wt. of Dry Soil (g) Moisture Content %	33.70 2.1	Dry (g) Wt. Total Sample	823.92
		Dry (g)	825.28
Wt. Hydrom. Sample W Wt. Hydrom. Sample D		Calc. Wt. "W" (g) Calc. Mass + #10	69.31 0.11

Sieve	Pan	Indiv.	Indiv.	Cum.	Cum.	%
Number	Weight	Wt. + Pan	Wt.	Wt.	%	Finer
(Size)	(g)	(g)	Retain.	Retain.	Retain.	By Wt.
3" 1 1/2" 3/4" 3/8" #4 #10	0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.48 0.88	0,00 0.00 0.00 0.00 0.48 0,88	0.00 0.00 0.00 0.00 0.48 1.36	0.0 0.0 0.0 0.1 0.2	100.0 100.0 100.0 99.9 99.8
#20	3.23	3.44	0.21	0.21	0.5	99.5
#40	3.12	4.35	1.22	1.43	2.2	97.8
#60	3.25	7.71	4.46	5.89	8.7	91.3
#100	3.05	8.12	5.07	10.96	16.0	84.0
#200	2.98	7.40	4.42	15.38	22.4	77.6

Data entered by: Data checked by: FileName: LKHYNS23

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Date: 09/17/2012 Date: 9/17/12



CLIENT LATA K	entucky	JOB NO. 2855-2	
BORING NO. DEPTH SAMPLE NO, SOIL DESCR. LOCATION	211-A-002 37.4-39.0' 211A002GRNSZ3 ERI12-SW-SWMU211A SW Plume RDSI Geotechnical	SAMPLED DATE TESTED WASH SIEVE DRY SIEVE	8/30/12 KD 9/13/12 JS Yes No
Hydrometer # Sp. Gr. of Soil Value of "alpha"	ASTM 152 H 2.65 1.00	Temp., Deg. C Temp. Coef. K Wt. Dry Sample "W"	23.4 0.01311 69.306

Deflocculant	Sodium Hexametaphosphate	% of Total Sample	100.0
Defloc. Corr'n	4.5		
Meniscus Corr'n	0.0		

T Elapsed Time (min)	Hydrometer Original	Reading Corrected "R"	100Ra/W	% Total Sample	Effective Depth L	Grain Diameter (mm)
0.0						
0.5						
1.0	57.00	52.50	75.8	75.8	6.94	0.0345
2,0	53.00	48.50	70.0	70.0	7.60	0.0255
5.0	49.00	44.50	64.2	64.2	8.25	0.0168
15.0	44.00	39.50	57.0	57.0	9.07	0.0102
30.0	40.50	36.00	51.9	51.9	9.65	0.0074
60.0	37.00	32.50	46.9	46.9	10.22	0.0054
120.0	35.00	30,50	44.0	44.0	10.55	0.0039
250.0	32.50	28.00	40.4	40.4	10.96	0.0027
1440.0	27.50	23.00	33.2	33.2	11.78	0.0012

Grain Diameter = K\*(SQRT(L/T))

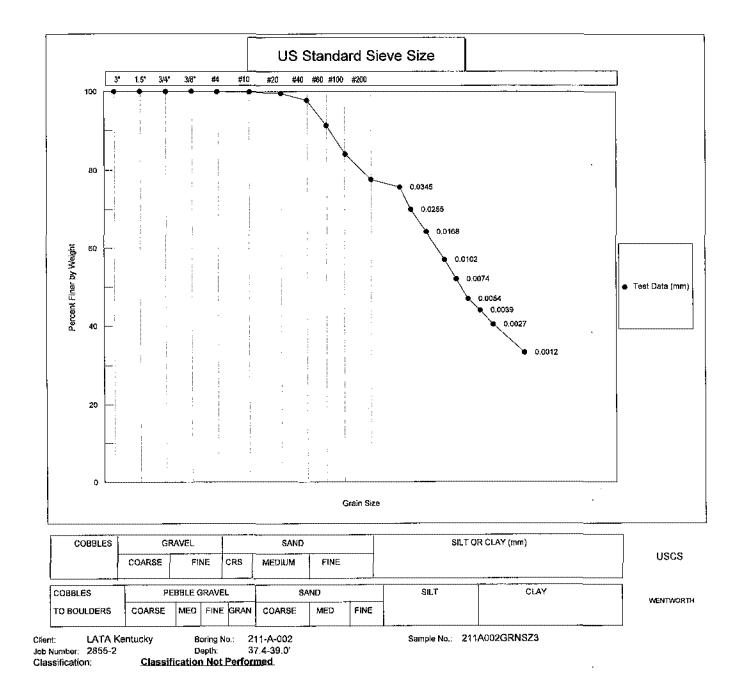
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Date: 09/17/2012 Date: 9/17 12



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F-21

CLIENT LATA Ken	tucky	JOB NO. 2855-03	
BORING NO. DEPTH SAMPLE NO. SOIL DESCR. LOCATION	211-A-012 12-15' 211A012GRNSZ1 ERI12-SW-SWMU211A SW Plume RDSI Geotechnical	SAMPLED DATE TESTED WASH SIEVE DRY SIEVE	09/17/12 KD 10/02/12 JS Yes No
MOISTURE DATA		WASH SIEVE ANALY	SIS
HYGROSCOPIC	Yes	Wt. Total Sample Wet (g)	1107.23
NATURAL	No	Weight of + #10 Before Washing (g) Weight of + #10	4.40
Wt. Wet Soil & Pan (g) Wt. Dry Soil & Pan (g)		After Washing (g) Weight of - #10	4.22
Wt. Lost Moisture (g) Wt. of Pan Only (g)	0.74 3.03	Wet (g) Weight of - #10	1102.83
Wt. of Dry Soil (g) Moisture Content %	39.52 1.9	Dry (g) Wt. Total Sample	1082.74
		Dry (g)	1086.96
Wt. Hydrom. Sample V Wt. Hydrom. Sample D		Calc. Wt. "W' (g) Calc. Mass + #10	66.02 0.26

Sieve	Pan	Indiv.	Indiv.	Cum.	Cum.	%
Number	Weight	Wt. + Pan	Wt.	Wt.	%	Finer
(Size)	(g)	(g)	Retain.	Retain.	Retain.	By Wt.
3"	0.00	0.00	0.00	0.00	0.0	100.0
1 1/2"	0.00	0.00	0.00	0.00	0.0	100.0
3/4"	0.00	0.00	0.00	0.00	0.0	100.0
3/8"	0.00	2.96	2.96	2.96	0.3	99.7
#4	0.00	0.93	0.93	3.89	0.4	99.6
#10	0.00	0.33	0.33	4.22	0.4	99.6
#20	1.78	1.83	0.05	0.05	0.5	99.5
#40	1.79	2.14	0.35	0.40	1.0	99.0
#60	1.77	3.04	1.27	1.67	2.9	97.1
#100	1.80	3.62	1.82	3.49	5.7	94.3
#200	1.77	3.10	1.33	4.82	7.7	92.3

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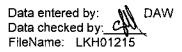
CLIENT LATA Ken	tucky	JOB NO. 2855-03	
BORING NO. DEPTH SAMPLE NO. SOIL DESCR. LOCATION	211-A-012 12-15' 211A012GRNSZ1 ERI12-SW-SWMU211A SW Plume RDSI Geotechnical	SAMPLED DATE TESTED WASH SIEVE DRY SIEVE	09/17/12 KD 10/02/12 JS Yes No
Hydrometer # Sp. Gr. of Soil Value of "alpha" Deflocculant Defloc. Corr'n Meniscus Corr'n	ASTM 152 H 2.65 1.00 Sodium Hexametaphosphate 5.0 0.0	Temp., Deg. C Temp. Coef. K Wt. Dry Sample "W" % of Total Sample	23.2 0.01314 66.016 100.0

T Elapsed Time (min)	Hydrometer Original	Reading Corrected "R"	100Ra/W	% Total Sample	Effective Depth L	Grain Diameter (mm)
0.0				***		
0.5					·	
1.0	48.00	43.00	65.1	65.1	8.42	0.0381
2.0	45.00	40.00	60.6	60.6	8.91	0.0277
5.0	38.00	33.00	50.0	50.0	10.06	0.0186
15.0	29.00	24.00	36.4	36.4	11.53	0.0115
30.0	24.00	19.00	28.8	28.8	12.35	0.0084
60.0	21.00	16.00	24.2	24.2	12.85	0.0061
120.0	19.75	14.75	22,3	22.3	13.05	0.0043
250.0	18.25	13.25	20.1	20.1	13.30	0.0030
1440.0	17.00	12.00	18.2	18.2	13.50	0.0013

Grain Diameter = K\*(SQRT(L/T))

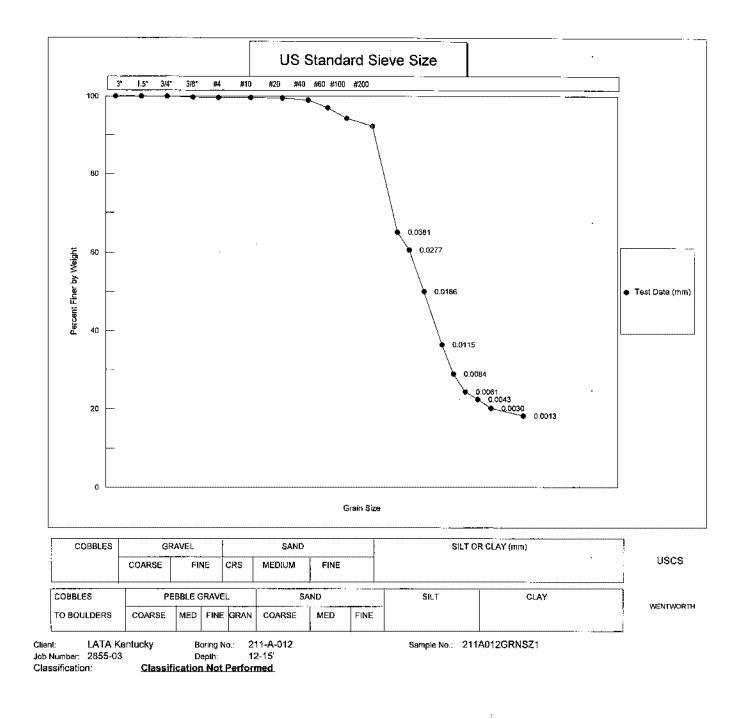
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Date: 10/04/2012 Date: 10/1/12





CLIENT LATA Ken	tucky	JOB NO. 2855-03	
BORING NO. DEPTH SAMPLE NO. SOIL DESCR. LOCATION	211-A-012 20-23' 211A012 GRNSZ2 ERI12-SW-SWMU211A SW Plume RDSI Geotechnical	SAMPLED DATE TESTED WASH SIEVE DRY SIEVE	09/17/12 KD 10/02/12 JS Yes No
MOISTURE DATA		WASH SIEVE ANALY	SIS
HYGROSCOPIC	Yes	Wt. Total Sample Wet (g)	1023.88
NATURAL	No	Weight of + #10 Before Washing (g)	122.94
Wt. Wet Soil & Pan_(g) Wt. Dry Soil & Pan_(g)		Weight of + #10 After Washing (g) Weight of - #10	85.39
Wt. Lost Moisture (g) Wt. of Pan Only (g)	0.74 3.08	Weight of - #10 Wet (g) Weight of - #10	900.94
Wt. of Dry Soil (g) Moisture Content %	31.85 2.3	Dry (g) Wt. Total Sample	917.18
		Dry (g)	1002.57
Wt. Hydrom. Sample V Wt. Hydrom. Sample D		Calc. Wt. "W" (g) Calc. Mass + #10	76.75 6.54

Sieve	Pan	Indiv.	Indiv.	Cum.	Cum.	%
Number	Weight	Wt. + Pan	Wt.	Wt.	%	Finer
(Size)	(g)	(g)	Retain.	Retain.	Retain.	By Wt.
3" 1 1/2" 3/4" 3/8" #4 #10	0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 20.30 38.42 26.67	0.00 0.00 20.30 38.42 26.67	0.00 0.00 20.30 58.72 85.39	0.0 0.0 2.0 5.9 8.5	100.0 100.0 100.0 98.0 94.1 91.5
#20	1.78	3.64	1.86	1.86	10.9	89.1
#40	1.75	6.01	4.26	6.12	16.5	83.5
#60	1.76	11.75	9.99	16.11	29.5	70.5
#100	1.78	8.69	6.91	23.02	38.5	61.5
#200	1.78	4.95	3.17	26.19	42.6	57.4

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Date: 10/04/2012 Date: 10/14/12



CLIENT LATA Ken	tucky	JOB NO. 2855-03	
BORING NO. DEPTH SAMPLE NO. SOIL DESCR. LOCATION	211-A-012 20-23' 211A012 GRNSZ2 ERI12-SW-SWMU211A SW Plume RDSI Geotechnical	SAMPLED DATE TESTED WASH SIEVE DRY SIEVE	09/17/12 KD 10/02/12 JS Yes No
Hydrometer # Sp. Gr. of Soil Value of "alpha" Deflocculant Defloc. Corr'n Meniscus Corr'n	ASTM 152 H 2.65 1.00 Sodium Hexametaphosphate 5.0 0.0	Temp., Deg. C Temp. Coef. K Wt. Dry Sample "W" % of Total Sample	23.2 0.01314 76.747 100.0

T Elapsed Time (min)	Hydrometer Original	Reading Corrected "R"	100Ra/W	% Total Sample	Effective Depth L	Grain Diameter (mm)
0.0		·				
0.5						
1.0	46.00	41.00	53.4	53.4	8.75	0.0389
2.0	43.00	38.00	49.5	49.5	9.24	0.0282
5.0	38.00	33.00	43.0	43.0	10.06	0.0186
15.0	32.75	27.75	36.2	36.2	10.92	0.0112
30.0	30.00	25.00	32.6	32.6	11.37	0.0081
60.0	28.25	23.25	30.3	30.3	11.66	0.0058
120.0	27.00	22.00	28.7	28.7	11.86	0.0041
250.0	26.00	21.00	27.4	27.4	12.03	0.0029
1440.0	24.50	19.50	25.4	25.4	12.27	0.0012

Grain Diameter = K\*(SQRT(L/T))

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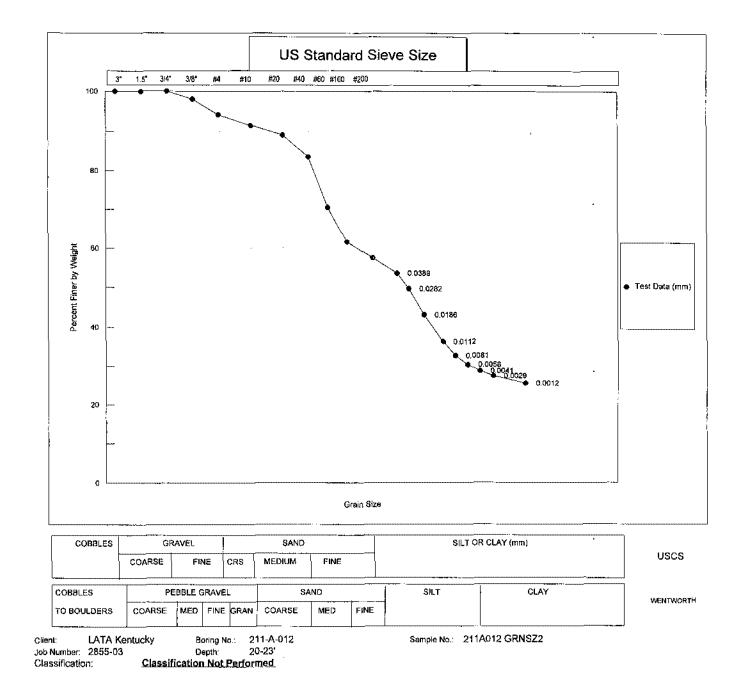
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CLIENT LATA Ken	tucky	JOB NO. 2855-03	
BORING NO. DEPTH SAMPLE NO. SOIL DESCR. LOCATION	211-A-012 40-42' 211A012GRNSZ3 ERI12-SW-SWMU211A SW Plume RDSI Geotechnical	SAMPLED DATE TESTED WASH SIEVE DRY SIEVE	09/17/12 KD 10/02/12 JS Yes No
MOISTURE DATA		WASH SIEVE ANALY	SIS
HYGROSCOPIC	Yes	Wt. Total Sample Wet (g)	1243.67
NATURAL	No	Weight of + #10	1243.07
		Before Washing (g) Weight of + #10	7.17
Wt. Wet Soil & Pan (g)		After Washing (g)	6.35
Wt. Dry Soil & Pan (g)		Weight of - #10	
Wt. Lost Moisture (g) Wt. of Pan Only (g)	0.51 3.06	Wet (g) Weight of - #10	1236.50
Wt. of Pan Only (g) Wt. of Dry Soil (g)	32.29	Dry (g)	1218.08
Moisture Content %	1.6	Wt. Total Sample	1210.00
		Dry (g)	1224.43
Wt. Hydrom. Sample V	Vet (g) 71.16	Calc. Wt. "W" (g)	70.42
Wt. Hydrom. Sample D		Calc. Mass + #10	0.37

Sieve	Pan	Indiv.	Indiv.	Cum.	Cum.	%
Number	Weight	Wt. + Pan	Wt.	Wt.	%	Finer
(Size)	(g)	(g)	Retain.	Retain.	Retain.	By Wt.
3"	0.00	0.00	0.00	0.00	0.0	100.0
1 1/2"	0.00	0.00	0.00	0.00	0.0	100.0
3/4"	0.00	0.00	0.00	0.00	0.0	100.0
3/8"	0.00	0.00	0.00	0.00	0.0	100.0
#4	0.00	1.76	1.76	1.76	D.1	99.9
#10	0.00	4.59	4.59	6.35	0.5	99.5
#20	1.78	2.84	1.06	1.06	2.0	98.0
#40	1.78	5.92	4.14	5.20	7.9	92.1
#60	1.78	9.68	7.90	13.10	19.1	80.9
#100	1.79	11.09	9.30	22.40	32.3	67.7
#200	1.78	10.51	8.73	31.13	44.7	55.3

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CLIENT LATA Ke	entucky	JOB NO. 2855-03	
BORING NO. DEPTH SAMPLE NO. SOIL DESCR. LOCATION	211-A-012 40-42' 211A012GRNSZ3 ERI12-SW-SWMU211A SW Plume RDSI Geotechnical	SAMPLED DATE TESTED WASH SIEVE DRY SIEVE	09/17/12 KD 10/02/12 JS Yes No
Hydrometer # Sp. Gr. of Soil Value of "alpha" Deflocculant Defloc. Corr'n Meniscus Corr'n	ASTM 152 H 2.65 1.00 Sodium Hexametaphosphate 5.0 0.0	Temp., Deg. C Temp. Coef. K Wt. Dry Sample "W" % of Total Sample	23.2 0.01314 70.422 100.0

T Etapsed Time (min)	Hydrometer Original	Reading Corrected "R"	100Ra/W	% Total Sampie	Effective Depth L	Grain Diameter (mm)
0.0						
0.5		***				
1.0	39.00	34.00	48.3	48.3	9.89	0.0413
2.0	36.50	31.50	44.7	44.7	10.30	0.0298
5.0	33.75	28.75	40.8	40.8	10.76	0.0193
15.0	29.00	24.00	34.1	34.1	11.53	0.0115
30.0	26.00	21.00	29.8	29.8	12.03	0.0083
60.0	23.00	18.00	25.6	25.6	12.52	0.0060
120.0	21.00	16.00	22.7	22.7	12.85	0.0043
250.0	19.00	14.00	19.9	19.9	13.17	0.0030
1440.0	17.25	12.25	17.4	17.4	13.46	0.0013

Grain Diameter = K\*(SQRT(L/T))

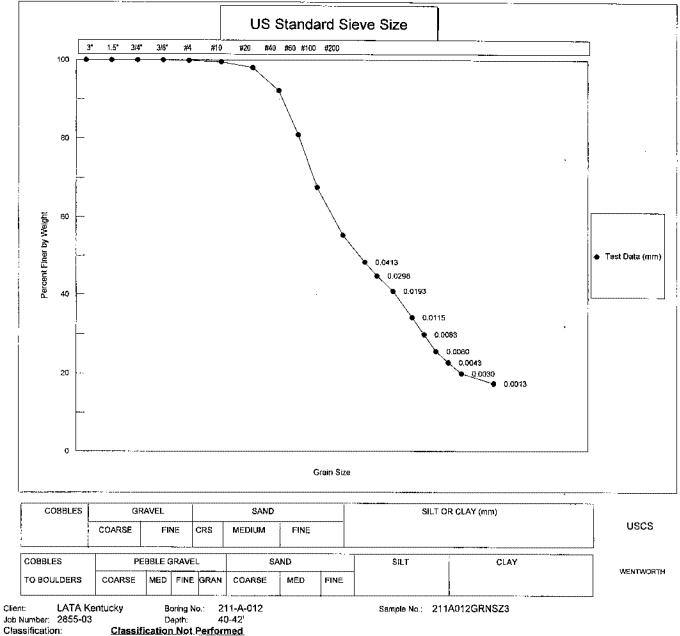
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CLIENT LATA Ken	tucky	JOB NO. 2855-03	
BORING NO. DEPTH SAMPLE NO. SOIL DESCR. LOCATION	211-A-027 12-15' 211A027GRNSZ1 ERI12-SW-SWMU211A SW Plume RDSI Geotechnical	SAMPLED DATE TESTED WASH SIEVE DRY SIEVE	09/18/12 KD 10/02/12 JS Yes No
MOISTURE DATA		WASH SIEVE ANALY	SIS
HYGROSCOPIC	Yes	Wt. Total Sample	4074.04
NATURAL	No	Wet (g) Weight of + #10 Before Washing (g)	1074.24 0.34
		Weight of + #10	
Wt. Wet Soil & Pan (g)		After Washing (g)	0.29
Wt. Dry Soil & Pan (g)		Weight of - #10	
Wt. Lost Moisture (g)	0.80	Wet (g)	1073.90
Wt. of Pan Only (g)	3.09	Weight of - #10	4044.00
Wt. of Dry Soil (g) Moisture Content %	28.18 2.8	Dry (g)	1044.30
Moisture Content %	2.0	Wt. Total Sample Dry (g)	1044.59
Wt. Hydrom. Sample V		Calc. Wt. "W" (g)	65.07
Wt. Hydrom. Sample D	ry (g) 65.05	Calc. Mass + #10	0.02

Sieve Number (Size)	Pan Weight (g)	Indiv. Wt. + Pan (g)	Indiv. Wt. Retain.	Cum. Wt. Retain.	Cum. % Retain.	% Finer By Wt.
3"	0.00	0.00	0.00	0.00	0.0	100.0
1 1/2"	0.00	0.00	0.00	0.00	0.0	100.0
3/4"	0.00	0.00	0.00	0.00	0.0	100.0
3/8"	0.00	0.00	0.00	0.00	0.0	100.0
#4	0.00	0.00	0.00	0.00	0.0	100.0
#10	0.00	0.29	0.29	0.29	0.0	100.0
#20	3.01	3.09	0.08	0.08	0.1	99.9
#40	3,19	3.66	0.47	0.55	0.9	99.1
#60	3.05	5.41	2.36	2.91	4.5	95.5
#100	3.08	7.07	3.99	6.90	10.6	89.4
#200	3.07	5.54	2.47	9.37	14.4	85.6

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Date: 10/5/2012 Date: 10/5/12



CLIENT LATA Ke	ntucky	JOB NO. 2855-03	
BORING NO. DEPTH SAMPLE NO. SOIL DESCR. LOCATION	211-A-027 12-15' 211A027GRNSZ1 ERI12-SW-SWMU211A SW Plume RDSI Geotechnical	SAMPLED DATE TESTED WASH SIEVE DRY SIEVE	09/18/12 KD 10/02/12 JS Yes No
Hydrometer # Sp. Gr. of Soii Value of "alpha" Deflocculant Defloc. Corr'n Meniscus Corr'n	ASTM 152 H 2.65 1.00 Sodium Hexametaphosphate 5.0 0.0	Temp., Deg. C Temp. Coef. K Wt. Dry Sample "W" % of Total Sample	23.3 0.01312 65.069 100.0

I Elapsed Time (min)	Hydrometer Original	Reading Corrected "R"	100Ra/W	% Total Sample	Effective Depth L	Grain Diameter (mm)
0.0						
0.5						
1.0	53.00	48.00	73.8	73.8	7.60	0.0362
2.0	47.50	42.50	65.3	65.3	8.50	0.0271
5.0	38.25	33.25	51.1	51.1	10.02	0.0186
15.0	29.00	24.00	36.9	36.9	11.53	0.0115
30.0	24.25	19.25	29.6	29.6	12.31	0.0084
60.0	22.50	17.50	26.9	26.9	12.60	0.0060
120.0	21.00	16.00	24.6	24.6	12.85	0.0043
250.0	19.00	14.00	21.5	21.5	13.17	0.0030
1440.0	18.00	13.00	20.0	20.0	13.34	0.0013

Grain Diameter = K\*(SQRT(L/T))

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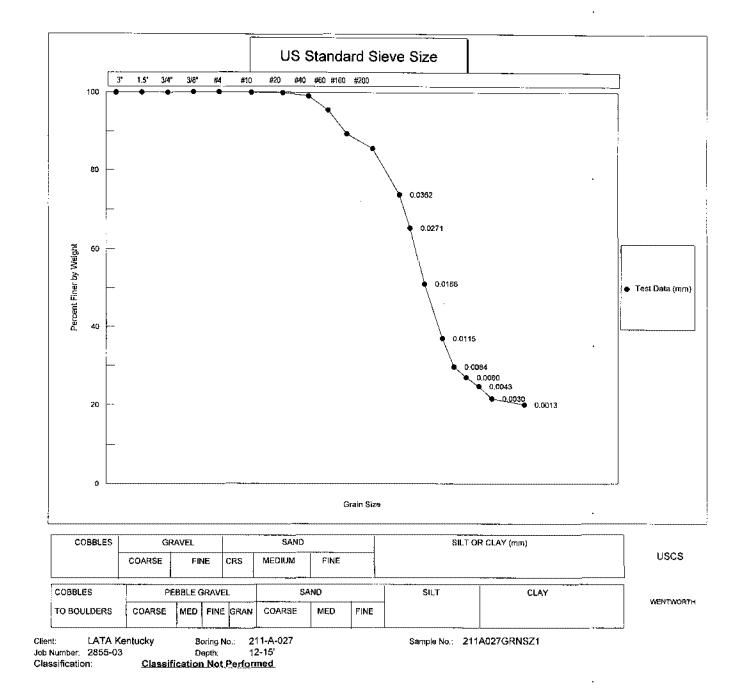
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CLIENT LATA Kent	lucky	JOB NO. 2855-03	
BORING NO. DEPTH SAMPLE NO. SOIL DESCR. LOCATION	211-A-027 22-25' 211A027GRNZ2 ERI12-SW-SWMU211A SW Plume RDSI Geotechnical	SAMPLED DATE TESTED WASH SIEVE DRY SIEVE	09/18/12 JS 10/02/12 JS Yes No
MOISTURE DATA		WASH SIEVE ANALY	SIS
HYGROSCOPIC	Yes	Wt. Total Sample Wet (g)	745.33
NATURAL	Νο	Weight of + #10 Before Washing (g) Weight of + #10	208.89
Wt. Wet Soil & Pan (g) Wt. Dry Soil & Pan (g)	33.43 32.67	After Washing (g) Weight of - #10	169.94
Wt. Lost Moisture (g) Wt. of Pan Only (g)	0.76 3.07	Wet (g) Weight of - #10	536.44
Wt. of Dry Soil (g) Moisture Content %	29.60 2.6	Dry (g) Wt. Total Sample	560.99
		Dry (g)	730.93
Wt. Hydrom. Sample W Wt. Hydrom. Sample D		Calc. Wt. "W" (g) Calc. Mass + #10	110.41 25.67

Sieve Number (Size)	Pan Weight (g)	Indiv. Wt. + Pan (g)	Indiv. Wt. Retain.	Cum. Wt. Retain.	Cum. % Retain.	% Finer By Wt.
3"	0.00	0.00	0.00	0.00	0.0	100.0
1 1/2"	0.00	0.00	0.00	0.00	0.0	100.0
3/4"	0.00	22.89	22.89	22.89	3.1	96.9
3/8"	0.00	48.61	48.61	71.50	9,8	90.2
#4	0.00	53.80	53.80	125.30	17.1	82.9
#10	0.00	44.64	44.64	169.94	23.2	76.8
#20	3.01	7.83	4.82	4.82	27.6	72.4
#40	3.12	12.75	9.64	14.45	36.3	63.7
#60	3.12	15.51	12.40	26.85	47.6	52.4
#100	3.05	12.36	9.31	36.16	56.0	44.0
#200	3.02	6.57	3.55	39.70	59.2	40.8

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Date: 10/5//2012 Date: 10/5//2



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CLIENT LATA Ke	entucky	JOB NO. 2855-03	
BORING NO. DEPTH SAMPLE NO. SOIL DESCR. LOCATION	211-A-027 22-25' 211A027GRNZ2 ERI12-SW-SWMU211A SW Plume RDS/ Geotechnical	SAMPLED DATE TESTED WASH SIEVE DRY SIEVE	09/18/12 JS 10/02/12 JS Yes No
Hydrometer # Sp. Gr. of Soil Value of "alpha" Deflocculant Defloc. Corr'n Meniscus Corr'n	ASTM 152 H 2.65 1.00 Sodium Hexametaphosphate 5.0 0.0	Temp., Deg. C Temp. Coef. K Wt. Dry Sample "W" % of Total Sample	23.4 0.01311 110.414 100.0

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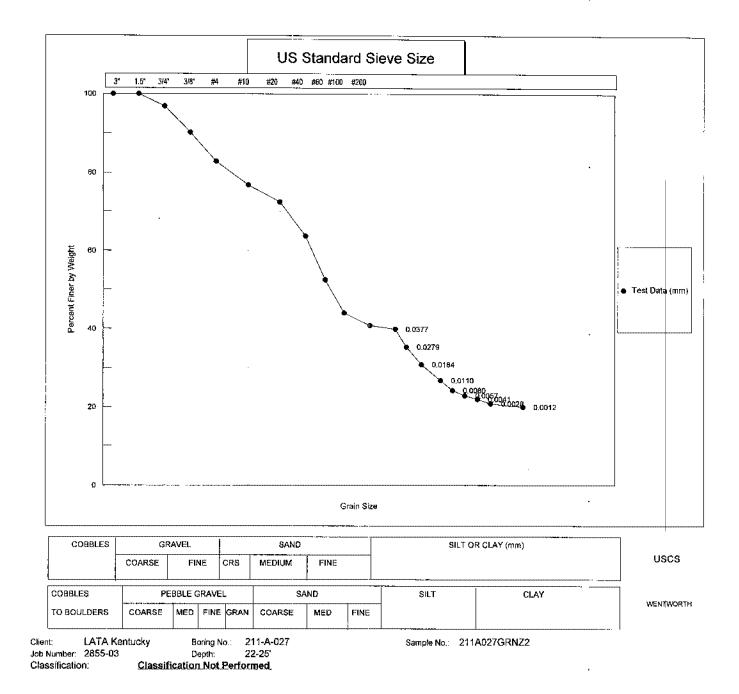
Elapsed Time (min)	Hydrometer Original	Reading Corrected "R"	100Ra/W	% ⊺otal Sample	Effective Depth L	Grain Diameter (mm)
0.0					·	
0.5					·	
1.0	49.00	44.00	39.8	39.8	8.25	0.0377
2.0	44.00	39.00	35.3	35.3	9.07	0.0279
5.0	39.00	34.00	30.8	30.8	9.89	0.0184
15.0	34.50	29.50	26.7	26.7	10.63	0.0110
30.0	31.75	26.75	24.2	24.2	11.08	0.0080
60.0	30.25	25.25	22.9	22.9	11.33	0.0057
120.0	29.25	24.25	22.0	22.0	11.49	0.0041
250.0	28.00	23.00	20.8	20.8	11.70	0.0028
1440.0	27.00	22.00	19.9	19.9	11.86	0.0012

Grain Diameter = K\*(SQRT(L/T))

Data entered by: DAW Data checked by: DAW FileName: LKHU2225

Date: 10/05/2012 Date: 10/5/12





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| CLIENT LATA Ken                                              | tucky                                                                                     | JOB NO. 2855-03                                   |                                         |
|--------------------------------------------------------------|-------------------------------------------------------------------------------------------|---------------------------------------------------|-----------------------------------------|
| BORING NO.<br>DEPTH<br>SAMPLE NO.<br>SOIL DESCR.<br>LOCATION | 211-A-027<br>35.5-37'<br>211A027GRNSZ3<br>ERI12-SW-SWMU211A<br>SW Plume RDSI Geotechnical | SAMPLED<br>DATE TESTED<br>WASH SIEVE<br>DRY SIEVE | 09/18/12 KD<br>10/02/12 JS<br>Yes<br>No |
| MOISTURE DATA                                                |                                                                                           | WASH SIEVE ANALY                                  | SIS                                     |
| HYGROSCOPIC                                                  | Yes                                                                                       | Wt. Total Sample<br>Wet (g)                       | 1121.88                                 |
| NATURAL                                                      | No                                                                                        | Weight of + #10                                   | 1121.00                                 |
|                                                              |                                                                                           | Before Washing (g)<br>Weight of + #10             | 491.75                                  |
| Wt. Wet Soil & Pan (g)                                       |                                                                                           | After Washing (g)                                 | 462.56                                  |
| Wt. Dry Soil & Pan (g)                                       | 34.66                                                                                     | Weight of - #10                                   |                                         |
| Wt. Lost Moisture (g)                                        | 0.17                                                                                      | Wet (g)                                           | 630.13                                  |
| Wt. of Pan Only (g)                                          | 3.06                                                                                      | Weight of - #10                                   |                                         |
| Wt. of Dry Soil (g)                                          | 31.60                                                                                     | Dry (g)                                           | 655.79                                  |
| Moisture Content %                                           | 0.5                                                                                       | Wt. Total Sample                                  | 4440.05                                 |
|                                                              |                                                                                           | Dry (g)                                           | 1118.35                                 |
| Wt. Hydrom, Sample W                                         | /et (a) 89.44                                                                             | Calc. Wt. "W" (g)                                 | 151.72                                  |
| Wt. Hydrom. Sample D                                         |                                                                                           | Calc. Mass + #10                                  | 62.75                                   |
|                                                              | 2 NG7                                                                                     |                                                   |                                         |

| Sieve<br>Number<br>(Size) | Pan<br>Weight<br>(g) | Indiv.<br>Wt. + Pan<br>(g) | Indiv.<br>Wt.<br>Retain. | Cum.<br>Wt.<br>Retain. | Cum.<br>%<br>Retain. | %<br>Finer<br>By Wt. |
|---------------------------|----------------------|----------------------------|--------------------------|------------------------|----------------------|----------------------|
| 3"                        | 0.00                 | 0.00                       | 0.00                     | 0.00                   | 0.0                  | 100.0                |
| 1 1/2"                    | 0.00                 | 0.00                       | 0.00                     | 0.00                   | 0.0                  | 100.0                |
| 3/4"                      | 0.00                 | 11.05                      | 11.05                    | 11.05                  | 1.0                  | 99.0                 |
| 3/8"                      | 0.00                 | 177.82                     | 177.82                   | 188.87                 | 16.9                 | 83.1                 |
| #4                        | 0.00                 | 157.69                     | 157.69                   | 346.56                 | 31.0                 | 69.0                 |
| #10                       | 0.00                 | 116.00                     | 116.00                   | 462.56                 | 41,4                 | 58.6                 |
|                           |                      |                            |                          |                        |                      |                      |
| #20                       | 3.11                 | 13.47                      | 10.36                    | 10.36                  | 48.2                 | 51.8                 |
| #40                       | 2.96                 | 22.16                      | 19.20                    | 29.56                  | 60.8                 | 39.2                 |
| #60                       | 3.03                 | 27.11                      | 24.07                    | 53.63                  | 76.7                 | 23.3                 |
| #100                      | 2.99                 | 17.11                      | 14.11                    | 67.75                  | 86.0                 | 14.0                 |
| #200                      | 3.07                 | 8.03                       | 4.96                     | 72.71                  | 89.3                 | 10.7                 |

Data entered by: DAW Data checked by: <u>JU</u> FileName: LKHU3537

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Date: 10/05/2012 Date: 10/6/12



| CLIENT LATA Ken                                                                                          | tucky                                                                                     | JOB NO. 2855-03                                                           |                                         |
|----------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------|---------------------------------------------------------------------------|-----------------------------------------|
| BORING NO.<br>DEPTH<br>SAMPLE NO.<br>SOIL DESCR.<br>LOCATION                                             | 211-A-027<br>35.5-37'<br>211A027GRNSZ3<br>ERI12-SW-SWMU211A<br>SW Plume RDSI Geotechnical | SAMPLED<br>DATE TESTED<br>WASH SIEVE<br>DRY SIEVE                         | 09/18/12 KD<br>10/02/12 JS<br>Yes<br>No |
| Hydrometer #<br>Sp. Gr. of Soil<br>Value of "alpha"<br>Deflocculant<br>Defloc. Corr'n<br>Meniscus Corr'n | ASTM 152 H<br>2.65<br>1.00<br>Sodium Hexametaphosphate<br>0.0<br>5.0                      | Temp., Deg. C<br>Temp. Coef. K<br>Wt. Dry Sample "W"<br>% of Total Sample | 23.1<br>0.01315<br>151.715<br>100.0     |

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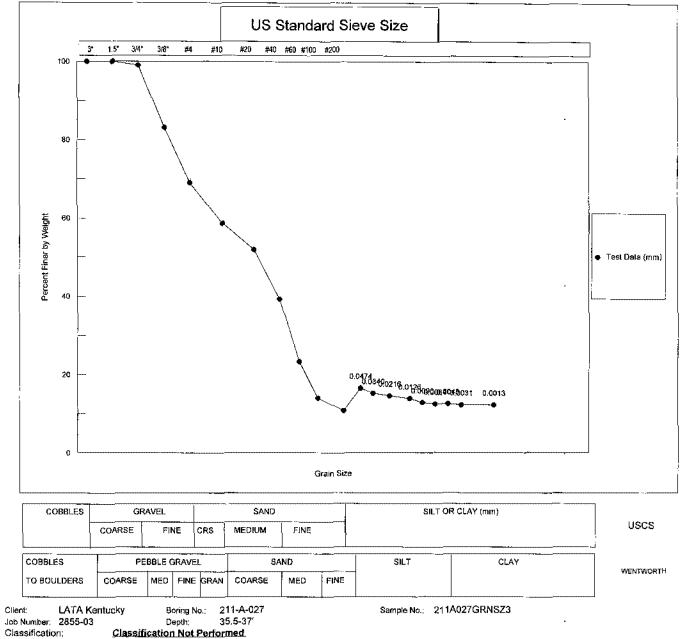
| Elapsed<br>Time<br>(min) | Hydrometer<br>Original | Reading<br>Corrected<br>"R" | 100Ra/W | %<br>Total<br>Sample | Effective<br>Depth<br>L | Grain<br>Diameter<br>(mm) |
|--------------------------|------------------------|-----------------------------|---------|----------------------|-------------------------|---------------------------|
| 0.0                      |                        |                             |         |                      |                         |                           |
| 0.5                      |                        |                             |         |                      |                         |                           |
| 1.0                      | 20.00                  | 25.00                       | 16.5    | 16.5                 | 13.01                   | 0.0474                    |
| 2.0                      | 18.00                  | 23.00                       | 15.2    | 15.2                 | 13.34                   | 0.0340                    |
| 5.0                      | 17.00                  | 22.00                       | 14.5    | 14.5                 | 13.50                   | 0.0216                    |
| 15.0                     | 16.00                  | 21.00                       | 13.8    | 13.8                 | 13.67                   | 0.0126                    |
| 30.0                     | 14.50                  | 19.50                       | 12.9    | 12.9                 | 13.91                   | 0.0090                    |
| 60.0                     | 14.00                  | 19.00                       | 12.5    | 12.5                 | 13.99                   | 0.0064                    |
| 120.0                    | 14.00                  | 19.00                       | 12.5    | 12.5                 | 13.99                   | 0.0045                    |
| 250.0                    | 13.50                  | 18.50                       | 12.2    | 12.2                 | 14.08                   | 0.0031                    |
| 1440.0                   | 13.50                  | 18.50                       | 12.2    | 12.2                 | 14.08                   | 0.0013                    |

Grain Diameter = K\*(SQRT(L/T))

Data entered by: DAW Data checked by: DAW FileName: LKHU3537

Date: 10/5/2012 Date: 10/5/10





F-39

Permeability Tests

# ASTM D5084-10

Advanced Terra Testing

## PERMEABILITY TEST - BACK PRESSURE SATURATED - FLOW PUMP METHOD ASTM D 5084

| CLIENT LA   | TA Environmental Services-Ky | JOB NO. 2855-04 |                  |
|-------------|------------------------------|-----------------|------------------|
| BORING NO.  | 211-A-027                    | SAMPLED         | 9/18/12 KD       |
| DEPTH       | 38-40'                       | TEST STARTED    | 10/12/12 CAL     |
| SAMPLE NO.  | 211A027PERM3                 | TEST FINISHED   | 10/23/12 CAL     |
| SOIL DESCR. | ERI12-SW-SWMU211A            | CELL NUMBER     | 14S              |
| LOCATION    | SW Plume RDSI Geotechnical   | SATURATED TEST  | Yes              |
| CONF. PRES. | PSF 5046                     | TEST TYPE       | TX/Pbp/Tap Water |

| MOISTURE/DENSITY<br>DATA                         | BEFORE<br>TEST | AFTER<br>TEST  |        |
|--------------------------------------------------|----------------|----------------|--------|
| Wt. Soil + Moisture (g)                          | 213.6          | 209.4          |        |
| Wt. Wet Soil & Pan (g)<br>Wt. Dry Soil & Pan (g) | 220.3<br>186.4 | 216.1<br>186.4 |        |
| Wt. Lost Moisture (g)                            | 33.8           | 29.7           |        |
| Wt. of Pan Only (g)                              | 6.7            | 6.7            |        |
| Wt. of Dry Soil (g)                              | 179.8          | 179.8          |        |
| Moisture Content %                               | 18.8           | 16.5           |        |
| Wet Density PCF                                  | 133.0          | 134.9          |        |
| Dry Density PCF                                  | 111.9          | 115.8          |        |
| Init. Diameter (in)                              | 1.611          | (cm)           | 4.092  |
| Init. Area (sq in)                               | 2.038          | (sq cm)        | 13.152 |
| Init. Height (in)                                | 3.002          | (cm)           | 7.625  |
| Vol. Bef. Consol. (cu ft)                        | 0.00354        |                |        |
| Vol. After Consol. (cu ft)                       | 0.00342        |                |        |
| Porosity %                                       | 30.60          |                |        |

# FLOW PUMP CALCULATIONS

| Pump Setting                  | 5        |
|-------------------------------|----------|
| Velocity CM/Sec               | 3.29E-05 |
| Q (cc/s)                      | 1.05E-06 |
| Height                        | 2.962    |
| Diameter                      | 1.595    |
| Pressure (psi)                | 1.949    |
| Area after consol. (cm*cm)    | 12.883   |
| Gradient                      | 18.214   |
| Permeability k (cm/s)         | 4.5E-09  |
| Permeability k (m/s)          | 4.5E-11  |
| Back Pressure (psi)           | 98.0     |
| Cell Pressure (psi)           | 133.0    |
| Ave. Effective Stress (psi)   | 34.026   |
| Average temperature degree C: | 22.7     |

| Data entry by:     | MLM Date:        |
|--------------------|------------------|
| Checked by: Cr.    | Date: 10/24/2012 |
| FileName: LKP00273 | - / /            |

10/24/2012



## TRIAXAL COMPRESSION TEST DATA

| CLIENT LATA E   | nvironmental Services-Ky   | JOB NO. 2855-04 |                  |
|-----------------|----------------------------|-----------------|------------------|
| BORING NO.      | 211-A-027                  | SAMPLED         | 9/18/12 KD       |
| DEPTH           | 38-40'                     | TEST STARTED    | 10/12/12 CAL     |
| SAMPLE NO.      | 211A027PERM3               | TEST FINISHED   | 10/23/12 CAL     |
| SOIL DESCR.     | ERI12-SW-SWMU211A          | SETUP NO.       | 14S              |
| LOCATION        | SW Plume RDSI Geotechnical | SATURATED TEST  | Yes              |
| CONF. PRES. PSF | 5046                       | TEST TYPE       | TX/Pbp/Tap Water |

#### SATURATION DATA

| Cell  | Back  | Burette |      | Pore     |       |        |   |      |
|-------|-------|---------|------|----------|-------|--------|---|------|
| Pres. | Pres. | Reading |      | Pressure |       |        |   |      |
| (PSI) | (PSI) | (CC)    |      | (PSI)    |       | Change | В |      |
|       |       | Close   | Open | Close    | Open  |        |   |      |
| 40.0  | 38.0  | 1.4     | 6.3  |          |       |        |   |      |
| 50.0  | 48.0  | 7.8     | 8.6  | 38.5     | 47.5  | 9.0    |   | 0.90 |
| 60.0  | 58.0  | 9.3     | 10.0 | 48.4     | 57.3  | 8.9    |   | 0.89 |
| 70.0  | 68.0  | 9.9     | 10.7 | 58.7     | 67.6  | 8.9    |   | 0.89 |
| 80.0  | 78.0  | 11.0    | 11.7 | 69.0     | 77.8  | 8.8    |   | 0.88 |
| 90.0  | 88.0  | 11.9    | 12.6 | 78.9     | 88.3  | 9.4    |   | 0.94 |
| 100.0 | 98.0  | 12.8    |      | 88.8     | 98.1  | 9.3    |   | 0.93 |
| 110.0 |       | 14.0    | 14.1 | 98.4     | 107.9 | 9.5    |   | 0.95 |

## CONSOLIDATION DATA

3.002

0.040

2.962

2.038

1.997

| Elapsed<br>Time<br>(Min) | SQRT<br>Time<br>(Min) | Burette<br>Reading<br>(CC) | Volume<br>Defl.<br>(cc) |
|--------------------------|-----------------------|----------------------------|-------------------------|
| 0.00                     | 0.00                  | 0.80                       | 0.00                    |
| 0.25                     | 0.50                  | 3.05                       | -2.25                   |
| 0.5                      | 0.71                  | 3.10                       | -2.30                   |
| 1                        | 1.00                  | 3.15                       | -2.35                   |
| 2                        | 1.41                  | 3.25                       | -2.45                   |
| 4                        | 2.00                  | 3.40                       | -2.60                   |
| 9                        | 3.00                  | 3.70                       | -2.90                   |
| 16                       | 4.00                  | 3.95                       | -3.15                   |
| 30                       | 5.48                  | 4.40                       | -3.60                   |
| 60                       | 7.75                  | 5.00                       | -4.20                   |
| 120                      | 10.95                 | 5.80                       | -5.00                   |
| 240                      | 15.49                 | 6.70                       | -5.90                   |
| 360                      | 18.97                 | 7.40                       | -6.60                   |

| Initial Height  | (in)       |
|-----------------|------------|
| Height Change   | (in)       |
| Ht. After Cons. | (in)       |
| Initial Area (  | sq in)     |
| Area After Cons | s. (sa in) |

| min. voi. (00)   |
|------------------|
| Vol. Change (CC) |
| Cell Exp. (CC)   |
| Net Change (CC)  |
| Cons. Vol. (CC)  |
|                  |

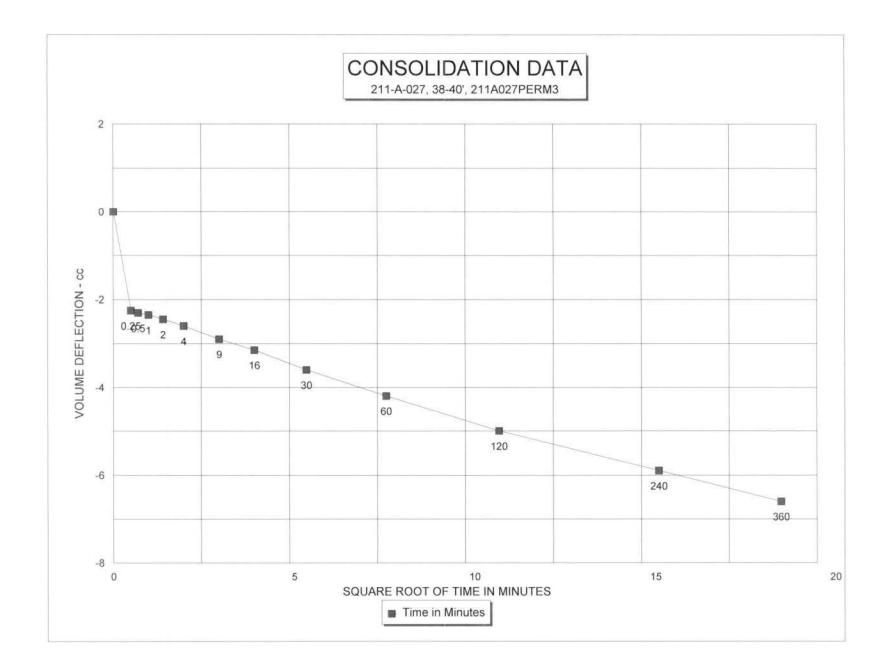
Init. Vol. (CC)

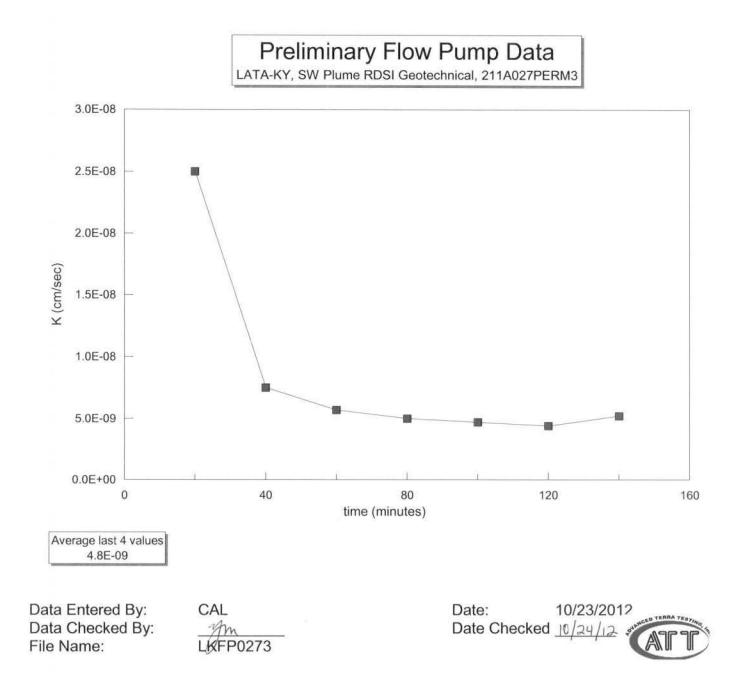


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| Data entry by:     | MLM       | Date:   |
|--------------------|-----------|---------|
| Checked by:        | Date: 10/ | 24/2012 |
| FileName: LKP00273 |           | 1       |

10/24/2012





Client LATA ENV. Services - Ky Job No. 2855-04 Sample No. 2114027 PERM3 ##GANA 38-40' Project SN Plame RDET Gestechnical Sampled 9/18/12 by 100 Prepped 10/12/12 by 2 Tx/Php 03 35 psi LK2855/LKDP0273 10/24/12

## PERMEABILITY TEST - BACK PRESSURE SATURATED - FLOW PUMP METHOD ASTM D 5084

| CLIENT LATA Env     | vironmental Services-Ky                         | JOB NO. 2855-04               |                        |
|---------------------|-------------------------------------------------|-------------------------------|------------------------|
| BORING NO.<br>DEPTH | 211-A-012<br>10-12'                             | SAMPLED<br>TEST STARTED       | 9/17/12<br>10/4/12 CAL |
| SAMPLE NO.          | 211A012PERM1                                    | TEST FINISHED                 | 10/6/12 CAL            |
| SOIL DESCR.         | ERI12-SW-SWMU211A<br>SW Plume RDSI Geotechnical | CELL NUMBER<br>SATURATED TEST | 13S<br>Yes             |
| CONF. PRES. PSF     | 1423                                            | TEST TYPE                     | TX/Pbp/Tap Water       |

| MOISTURE/DENSITY<br>DATA   | BEFORE<br>TEST | AFTER<br>TEST |        |
|----------------------------|----------------|---------------|--------|
| Wt. Soil + Moisture (g)    | 202.0          | 196.9         |        |
| Wt. Wet Soil & Pan (g)     | 208.6          | 203.5         |        |
| Wt. Dry Soil & Pan (g)     | 169.4          | 169.4         |        |
| Wt. Lost Moisture (g)      | 39.2           | 34.1          |        |
| Wt. of Pan Only (g)        | 6.6            | 6.6           |        |
| Wt. of Dry Soil (g)        | 162.8          | 162.8         |        |
| Moisture Content %         | 24.1           | 20.9          |        |
| Wet Density PCF            | 126.0          | 132.3         |        |
| Dry Density PCF            | 101.5          | 109.4         |        |
| Init. Diameter (in)        | 1.618          | (cm)          | 4.110  |
| Init. Area (sq in)         | 2.056          | (sq cm)       | 13.266 |
| Init. Height (in)          | 2.971          | (cm)          | 7.546  |
| Vol. Bef. Consol. (cu ft)  | 0.00354        |               |        |
| Vol. After Consol. (cu ft) | 0.00328        |               |        |
| Porosity %                 | 36.68          |               |        |

## FLOW PUMP CALCULATIONS

| Pump Setting                  | 15       |
|-------------------------------|----------|
| Velocity CM/Sec               | 9.85E-05 |
| Q (cc/s)                      | 3.15E-06 |
| Height                        | 2.950    |
| Diameter                      | 1.564    |
| Pressure (psi)                | 2.180    |
| Area after consol. (cm*cm)    | 12.399   |
| Gradient                      | 20.455   |
| Permeability k (cm/s)         | 1.2E-08  |
| Permeability k (m/s)          | 1.2E-10  |
| Back Pressure (psi)           | 38.0     |
| Cell Pressure (psi)           | 47.9     |
| Ave. Effective Stress (psi)   | 8.810    |
| Average temperature degree C: | 21.8     |

| Data entry by:     | MLM      | Date:   | 10/08/2012 |
|--------------------|----------|---------|------------|
| Checked by: Gtc    | Date: 10 | 100/10- |            |
| FileName: LKP0A121 |          |         |            |



## TRIAXAL COMPRESSION TEST DATA

| CLIENT LATA En  | vironmental Services-Ky    | JOB NO. 2855-04 |                  |
|-----------------|----------------------------|-----------------|------------------|
| BORING NO.      | 211-A-012                  | SAMPLED         | 9/17/12          |
| DEPTH           | 10-12'                     | TEST STARTED    | 10/4/12 CAL      |
| SAMPLE NO.      | 211A012PERM1               | TEST FINISHED   | 10/6/12 CAL      |
| SOIL DESCR.     | ERI12-SW-SWMU211A          | SETUP NO.       | 13S              |
| LOCATION        | SW Plume RDSI Geotechnical | SATURATED TEST  | Yes              |
| CONF. PRES. PSF | 1423                       | TEST TYPE       | TX/Pbp/Tap Water |

#### SATURATION DATA

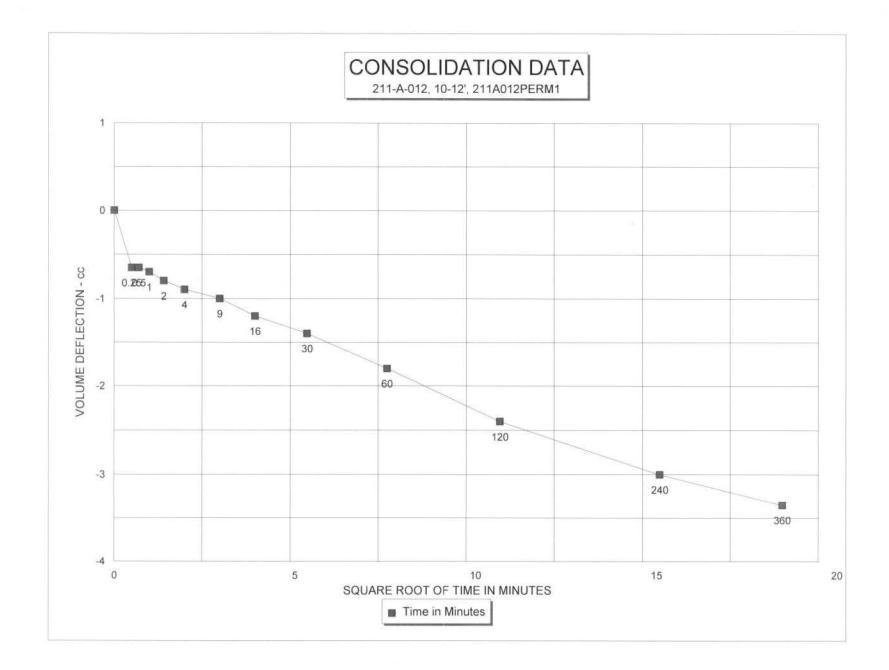
| Cell<br>Pres.<br>(PSI) | Back<br>Pres.<br>(PSI) | Burette<br>Reading<br>(CC) |      | Pore<br>Pressure<br>(PSI) |      | Change | В |      |
|------------------------|------------------------|----------------------------|------|---------------------------|------|--------|---|------|
|                        |                        | Close                      | Open | Close                     | Open |        |   |      |
| 40.0                   | 38.0                   | 1.8                        | 7.2  |                           |      |        |   |      |
| 50.0                   |                        | 12.0                       | 12.2 | 39.0                      | 48.5 | 9.5    |   | 0.95 |

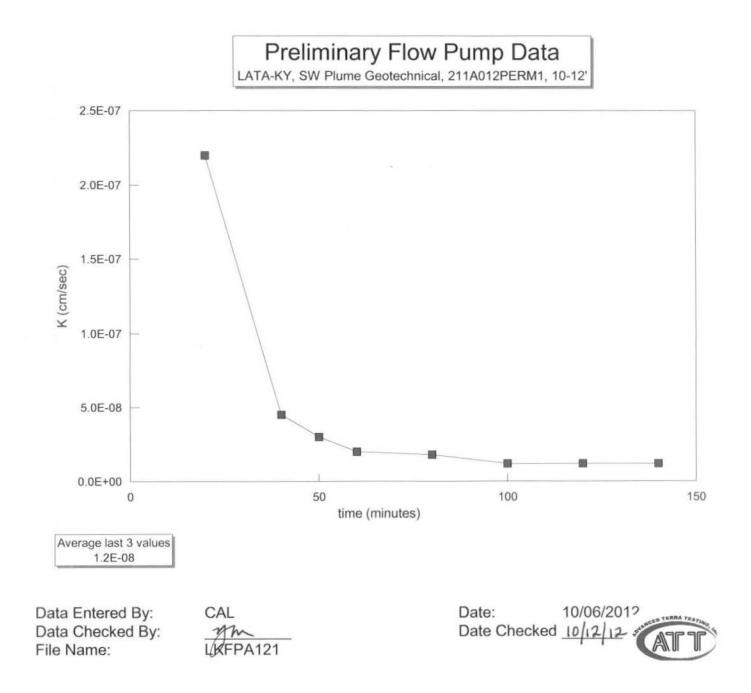
## CONSOLIDATION DATA

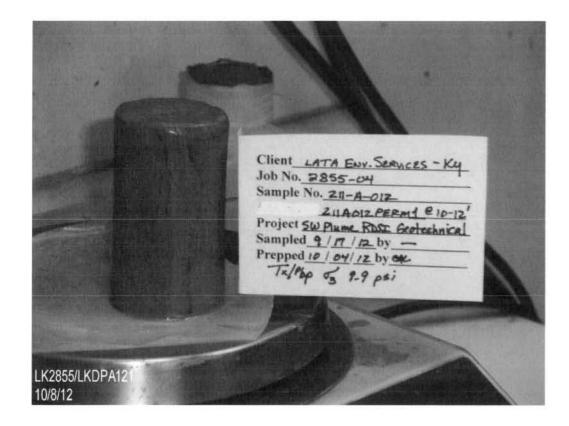
| Elapse<br>Time<br>(Min)  | Time             | Burette<br>Reading<br>(CC) | Volume<br>Defl.<br>(cc) |                       |
|--------------------------|------------------|----------------------------|-------------------------|-----------------------|
| (IVIII)                  | ((10)11)         | (88)                       | (00)                    |                       |
| 0.                       | .00 0.00         | 12.20                      | 0.00                    |                       |
| 0.                       | 25 0.50          | 12.85                      | -0.65                   |                       |
|                          | 0.5 0.71         | 12.85                      | -0.65                   |                       |
|                          | 1 1.00           | 12.90                      | -0.70                   |                       |
|                          |                  | 13.00                      | -0.80                   |                       |
|                          | 2 1.41<br>4 2.00 | 13.10                      | -0.90                   |                       |
|                          | 9 3.00           | 13.20                      | -1.00                   |                       |
|                          | 16 4.00          | 13.40                      | -1.20                   |                       |
|                          | 30 5.48          | 13.60                      | -1.40                   |                       |
|                          | 60 7.75          | 14.00                      | -1.80                   |                       |
| 1                        | 20 10.95         | 14.60                      | -2.40                   |                       |
| 2                        | 40 15.49         | 15.20                      | -3.00                   |                       |
| 3                        | 60 18.97         | 15.55                      | -3.35                   |                       |
| Initial Height (in)      | 2.971            | Init. Vol. (C              | C)                      | 100.12                |
| Height Change (in)       | 0.021            | Vol. Change                |                         | 14.80                 |
| Ht. After Cons. (in)     | 2.950            | Cell Exp. (0               |                         | 7.60                  |
| Initial Area (sq in)     | 2.056            | Net Change                 |                         | 7.20                  |
| Area After Cons. (sq in) | 1.922            | Cons. Vol. (               | CC)                     | 92.92                 |
| Data entry by: MLM       | Date:            | 10/08/2012                 |                         | STANCED TERRA TESTINO |

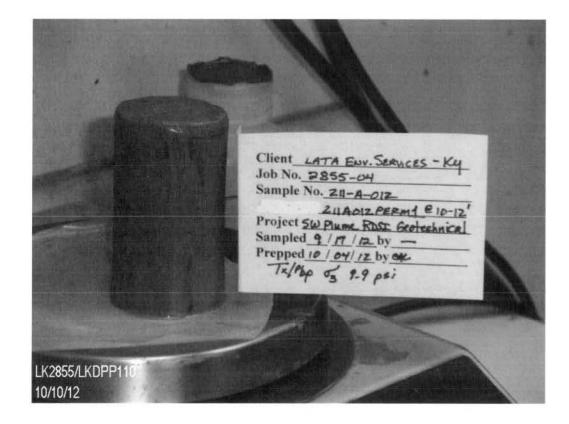
| Data entry by:     | MLM Date       | 2 |
|--------------------|----------------|---|
| Checked by: CK     | Date: 10/11/12 |   |
| FileName: LKP0A121 |                |   |











| CLIENT                                                              | LATA Envi | ronmental Service-Ky                                                                           | JOB NO. 2855-04                                                                        |                                                                           |
|---------------------------------------------------------------------|-----------|------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------|---------------------------------------------------------------------------|
| BORING N<br>DEPTH<br>SAMPLE N<br>SOIL DESC<br>LOCATION<br>CONF. PRE | O.<br>CR. | 211-A-012<br>23-25'<br>211A012PERM2<br>ERI12-SW-SWMU211A<br>SW Plume RDSI Geotechnical<br>3105 | SAMPLED<br>TEST STARTED<br>TEST FINISHED<br>CELL NUMBER<br>SATURATED TEST<br>TEST TYPE | 9/17/12<br>10/04/12 CAL<br>10/09/12 CAL<br>15S<br>Yes<br>TX/Pbp/Tap Water |

| MOISTURE/DENSITY<br>DATA   | BEFORE<br>TEST | AFTER<br>TEST |        |
|----------------------------|----------------|---------------|--------|
| Wt. Soil + Moisture (g)    | 214.8          | 215.8         |        |
| Wt. Wet Soil & Pan (g)     | 223.0          | 223.9         |        |
| Wt. Dry Soil & Pan (g)     | 197.5          | 197.5         |        |
| Wt. Lost Moisture (g)      | 25.4           | 26.4          |        |
| Wt. of Pan Only (g)        | 8.1            | 8.1           |        |
| Wt. of Dry Soil (g)        | 189.4          | 189.4         |        |
| Moisture Content %         | 13.4           | 13.9          |        |
| Wet Density PCF            | 134.5          | 143.3         |        |
| Dry Density PCF            | 118.6          | 125.8         |        |
| Init. Diameter (in)        | 1.613          | (cm)          | 4.097  |
| Init. Area (sq in)         | 2.043          | (sq cm)       | 13.184 |
| Init. Height (in)          | 2.977          | (cm)          | 7.562  |
| Vol. Bef. Consol. (cu ft)  | 0.00352        |               |        |
| Vol. After Consol. (cu ft) | 0.00332        |               |        |
| Porosity %                 | 28.07          |               |        |

# FLOW PUMP CALCULATIONS

| Pump Setting                | 5        |
|-----------------------------|----------|
| Velocity CM/Sec             | 3.29E-05 |
| Q (cc/s)                    | 1.05E-06 |
| Height                      | 2.920    |
| Diameter                    | 1.582    |
| Pressure (psi)              | 2.510    |
| Area after consol. (cm*cm)  | 12.674   |
| Gradient                    | 23.794   |
| Permeability k (cm/s)       | 3.5E-09  |
| Permeability k (m/s)        | 3.5E-11  |
| Back Pressure (psi)         | 48.0     |
| Cell Pressure (psi)         | 69.6     |
| Ave. Effective Stress (psi) | 20.345   |

Average temperature degree C: 22.4 Notes: Sample diameter is less than specification for nominal particle size in sample.

| Data entry by:     |             | Date: |
|--------------------|-------------|-------|
| Checked by: Ctt    | Date: 10/12 | 2012  |
| FileName: LKP0A122 |             |       |

10/10/2012



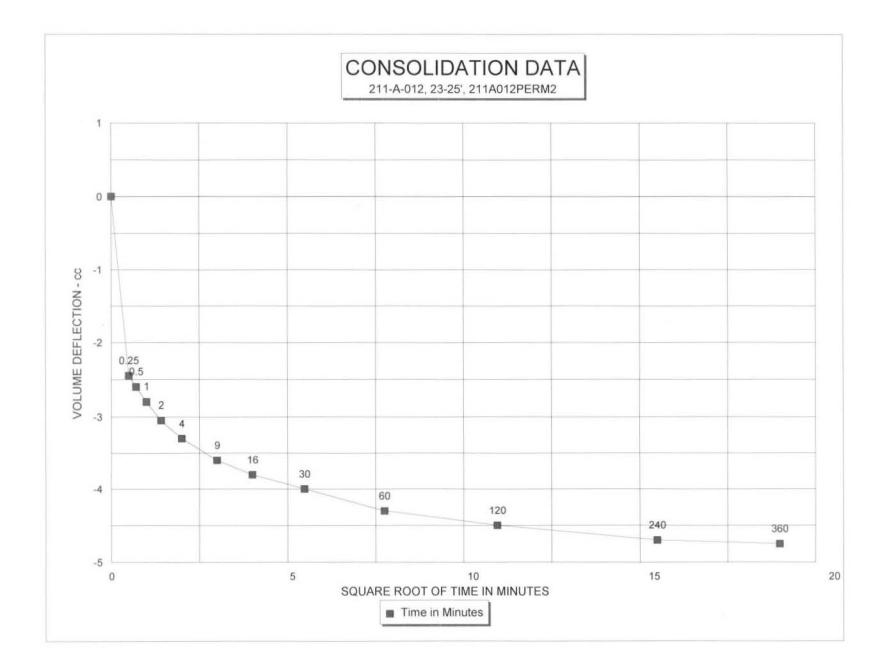
| CLIENT LATA En  | vironmental Service-Ky     | JOB NO. 2855-04 |                  |
|-----------------|----------------------------|-----------------|------------------|
| BORING NO.      | 211-A-012                  | SAMPLED         | 9/17/12          |
| DEPTH           | 23-25'                     | TEST STARTED    | 10/04/12 CAL     |
| SAMPLE NO.      | 211A012PERM2               | TEST FINISHED   | 10/09/12 CAL     |
| SOIL DESCR.     | ERI12-SW-SWMU211A          | SETUP NO.       | 15S              |
| LOCATION        | SW Plume RDSI Geotechnical | SATURATED TEST  | Yes              |
| CONF. PRES. PSF | 3105                       | TEST TYPE       | TX/Pbp/Tap Water |

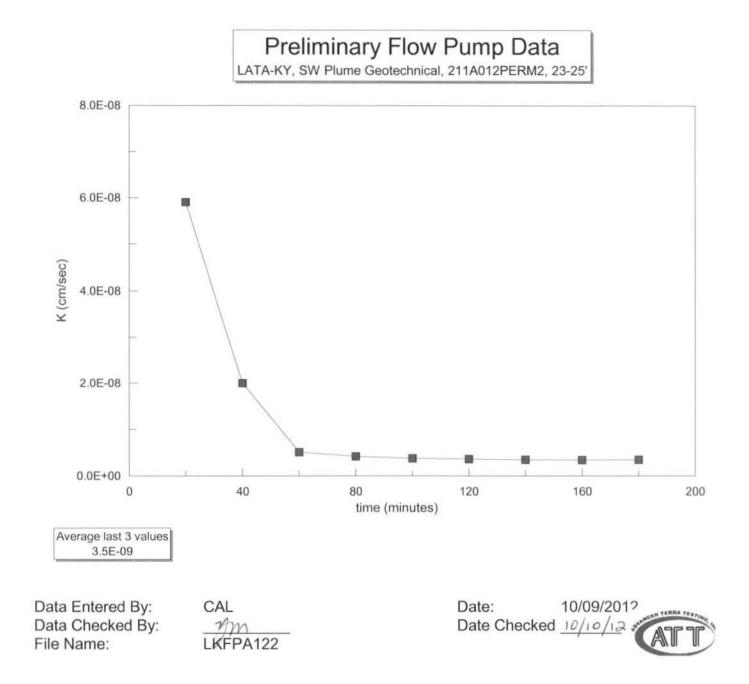
#### SATURATION DATA

| Cell<br>Pres.<br>(PSI) | Back<br>Pres.<br>(PSI) | Burette<br>Reading<br>(CC) |      | Pore<br>Pressure<br>(PSI) | C    | Change | В |      |
|------------------------|------------------------|----------------------------|------|---------------------------|------|--------|---|------|
|                        |                        | Close                      | Open | Close                     | Open |        |   |      |
| 40.0                   | 38.0                   | 1.8                        | 7.3  |                           |      |        |   |      |
| 50.0                   | 48.0                   | 9.5                        | 10.4 | 39.2                      | 48.5 | 9.3    |   | 0.93 |
| 60.0                   |                        | 11.4                       | 11.8 | 49.0                      | 58.7 | 9.7    |   | 0.97 |

## CONSOLIDATION DATA

| Elapsed                  | SQRT          | Burette        | Volume |       |
|--------------------------|---------------|----------------|--------|-------|
| Time                     | Time          | Reading        | Defl.  |       |
| (Min)                    | (Min)         | (CC)           | (cc)   |       |
| 0.00                     | 0.00          | 11.80          | 0.00   |       |
| 0.25                     | 0.50          | 14.25          | -2.45  |       |
| 0.5                      | 0.71          | 14.40          | -2.60  |       |
| 1                        | 1.00          | 14.60          | -2.80  |       |
| 2                        | 1.41          | 14.85          | -3.05  |       |
| 2 4                      | 2.00          | 15.10          | -3.30  |       |
| 9                        | 3.00          | 15.40          | -3.60  |       |
| 16                       | 4.00          | 15.60          | -3.80  |       |
| 30                       | 5.48          | 15.80          | -4.00  |       |
| 60                       | 7.75          | 16.10          | -4.30  |       |
| 120                      | 10.95         | 16.30          | -4.50  |       |
| 240                      | 15.49         | 16.50          | -4.70  |       |
| 360                      | 18.97         | 16.55          | -4.75  |       |
|                          |               |                |        |       |
| Initial Height (in)      | 2.977         | Init. Vol. (CC |        | 99.70 |
| Height Change (in)       | 0.057         | Vol. Change    | (CC)   | 15.20 |
| Ht. After Cons. (in)     | 2.920         | Cell Exp. (C   | C)     | 9.51  |
| Initial Area (sq in)     | 2.043         | Net Change     | (CC)   | 5.69  |
| Area After Cons. (sq in) | 1.964         | Cons. Vol. (   | CC)    | 94.02 |
|                          | Date:<br>2012 | 10/10/2012     |        | ATT T |





Client LATA EAN Services - KT Job No. 2755-09 Sample No. 21/A-0/A 2010/2 Alter 23-25' Project Sel Reme Geofechnical Sampled 1/17/12-by Prepped 10/22/ E. by \_\_\_\_\_ prepart # ERTD-SW-SWMU 21/A Tx/Pbp of 3105 psf LK2855/LKDPA122 10/10/12

| CLIENT                                                            | LATA Env        | ironmenetal Services -KY                                                                       | JOB NO. 2855-04                                                                        | 4                                                                          |
|-------------------------------------------------------------------|-----------------|------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------|----------------------------------------------------------------------------|
| BORING N<br>DEPTH<br>SAMPLE N<br>SOIL DES<br>LOCATION<br>CONF. PR | NO.<br>CR.<br>N | 211-A-012<br>38-40'<br>211A012PERM3<br>ERI12-SW-SWMU211A<br>SW Plume RDSI Geotechnical<br>5046 | SAMPLED<br>TEST STARTED<br>TEST FINISHED<br>CELL NUMBER<br>SATURATED TEST<br>TEST TYPE | 09/17/12<br>10/06/12 CAL<br>10/16/12 CAL<br>13S<br>Yes<br>TX/Pbp/Tap Water |

| MOISTURE/DENSITY           | BEFORE  | AFTER   |        |
|----------------------------|---------|---------|--------|
| DATA                       | TEST    | TEST    |        |
| Wt. Soil + Moisture (g)    | 197.8   | 194.4   |        |
| Wt. Wet Soil & Pan (g)     | 206.1   | 202.7   |        |
| Wt. Dry Soil & Pan (g)     | 164.4   | 164.4   |        |
| Wt. Lost Moisture (g)      | 41.8    | 38.3    |        |
| Wt. of Pan Only (g)        | 8.3     | 8.3     |        |
| Wt. of Dry Soil (g)        | 156.0   | 156.0   |        |
| Moisture Content %         | 26.8    | 24.6    |        |
| Wet Density PCF            | 123.0   | 124.1   |        |
| Dry Density PCF            | 97.0    | 99.6    |        |
| Init. Diameter (in)        | 1.620   | (cm)    | 4.115  |
| Init. Area (sq in)         | 2.061   | (sq cm) | 13.299 |
| Init. Height (in)          | 2.972   | (cm)    | 7.549  |
| Vol. Bef. Consol. (cu ft)  | 0.00355 |         |        |
| Vol. After Consol. (cu ft) | 0.00345 |         |        |
| Porosity %                 | 39.21   |         |        |
|                            |         |         |        |

#### FLOW PUMP CALCULATIONS

| Pump Setting                | 19       |
|-----------------------------|----------|
| Velocity CM/Sec             | 1.25E-04 |
| Q (cc/s)                    | 3.99E-06 |
| Height                      | 2.868    |
| Diameter                    | 1.627    |
| Pressure (psi)              | 4.100    |
| Area after consol. (cm*cm)  | 13.421   |
| Gradient                    | 39.571   |
| Permeability k (cm/s)       | 7.5E-09  |
| Permeability k (m/s)        | 7.5E-11  |
| Back Pressure (psi)         | 108.0    |
| Cell Pressure (psi)         | 143.0    |
| Ave. Effective Stress (psi) | 32.950   |
|                             |          |

Average temperature degree C:

| Data entry by:     | DAW    | Date:    |
|--------------------|--------|----------|
| Checked by:        | Date:_ | 10/18/12 |
| FileName: LKP00123 |        |          |

10/18/2012

22.7



| CLIENT LATA En  | vironmenetal Services -KY  | JOB NO. 2855-04 |                  |
|-----------------|----------------------------|-----------------|------------------|
| BORING NO.      | 211-A-012                  | SAMPLED         | 09/17/12         |
| DEPTH           | 38-40'                     | TEST STARTED    | 10/06/12 CAL     |
| SAMPLE NO.      | 211A012PERM3               | TEST FINISHED   | 10/16/12 CAL     |
| SOIL DESCR.     | ERI12-SW-SWMU211A          | SETUP NO.       | 13S              |
| LOCATION        | SW Plume RDSI Geotechnical | SATURATED TEST  | Yes              |
| CONF. PRES. PSF | 5046                       | TEST TYPE       | TX/Pbp/Tap Water |

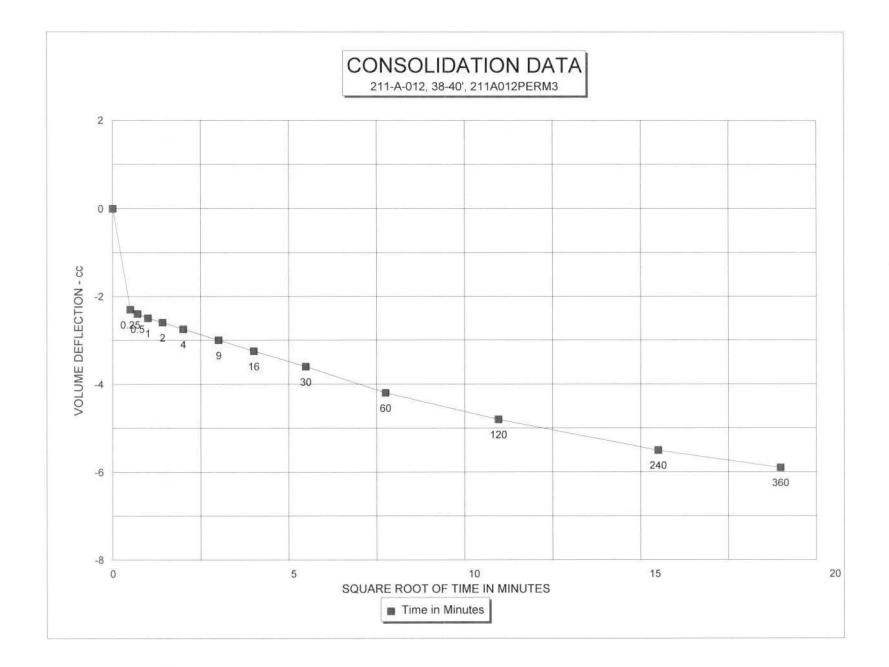
#### SATURATION DATA

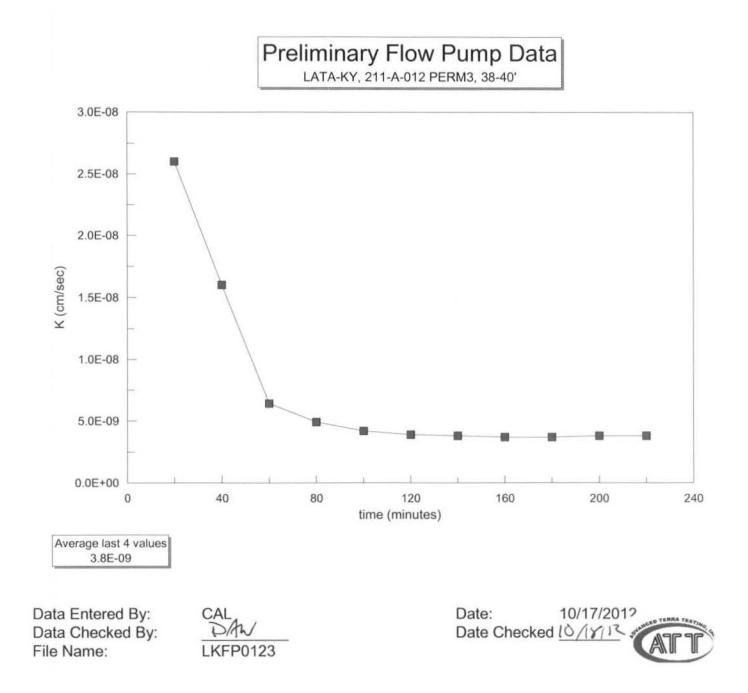
| Cell<br>Pres.<br>(PSI) | Back<br>Pres.<br>(PSI) | Burette<br>Reading<br>(CC) |            | Pore<br>Pressure<br>(PSI) |               | Change | В                     |
|------------------------|------------------------|----------------------------|------------|---------------------------|---------------|--------|-----------------------|
|                        |                        | Close                      | Open       | Close                     | Open          |        |                       |
| 40.0                   | 38.0                   | 1.1                        | 6.5        |                           |               |        |                       |
| 50.0                   | 48.0                   | 7.4                        | 8.2        | 39.0                      | 47.3          | 8.3    | 0.83                  |
| 60.0                   | 58.0                   | 8.0                        | 8.7        | 49.0                      | 57.9          | 8.9    | 0.89                  |
| 70.0                   | 68.0                   | 8.9                        | 9.6        | 58.9                      | 67.3          | 8.4    | 0.84                  |
| 80.0                   | 78.0                   | 9.7                        | 10.4       | 68.9                      | 77.7          | 8.8    | 0.88                  |
| 90.0                   | 88.0                   | 10.7                       | 11.4       | 79.0                      | 88.0          | 9.0    | 0.90                  |
| 100.0                  | 98.0                   | 11.5                       | 12.1       | 88.9                      | 98.1          | 9.2    | 0.92                  |
| 110.0                  | 108.0                  | 12.5                       | -          | 98.8                      | 108.0         | 9.2    | 0.92                  |
| 120.0                  |                        | 13.1                       | 13.1       | 108.4                     | 117.9         | 9.5    | 0.95                  |
|                        |                        | CONSC                      | LIDATION D | ATA                       |               |        |                       |
|                        |                        | Elapsed                    | SQRT       |                           | Burette       | Volume |                       |
|                        |                        | Time                       | Time       |                           | Reading       | Defl.  |                       |
|                        |                        | (Min)                      | (Min)      |                           | (CC)          | (cc)   |                       |
|                        |                        | 0.00                       | 0.00       |                           | 0.30          | 0.00   |                       |
|                        |                        | 0.25                       | 0.50       |                           | 2.60          | -2.30  |                       |
|                        |                        | 0.5                        | 0.71       |                           | 2.70          | -2.40  |                       |
|                        |                        | 1                          | 1.00       |                           | 2.80          | -2.50  |                       |
|                        |                        | 2                          | 1.41       |                           | 2.90          | -2.60  |                       |
|                        |                        | 4                          | 2.00       |                           | 3.05          | -2.75  |                       |
|                        |                        | 9                          | 3.00       |                           | 3.30          | -3.00  |                       |
|                        |                        | 16                         | 4.00       |                           | 3.55          | -3.25  |                       |
|                        |                        | 30                         | 5.48       |                           | 3.90          | -3.60  |                       |
|                        |                        | 60                         | 7.75       |                           | 4.50          | -4.20  |                       |
|                        |                        | 120                        | 10.95      |                           | 5.10          | -4.80  |                       |
|                        |                        | 240                        | 15.49      |                           | 5.80          | -5.50  |                       |
|                        |                        | 360                        | 18.97      |                           | 6.20          | -5.90  |                       |
|                        |                        |                            |            |                           | The same as a |        |                       |
| Initial Height         | (in)                   |                            | 2.972      |                           | Init. Vol. (C |        | 100.40                |
| Height Chang           |                        |                            | 0.104      |                           | Vol. Change   |        | 18.80                 |
| Ht. After Cons         |                        |                            | 2.868      |                           | Cell Exp. (   |        | 16.19                 |
| Initial Area           | (sq in)                |                            | 2.061      |                           | Net Change    |        | 2.61                  |
| Area After Co          | ins. (sq in)           | Y                          | 2.080      |                           | Cons. Vol.    | (CC)   | 97.79                 |
| Data                   |                        | DAIA                       | Data       | 10/10/00 10               |               |        | SHANCED TERRA TESTINO |
| Data entry by          |                        | DAW                        | Date:      | 10/18/2012                |               |        |                       |

| Data entry by:     | DAW   | Date:  |
|--------------------|-------|--------|
| Checked by: 04c    | Date: | 118/12 |
| FileName: LKP00123 |       | /      |

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| and a second of the                                                                 |
|-------------------------------------------------------------------------------------|
| Client LATA GAULADAMENTAL SCANCES - Ky<br>Job No. 2855-04                           |
| Sample No. 2114-012 @ 38-90'<br>211A 012 F EAM 3                                    |
| Project SW Plume RDSI Gestechnical<br>Sampled 9/17/12 by<br>Prepped 10/06/12 by CAL |
| Tx/Pbp 53 35psi                                                                     |
| LK2855/LKDP0123<br>10/18/12                                                         |

| CLIENT                                                                | LATA Envi | ronmental Services - KY                                                                        | JOB NO.                                                             | 2855-04                         |                                                                            |
|-----------------------------------------------------------------------|-----------|------------------------------------------------------------------------------------------------|---------------------------------------------------------------------|---------------------------------|----------------------------------------------------------------------------|
| BORING NO<br>DEPTH<br>SAMPLE NO<br>SOIL DESC<br>LOCATION<br>CONF. PRE | O.<br>CR. | 211-A-027<br>10-12'<br>211A027PERM1<br>ERI12-SW-SWMU211A<br>SW Plume RDSI Geotechnical<br>1423 | SAMPLED<br>TEST STA<br>TEST FINI<br>CELL NUM<br>SATURAT<br>TEST TYP | RTED<br>SHED<br>1BER<br>ED TEST | 09/18/12<br>10/04/12 CAL<br>10/11/12 CAL<br>14S<br>Yes<br>TX/Pbp/Tap Water |

| MOISTURE/DENSITY<br>DATA   | BEFORE<br>TEST | AFTER<br>TEST |        |
|----------------------------|----------------|---------------|--------|
| Wt. Soil + Moisture (g)    | 192.6          | 189.8         |        |
| Wt. Wet Soil & Pan (g)     | 200.8          | 198.0         |        |
| Wt. Dry Soil & Pan (g)     | 165.3          | 165.3         |        |
| Wt. Lost Moisture (g)      | 35.5           | 32.7          |        |
| Wt. of Pan Only (g)        | 8.2            | 8.2           |        |
| Wt. of Dry Soil (g)        | 157.1          | 157.1         |        |
| Moisture Content %         | 22.6           | 20.8          |        |
| Wet Density PCF            | 127.7          | 128.1         |        |
| Dry Density PCF            | 104.2          | 106.0         |        |
| Init. Diameter (in)        | 1.564          | (cm)          | 3.973  |
| Init. Area (sq in)         | 1.921          | (sq cm)       | 12.395 |
| Init. Height (in)          | 2.991          | (cm)          | 7.597  |
| Vol. Bef. Consol. (cu ft)  | 0.00333        |               |        |
| Vol. After Consol. (cu ft) | 0.00327        |               |        |
| Porosity %                 | 35.31          |               |        |

#### FLOW PUMP CALCULATIONS

| Pump Setting                  | 15       |
|-------------------------------|----------|
| Velocity CM/Sec               | 9.85E-05 |
| Q (cc/s)                      | 3.15E-06 |
| Height                        | 2.956    |
| Diameter                      | 1.559    |
| Pressure (psi)                | 1.403    |
| Area after consol. (cm*cm)    | 12.321   |
| Gradient                      | 13.138   |
| Permeability k (cm/s)         | 1.9E-08  |
| Permeability k (m/s)          | 1.9E-10  |
| Back Pressure (psi)           | 68.0     |
| Cell Pressure (psi)           | 77.9     |
| Ave. Effective Stress (psi)   | 9.199    |
| Average temperature degree C: | 22.3     |

| Data entry by:     | DAW       | Date: | 10/12/2012 |
|--------------------|-----------|-------|------------|
| Checked by:        | Date: 10- | 12-12 |            |
| FileName: LKP00271 |           |       |            |



| CLIENT LATA     | Environmental Services - KY | JOB NO. 2855-04 |                  |
|-----------------|-----------------------------|-----------------|------------------|
| BORING NO.      | 211-A-027                   | SAMPLED         | 09/18/12         |
| DEPTH           | 10-12'                      | TEST STARTED    | 10/04/12 CAL     |
| SAMPLE NO.      | 211A027PERM1                | TEST FINISHED   | 10/11/12 CAL     |
| SOIL DESCR.     | ERI12-SW-SWMU211A           | SETUP NO.       | 14S              |
| LOCATION        | SW Plume RDSI Geotechnical  | SATURATED TEST  | Yes              |
| CONF. PRES. PSF | 1423                        | TEST TYPE       | TX/Pbp/Tap Water |

#### SATURATION DATA

| Cell<br>Pres.<br>(PSI) | Back<br>Pres.<br>(PSI) | Burette<br>Reading<br>(CC) |      | Pore<br>Pressure<br>(PSI) | C    | Change | В |      |
|------------------------|------------------------|----------------------------|------|---------------------------|------|--------|---|------|
|                        |                        | Close                      | Open | Close                     | Open |        |   |      |
| 40.0                   | 38.0                   | 2.2                        | 8.1  |                           |      |        |   |      |
| 50.0                   | 48.0                   | 10.6                       | 11.4 | 38.8                      | 46.8 | 8.0    |   | 0.80 |
| 60.0                   | 58.0                   | 11.7                       | 12.5 | 48.9                      | 57.8 | 8.9    |   | 0.89 |
| 70.0                   | 68.0                   | 12.4                       | 13.1 | 58.7                      | 68.1 | 9.4    |   | 0.94 |
| 80.0                   |                        | 13.5                       | 13.8 | 68.6                      | 78.1 | 9.5    |   | 0.95 |

# CONSOLIDATION DATA

|                          | Elapsed<br>Time<br>(Min) | SQRT<br>Time<br>(Min) | Burette<br>Reading<br>(CC) | Volume<br>Defl.<br>(cc) |  |
|--------------------------|--------------------------|-----------------------|----------------------------|-------------------------|--|
|                          | (IVIIII)                 | (MIII)                | (00)                       | (00)                    |  |
|                          | 0.00                     | 0.00                  | 0.20                       | 0.00                    |  |
|                          | 0.25                     | 0.50                  | 0.85                       | -0.65                   |  |
|                          | 0.5                      | 0.71                  | 0.85                       | -0.65                   |  |
|                          | 1                        | 1.00                  | 0.90                       | -0.70                   |  |
|                          | 2                        | 1.41                  | 0.90                       | -0.70                   |  |
|                          | 4<br>9                   | 2.00                  | 1.00                       | -0.80                   |  |
|                          | 9                        | 3.00                  | 1.10                       | -0.90                   |  |
|                          | 16                       | 4.00                  | 1.25                       | -1.05                   |  |
|                          | 30                       | 5.48                  | 1.45                       | -1.25                   |  |
|                          | 60                       | 7.75                  | 1.75                       | -1.55                   |  |
|                          | 120                      | 10.95                 | 2.10                       | -1.90                   |  |
|                          | 240                      | 15.49                 | 2.50                       | -2.30                   |  |
|                          | 360                      | 18.97                 | 2.60                       | -2.40                   |  |
| Initial Height (in)      |                          | 2.991                 | Init. Vol. (CC             | 2)                      |  |
| Height Change (in)       |                          | 0.035                 | Vol. Change                | (CC)                    |  |
| Ht. After Cons. (in)     |                          | 2.956                 | Cell Exp. (C               |                         |  |
| Initial Area (sq in)     |                          | 1.921                 | Net Change                 | (CC)                    |  |
| Area After Cons. (sq in) |                          | 1.910                 | Cons. Vol. (               | CC)                     |  |
| (3) (3)                  |                          |                       |                            |                         |  |

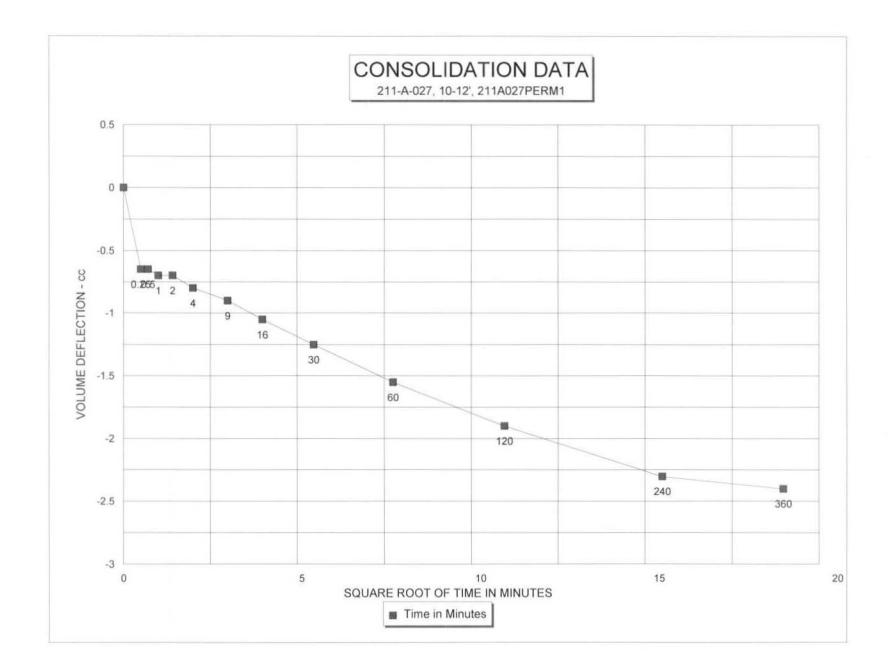
| Data entry by:     | DAW   | Date:    |
|--------------------|-------|----------|
| Checked by: are    | Date: | 10-12-12 |
| FileName: LKP00271 |       |          |

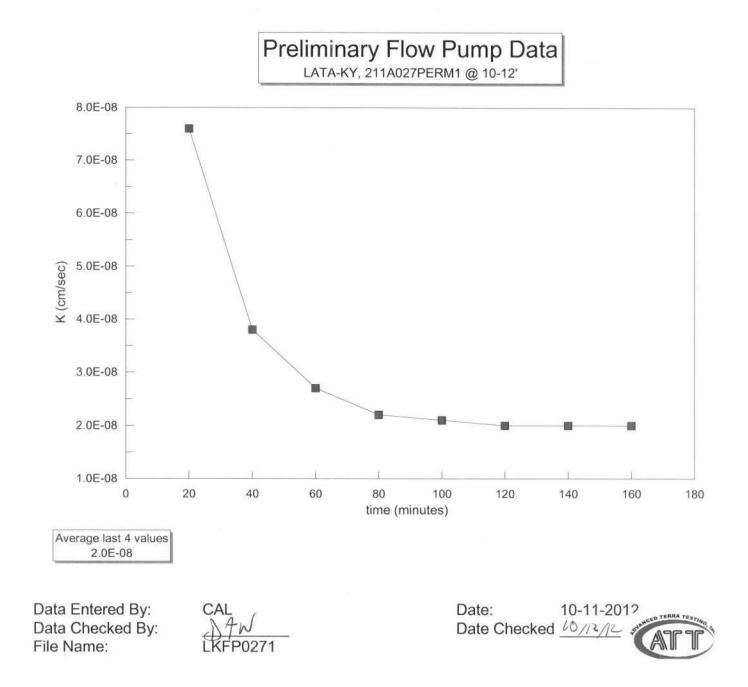
10/12/2012



94.18 14.40 12.75

1.65 92.53





Client LATA Environmental Services - Ky Job No. 2855 -04 Sample No. 211-4 -027 211 A 027 PERMI @ 10-12 Project SW Plume RDST Gertechnical Sampled 9 / 18/12 by\_ Prepped 10 / 4 /12 by care TX/Pop 03 9.9 psi LK2855/LKDP1012 10/12/12

| CLIENT LATA En                                                                  | vironmental Services - KY                                                                          | JOB NO. 2855-04                                                                        |                                                                |
|---------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------|----------------------------------------------------------------|
| BORING NO.<br>DEPTH<br>SAMPLE NO.<br>SOIL DESCR.<br>LOCATION<br>CONF. PRES. PSF | 211-A-027<br>22.5-24.5'<br>211A027PERM2<br>ERI12-SW-SWMU211A<br>SW Plume RDSI Geotechnical<br>2911 | SAMPLED<br>TEST STARTED<br>TEST FINISHED<br>CELL NUMBER<br>SATURATED TEST<br>TEST TYPE | 10/10/12 CAL<br>10/15/12 DPM<br>15S<br>Yes<br>TX/Pbp/Tap Water |

| MOISTURE/DENSITY           | BEFORE  | AFTER   |        |
|----------------------------|---------|---------|--------|
| DATA                       | TEST    | TEST    |        |
| Wt. Soil + Moisture (g)    | 249.3   | 252.1   |        |
| Wt. Wet Soil & Pan (g)     | 255.9   | 258.7   |        |
| Wt. Dry Soil & Pan (g)     | 228.6   | 228.6   |        |
| Wt. Lost Moisture (g)      | 27.3    | 30.1    |        |
| Wt. of Pan Only (g)        | 6.6     | 6.6     |        |
| Wt. of Dry Soil (g)        | 222.0   | 222.0   |        |
| Moisture Content %         | 12.3    | 13.6    |        |
| Wet Density PCF            | 136.1   | 139.8   |        |
| Dry Density PCF            | 121.2   | 123.1   |        |
| Init. Diameter (in)        | 1.663   | (cm)    | 4.224  |
| Init. Area (sq in)         | 2.172   | (sq cm) | 14.014 |
| Init. Height (in)          | 3.212   | (cm)    | 8.158  |
| Vol. Bef. Consol. (cu ft)  | 0.00404 |         |        |
| Vol. After Consol. (cu ft) | 0.00397 |         |        |
| Porosity %                 | 26.75   |         |        |

#### FLOW PUMP CALCULATIONS

| Pump Setting                  | 5        |
|-------------------------------|----------|
| Velocity CM/Sec               | 3.29E-05 |
| Q (cc/s)                      | 1.05E-06 |
| Height                        | 3.181    |
| Diameter                      | 1.658    |
| Pressure (psi)                | 2.260    |
| Area after consol. (cm*cm)    | 13.929   |
| Gradient                      | 19.666   |
| Permeability k (cm/s)         | 3.8E-09  |
| Permeability k (m/s)          | 3.8E-11  |
| Back Pressure (psi)           | 58.0     |
| Cell Pressure (psi)           | 78.2     |
| Ave. Effective Stress (psi)   | 19.070   |
| Average temperature degree C: | 22.4     |

| Data entry by:     | DAW       | Date: | 10/16/2012 |
|--------------------|-----------|-------|------------|
| Checked by:        | Date: 10/ | 16/12 |            |
| FileName: LKP027P2 | 1         | /     |            |



| BORING NO.      | 211-A-027                  | SAMPLED        |                  |
|-----------------|----------------------------|----------------|------------------|
| DEPTH           | 22.5-24.5'                 | TEST STARTED   | 10/10/12 CAL     |
| SAMPLE NO.      | 211A027PERM2               | TEST FINISHED  | 10/15/12 DPM     |
| SOIL DESCR.     | ERI12-SW-SWMU211A          | SETUP NO.      | 15S              |
| LOCATION        | SW Plume RDSI Geotechnical | SATURATED TEST | Yes              |
| CONF. PRES. PSF | 2911                       | TEST TYPE      | TX/Pbp/Tap Water |

JOB NO. 2855-04

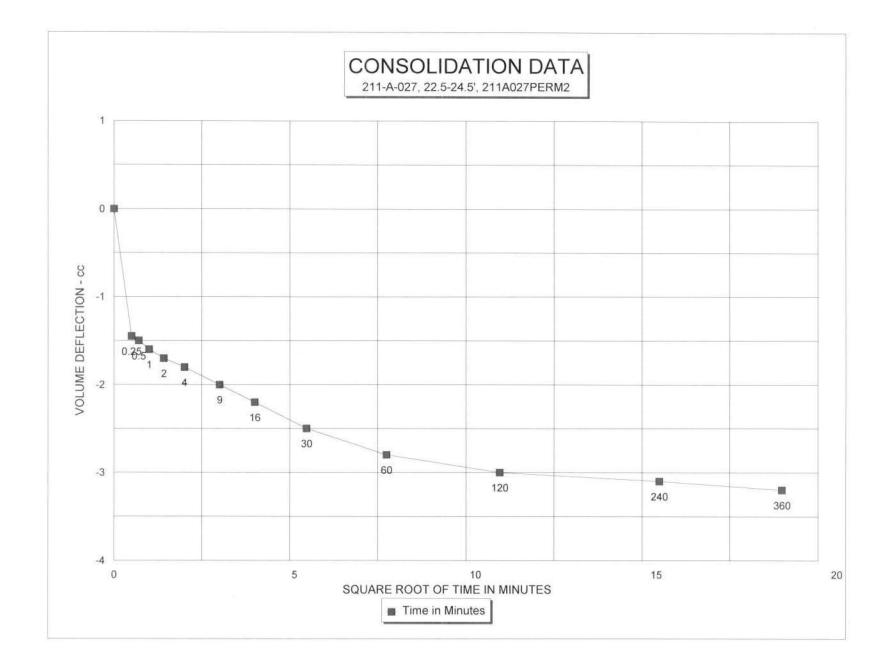
#### SATURATION DATA

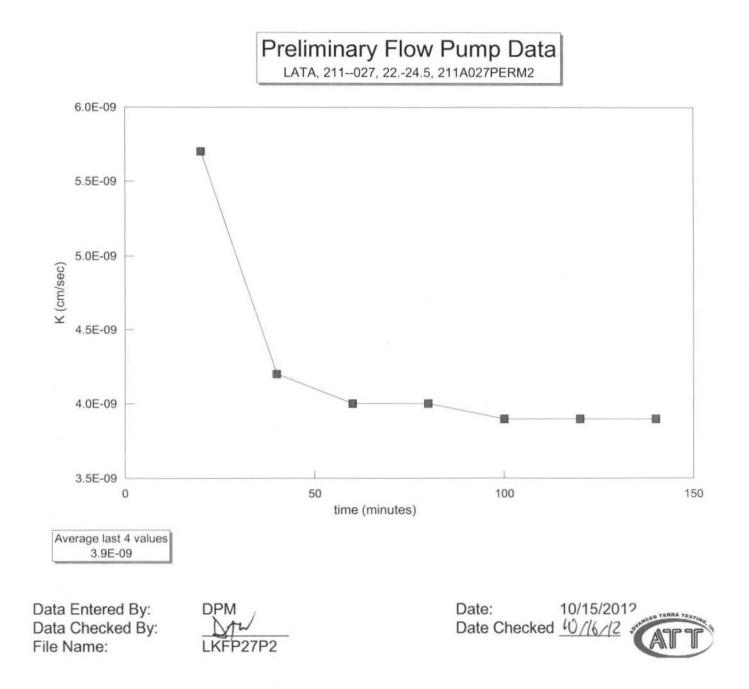
CLIENT LATA Environmental Services - KY

| Cell<br>Pres.<br>(PSI) | Back<br>Pres.<br>(PSI) | Burette<br>Reading<br>(CC) |      | Pore<br>Pressure<br>(PSI) | (    | Change | В |      |
|------------------------|------------------------|----------------------------|------|---------------------------|------|--------|---|------|
| 10.0                   | 22.0                   | Close                      | Open | Close                     | Open |        |   |      |
| 40.0                   | 38.0                   | 1.7                        | 7.7  |                           |      |        |   |      |
| 50.0                   | 48.0                   | 7.7                        | 8.7  | 39.1                      | 47.6 | 8.5    |   | 0.85 |
| 60.0                   | 58.0                   | 8.9                        | 9.7  | 49.2                      | 58.2 | 9.0    |   | 0.90 |
| 70.0                   |                        | 9.8                        | 10.0 | 59.1                      | 68.6 | 9.5    |   | 0.95 |

# CONSOLIDATION DATA

| Elapsed<br>Time            | SQRT<br>Time | Burette<br>Reading | Volume<br>Defl. |              |
|----------------------------|--------------|--------------------|-----------------|--------------|
| (Min)                      | (Min)        | (CC)               | (cc)            |              |
| 0.00                       | 0.00         | 10.00              | 0.00            |              |
| 0.25                       | 5 0.50       | 11.45              | -1.45           |              |
| 0.5                        |              | 11.50              | -1.50           |              |
| 1                          | 1.00         | 11.60              | -1.60           |              |
| 2                          | 2 1.41       | 11.70              | -1.70           |              |
| 4                          | 2.00         | 11.80              | -1.80           |              |
| 9                          | 3.00         | 12.00              | -2.00           |              |
| 16                         |              | 12.20              | -2.20           |              |
| 30                         |              | 12.50              | -2.50           |              |
| 60                         | 7.75         | 12.80              | -2.80           |              |
| 120                        | 10.95        | 13.00              | -3.00           |              |
| 240                        | 15.49        | 13.10              | -3.10           |              |
| 360                        | 18.97        | 13.20              | -3.20           |              |
| Lawsell Lawsell Max        | 0.040        |                    |                 |              |
| Initial Height (in)        | 3.212        | Init. Vol. (CC     |                 | 114.35       |
| Height Change (in)         | 0.031        | Vol. Change        |                 | 12.10        |
| Ht. After Cons. (in)       | 3.181        | Cell Exp. (C       |                 | 10.32        |
| Initial Area (sq in)       | 2.172        | Net Change         |                 | 1.78         |
| Area After Cons. (sq in)   | 2.159        | Cons. Vol. (       |                 | 112.56       |
| Data entry by: DAW         | Date:        | 10/16/2012         | Suran           | MALA LESTINO |
| Checked by: On Date: 10/16 | 12           |                    |                 |              |
| FileName: LKP027P2         |              |                    |                 |              |
|                            |              | E (0               |                 |              |





1.3 Client LATA Environmtal-ky Job No. 2855-04 BoringNo. 2/1-A-027 Depth 22.5-27.5' Sample No. 2 /1 A027 /ERM 2 Project SW Plume RPSI Goo. Sampled / / by\_ Prepped / / by Project No. EAI12-SW-SWM41211A Tx/Pbp O3 = 2911 ps P LK2855/LKDP27P2 10/16/12

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| CLIENT LATA En                                                                  | vironmental Services - KY                                                                 | JOB NO. 2855-02                                                                        |                                                                              |
|---------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------|------------------------------------------------------------------------------|
| BORING NO.<br>DEPTH<br>SAMPLE NO.<br>SOIL DESCR.<br>LOCATION<br>CONF. PRES. PSF | MW513<br>10-12'<br>MW513 PERM1<br>ERI12-SW-SWMU211A<br>SW Plume RDSI Geotechnical<br>1423 | SAMPLED<br>TEST STARTED<br>TEST FINISHED<br>CELL NUMBER<br>SATURATED TEST<br>TEST TYPE | 08/27/12 KD<br>9/15/12 CAL<br>9/24/12 DPM<br>15S<br>Yes<br>TX/Pbp/Tap Water. |
|                                                                                 | BEFORE AFTER                                                                              |                                                                                        |                                                                              |

| DATA                       | TEST    | TEST    |        |
|----------------------------|---------|---------|--------|
|                            |         |         |        |
| Wt. Soil + Moisture (g)    | 649.7   | 647.0   |        |
| Wt. Wet Soil & Pan (g)     | 664.0   | 661.3   |        |
| Wt. Dry Soil & Pan (g)     | 541.0   | 541.0   |        |
| Wt. Lost Moisture (g)      | 122.9   | 120.2   |        |
| Wt. of Pan Only (g)        | 14.2    | 14.2    |        |
| Wt. of Dry Soil (g)        | 526.8   | 526.8   |        |
| Moisture Content %         | 23.3    | 22.8    |        |
| Wet Density PCF            | 127.0   | 129.8   |        |
| Dry Density PCF            | 103.0   | 105.7   |        |
|                            |         |         |        |
| Init. Diameter (in)        | 2.839   | (cm)    | 7.211  |
| Init. Area (sq іп)         | 6.330   | (sq cm) | 40.843 |
| Init. Height (in)          | 3.078   | (cm)    | 7.818  |
| Vol. Bef. Consol. (cu ft)  | 0.01128 |         |        |
| Vol. After Consol. (cu ft) | 0.01099 |         |        |
| Porosity %                 | 38.64   |         |        |

#### FLOW PUMP CALCULATIONS

| Pump Setting (gear number)<br>Percentage of Pump setting<br>Q (cc/s)<br>Height<br>Diameter<br>Pressure (psi)<br>Area after consol. (cm*cm)<br>Gradient<br>Permeability k (cm/s)<br>Permeability k (m/s) | 11<br>100<br>5.71E-05<br>3.052<br>2.814<br>0.429<br>40.129<br>3.891<br>3.7E-07<br><b>3.7E-09</b> |
|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------|
| Permeability k (m/s)<br>Back Pressure (psi)                                                                                                                                                             | 3.7E-09<br>38.0                                                                                  |
| Cell Pressure (psi)                                                                                                                                                                                     | 47.9                                                                                             |
| Ave. Effective Stress (psi)                                                                                                                                                                             | 9.686                                                                                            |
| Average temperature degree C:                                                                                                                                                                           | 22.5                                                                                             |

|  | <br> |  |
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|  |      |  |
|  |      |  |

| Data entry by:     | DAW Date:            |
|--------------------|----------------------|
| Checked by: 04     | Date: <u>9/26/12</u> |
| FileName: LKP05131 |                      |

09/25/2012



JOB NO. 2855-02

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# SATURATION DATA

CLIENT LATA Environmental Services - KY

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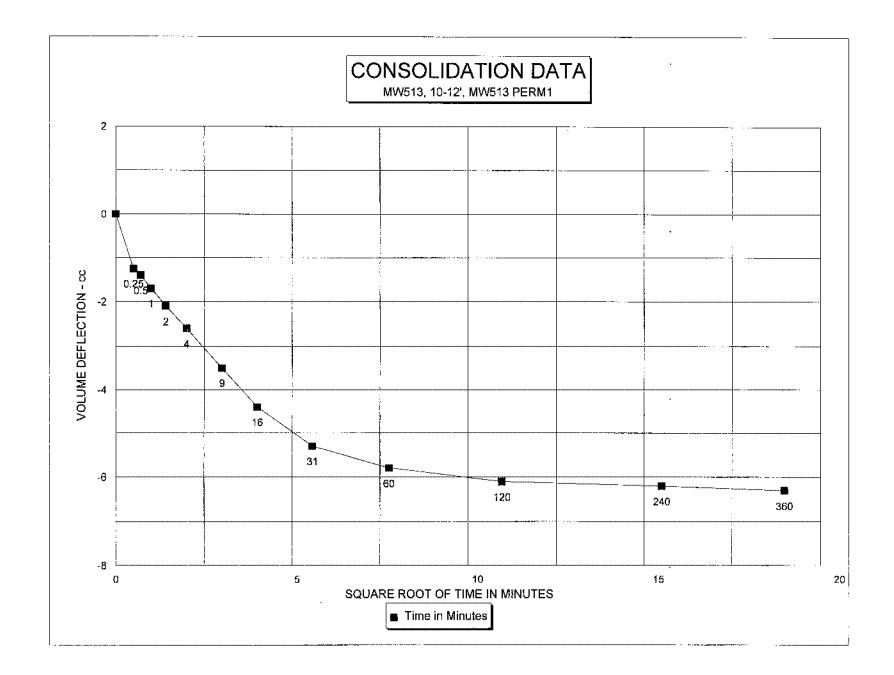
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| Cell<br>Pres.<br>(PSI) | Back<br>Pres.<br>(PSI) | Burette<br>Reading<br>(CC) |              | Pore<br>Pressure<br>(PSI) | 1    | Change | в |      |  |
|------------------------|------------------------|----------------------------|--------------|---------------------------|------|--------|---|------|--|
| 40.0                   | 38.0                   | Close<br>3.7               | Open<br>10.7 | Close                     | Open |        |   |      |  |
| 50.0                   | 00.0                   | 11.7                       | 12.0         | 39.1                      | 49.1 | 10.0   |   | 1.00 |  |

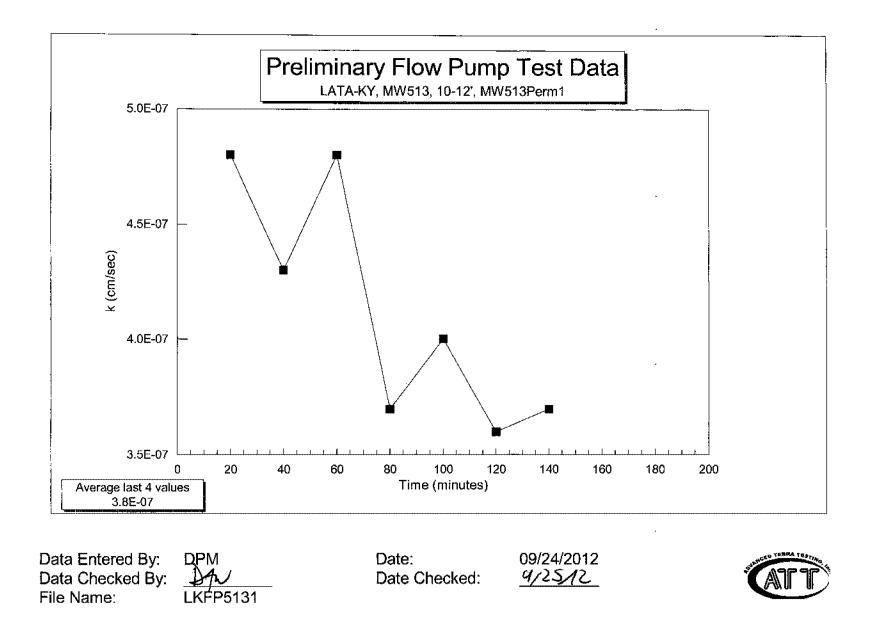
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#### CONSOLIDATION DATA

|                          | Elapsed       | SQRT          |            | Burette        | Volume |                     |
|--------------------------|---------------|---------------|------------|----------------|--------|---------------------|
|                          | Time          | Time          |            | Reading        | Defl.  |                     |
|                          | (Min)         | (Min)         |            | (CC)           | (cc)   |                     |
|                          | 0.00          | 0.00          |            | 12.10          | 0.00   |                     |
|                          | 0.25          | 0.50          |            | 13.35          | -1.25  |                     |
|                          | 0.25          | 0.50          |            | 13.50          | -1.40  |                     |
|                          |               |               |            |                |        |                     |
|                          | 1             | 1.00          |            | 13.80          | -1.70  |                     |
|                          | 2             | 1.41          |            | 14.20          | -2.10  |                     |
|                          | 4             | 2.00          |            | 14.70          | -2.60  |                     |
|                          | 9             | 3.00          |            | 15.60          | -3.50  |                     |
|                          | 16            | 4.00          |            | 16.50          | -4.40  |                     |
|                          | 31            | 5.57          |            | 17.40          | -5.30  |                     |
|                          | 60            | 7.75          |            | 17.90          | -5.80  |                     |
|                          | 120           | 10.95         |            | 18.20          | -6.10  |                     |
|                          | 240           | 15.49         |            | 18.30          | -6.20  |                     |
|                          | 360           | 18.97         |            | 18.40          | -6.30  |                     |
|                          |               |               |            |                |        |                     |
| Initial Height (in)      |               | 3.078         |            | Init. Vol. (CC | 2)     | 319.35              |
| Height Change (in)       |               | 0.026         |            | Vol. Change    | (CC)   | 15.70               |
| Ht. After Cons. (in)     |               | 3.052         |            | Cell Exp. (C   |        | 7.49                |
| Initial Area (sq in)     |               | 6.330         |            | Net Change     |        | 8.21                |
| Area After Cons. (sq in) |               | 6.220         |            | Cons. Vol. (   |        | 311.14              |
|                          |               | 0. <b>220</b> |            | 00110. 101. (  | 00,    | ANCED TERRA TESTINO |
| Data entry by:           | DAW D         | late:         | 09/25/2012 |                |        |                     |
| Checked by: Ott          | Date: 9/26/12 |               |            |                |        |                     |
| FileName: LKP05131       | - Herelie     | £             |            |                |        |                     |
| Thermanie. LIVE 00101    |               |               |            |                |        |                     |



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| CLIENT                                                                | LATA Envi | ronmental Services-Ky                                                                    | JOB NO.                                                                 | 2855-02                |                                                                            |
|-----------------------------------------------------------------------|-----------|------------------------------------------------------------------------------------------|-------------------------------------------------------------------------|------------------------|----------------------------------------------------------------------------|
| BORING NO<br>DEPTH<br>SAMPLE NO<br>PROJECT N<br>LOCATION<br>CONF. PRE | D,<br>∳O. | MW513<br>20-21'<br>MW513Perm2<br>ERI12-SW-SWMU211A<br>SW Plume RDSI Geotechnical<br>3299 | SAMPLED<br>TEST STAI<br>TEST FINIS<br>CELL NUM<br>SATURATE<br>TEST TYPI | SHED<br>BER<br>ED TEST | 8/27/12 KD<br>9/15/12 CAL<br>9/29/12 CAL<br>11P<br>Yes<br>TX/Pbp/Tap Water |

| MOISTURE/DENSITY           | BEFORE  | AFTER   |        |
|----------------------------|---------|---------|--------|
| DATA                       | TEST    | TEST    |        |
| Wt. Soil + Moisture (g)    | 677.3   | 686.4   |        |
| Wt. Wet Soil & Pan (g)     | 692.8   | 701.9   |        |
| Wt. Dry Soil & Pan (g)     | 590.0   | 590.0   |        |
| Wt. Lost Moisture (g)      | 102.8   | 112.0   |        |
| Wt. of Pan Only (g)        | 15.5    | 15.5    |        |
| Wt. of Dry Soil (g)        | 574.5   | 574.5   |        |
| Moisture Content %         | 17.9    | 19.5    |        |
| Wet Density PCF            | 133.0   | 146.4   |        |
| Dry Density PCF            | 112.8   | 122.5   |        |
| Init. Diameter (in)        | 2.830   | (cm)    | 7.188  |
| init. Area (sq in)         | 6.290   | (sq cm) | 40.584 |
| init. Height (in)          | 3.085   | (cm)    | 7.836  |
| Vol. Bef. Consol. (cu ft)  | 0.01123 |         |        |
| Vol. After Consol. (cu ft) | 0.01034 |         |        |
| Porosity %                 | 38.24   |         |        |

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#### FLOW PUMP CALCULATIONS

| Pump Setting<br>Velocity CM/Sec<br>Q (cc/s) | 5<br>3.29E-05<br>1.05E-06 |
|---------------------------------------------|---------------------------|
| Height                                      | 3.051                     |
| Diameter                                    | 2.730                     |
| Pressure (psi)                              | 5.490                     |
| Area after consol. (cm*cm)                  | 37.769                    |
| Gradient                                    | 49.808                    |
| Permeability k (cm/s)                       | 5.6E-10                   |
| Permeability k (m/s)                        | 5.6E-12                   |
| Back Pressure (psi)                         | 0.88                      |
| Cell Pressure (psi)                         | 111.0                     |
| Ave. Effective Stress (psi)                 | 20.255                    |
| Average temperature degree C:               | 23.4                      |

| Data entry by:     |        | Date:    |
|--------------------|--------|----------|
| Checked by: 041_   | Date:_ | 10/02/12 |
| FileName: LKP05132 |        |          |

10/01/2012



| BORING NO.<br>DEPTH<br>SAMPLE NO.<br>PROJECT NO.<br>LOCATION | MW513<br>20-21'<br>MW513Perm2<br>ERI12-SW-SWMU211A<br>SW Plume RDS/ Geotechnical | SAMPLED<br>TEST STARTED<br>TEST FINISHED<br>SETUP NO.<br>SATURATED TEST | 8/27/12 KD<br>9/15/12 CAL<br>9/29/12 CAL<br>11P<br>Yes<br>TX/9ba/Cap Water |
|--------------------------------------------------------------|----------------------------------------------------------------------------------|-------------------------------------------------------------------------|----------------------------------------------------------------------------|
| CONF. PRES. PSF                                              | .3299                                                                            | . TEST TYPE                                                             | TX/Pbp/Tap Water                                                           |

JOB NO. 2855-02

#### SATURATION DATA

CLIENT LATA Environmental Services-Ky

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| Cell<br>Pres.<br>(PSI) | Back<br>Pres.<br>(PSI) | Burette<br>Reading<br>(CC) |      | Pore<br>Pressure<br>(PSI) | C    | Change | в |      |
|------------------------|------------------------|----------------------------|------|---------------------------|------|--------|---|------|
|                        | • •                    | Close                      | Open | Close                     | Open | Ť      |   |      |
| 40.0                   | 38.0                   | 4.7                        | 13.7 |                           |      |        |   |      |
| 50.0                   | 48.0                   | 15.5                       | 18.0 | 38.5                      | 46.6 | 8.1    |   | 0.81 |
| 60.0                   | 58.0                   | 22.7                       | 24.1 | 48.4                      | 57.5 | 9.1    |   | 0.91 |
| 70.0                   | 68.0                   | 26.9                       | 27.8 | 58.7                      | 68.0 | 9.3    |   | 0.93 |
| 80.0                   | 78.0                   | 28.3                       | 29.1 | 68.5                      | 77.8 | 9.3    |   | 0.93 |
| 90.0                   | 88.0                   | 29.8                       | 30.5 | 78.4                      | 87.8 | 9.4    |   | 0.94 |
| 100.0                  |                        | 31.1                       | 31.1 | 88.5                      | 98.0 | 9.5    |   | 0.95 |

## CONSOLIDATION DATA

| Elapsed<br>Time<br>(Min) | SQRT<br>Time<br>(Min) | Burette<br>Reading<br>(CC) | Volume<br>Defl.<br>(cc) |
|--------------------------|-----------------------|----------------------------|-------------------------|
| 0.00                     | 0.00                  | 0.50                       | 0.00                    |
| 0.25                     | 0.50                  | 2.60                       | -2.10                   |
| 0.5                      | 0.71                  | 2.70                       | -2.20                   |
| 1                        | 1.00                  | 2.80                       | -2.30                   |
| 2                        | 1.41                  | 3.00                       | -2.50                   |
| 4                        | 2.00                  | 3.20                       | -2.70                   |
| 9                        | 3.00                  | 3.60                       | -3.10                   |
| 16                       | 4.00                  | 3.90                       | -3.40                   |
| 30                       | 5.48                  | 4.35                       | -3.85                   |
| 60                       | 7.75                  | 5.05                       | -4.55                   |
| 120                      | 10.95                 | 5.90                       | -5.40                   |
| 240                      | 15.49                 | 7.10                       | -6.60                   |
| 360                      | 18.97                 | 7.95                       | -7.45                   |
|                          |                       |                            |                         |

| Initial Height (in)      |
|--------------------------|
| Height Change (in)       |
| Ht. After Cons. (in)     |
| Initial Area (sq in)     |
| Area After Cons. (sq in) |

| 10/01 | 12  | <b>n</b> 1 | 2 |
|-------|-----|------------|---|
| 10/01 | • ~ | vι         | £ |

Init. Vol. (CC)

Vol. Change (CC)

Net Change (CC)

Cons. Vol. (CC)

Cell Exp. (CC)

3.085

0.034 3.051

6.290

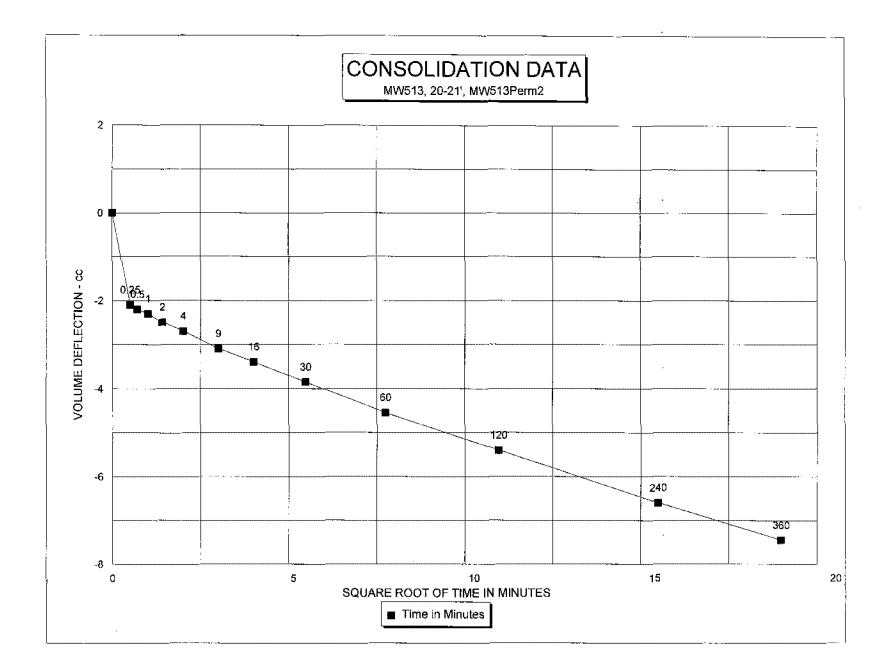
5.854

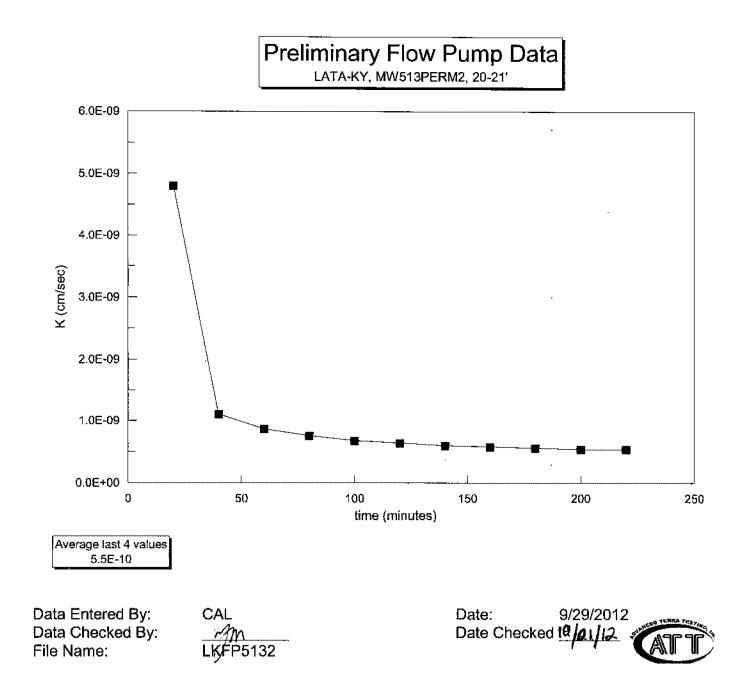


318.05

40.85

| Data entry by:     | MLM ,0        |   |
|--------------------|---------------|---|
| Checked by: CAL    | Date: 10/02/1 | L |
| FileName: LKP05132 | - 1 - 1       |   |





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| CLIENT LATA Envi | ironmental Services - KY   | JOB NO. 2855-02 |                  |
|------------------|----------------------------|-----------------|------------------|
| BORING NO.       | MW513                      | SAMPLED         | 08/23/12 KD      |
| DEPTH            | 40-42'                     | TEST STARTED    | 09/15/12 CAL     |
| SAMPLE NO.       | MW513PERM3                 | TEST FINISHED   | 09/26/12 CAL     |
| SOIL DESCR.      | ERI12-SW-SWMU211A          | CELL NUMBER     | 1P               |
| LOCATION         | SW Plume RDSI Geotechnical | SATURATED TEST  | Yes              |
| CONF. PRES. PSF  | 5305                       | TEST TYPE       | TX/Pbp/Tap Water |

| MOISTURE/DENSITY           | BEFORE  | AFTER   |        |
|----------------------------|---------|---------|--------|
| DATA                       | TEST    | TEST    |        |
| Wt. Soil + Moisture (g)    | 657.4   | 659.7   |        |
| Wt. Wet Soil & Pan (g)     | 664.1   | 666.5   |        |
| Wt. Dry Soil & Pan (g)     | 540.4   | 540.4   |        |
| Wt. Lost Moisture (g)      | 123.7   | 126.1   |        |
| Wt. of Pan Only (g)        | 6.7     | 6.7     |        |
| Wt. of Dry Soil (g)        | 533.7   | 533.7   |        |
| Moisture Content %         | 23.2    | 23.6    |        |
| Wet Density PCF            | 126.7   | 136.8   |        |
| Dry Density PCF            | 102.8   | 110.6   |        |
| Init. Diameter (in)        | 2.857   | (cm)    | 7.257  |
| Init. Area (sq in)         | 6.411   | (sq.cm) | 41.362 |
| Init. Height (in)          | 3.084   | (cm)    | 7.833  |
| Vol. Bef. Consol. (cu ft)  | 0.01144 |         |        |
| Vol. After Consol. (cu ft) | 0.01064 |         |        |
| Porosity %                 | 41.86   |         |        |

# FLOW PUMP CALCULATIONS

| Pump Setting (gear number)<br>Percentage of Pump setting<br>Q (cc/s)<br>Height<br>Diameter<br>Pressure (psi)<br>Area after consol. (cm*cm)<br>Gradient<br>Permeability k (cm/s)<br><b>Permeability k (m/s)</b><br>Back Pressure (psi) | 11<br>100<br>5.71E-05<br>3.057<br>2.767<br>0.850<br>38.786<br>7.697<br>1.9E-07<br><b>1.9E-07</b><br><b>1.9E-09</b><br>48.0 |
|---|--|
| Cell Pressure (psi)<br>Ave. Effective Stress (psi)  | 48.0<br>84.8<br>36.375   |
| Average temperature degree C:   | 22.5   |

Date: <u>9/27/101</u>2

| Data entry by:     | DAW   |
|--------------------|-------|
| Checked by: CAL    | Date: |
| FileName: LKP05133 |       |

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09/27/2012



| CLIENT LATA En  | vironmental Services - KY  | JOB NO. 2855-02 |                  |
|-----------------|----------------------------|-----------------|------------------|
| BORING NO.      | MW513                      | SAMPLED         | 08/23/12 KD      |
| DEPTH           | 40-42'                     | TEST STARTED    | 09/15/12 CAL     |
| SAMPLE NO.      | MW513PERM3                 | TEST FINISHED   | 09/26/12 CAL     |
| SOIL DESCR.     | ERI12-SW-SWMU211A          | SETUP NO.       | 1P               |
| LOCATION        | SW Plume RDSI Geotechnical | SATURATED TEST  | Yes              |
| CONF. PRES. PSF | 5305                       | TEST TYPE       | TX/Pbp/Tap Water |

# SATURATION DATA

| Cell<br>Pres.<br>(PSI) | Back<br>Pres.<br>(PSI) | Burette<br>Reading<br>(CC) |      | Pore<br>Pressure<br>(PSI) | C    | hange | В |      |
|------------------------|------------------------|----------------------------|------|---------------------------|------|-------|---|------|
|                        |                        | Close                      | Open | Close                     | Open |       |   |      |
| 40.0                   | 38.0                   | 4.2                        | 15.6 |                           |      |       |   |      |
| 50.0                   | 48.0                   | 20.9                       | 24.6 | 38.8                      | 45.3 | 6.5   |   | 0.65 |
| 60.0                   |                        | 24.3                       | 25.5 | 48.9                      | 58.7 | 9.8   |   | 0.98 |

#### CONSOLIDATION DATA

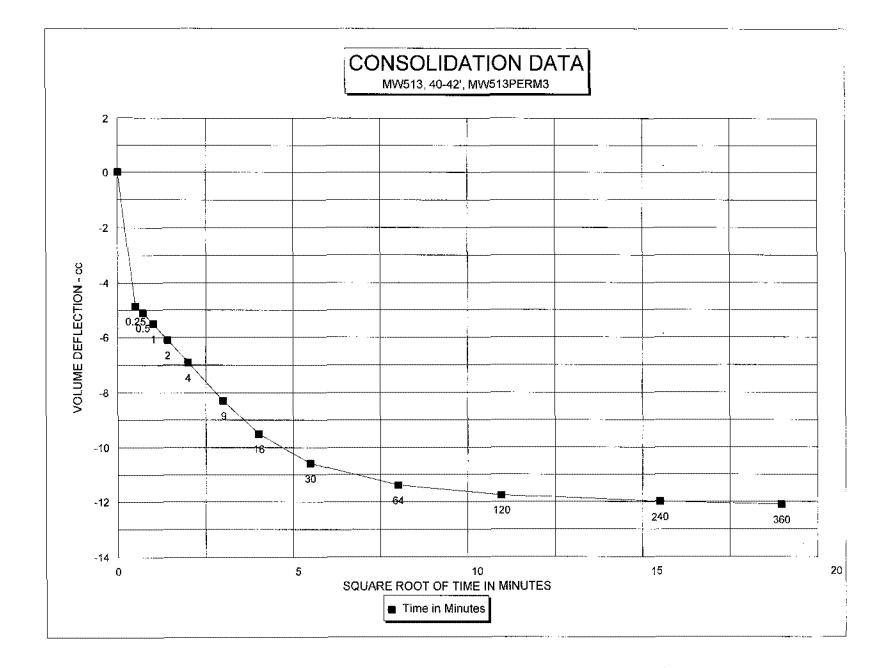
|                          | Elapsed         | SQRT  |            | Burette        | Volume |                   |
|--------------------------|-----------------|-------|------------|----------------|--------|-------------------|
|                          | Time            | Time  |            | Reading        | Defl.  |                   |
|                          | (Min)           | (Min) |            | (CC)           | (CC)   |                   |
|                          | (1111)          | (min) |            | (00)           | (00)   |                   |
|                          | 0.00            | 0.00  |            | 0.10           | 0.00   |                   |
|                          | 0.25            | 0.50  |            | 4.95           | -4.85  |                   |
|                          | 0.5             | 0.71  |            | 5.20           | -5.10  |                   |
|                          | 1               | 1.00  |            | 5.60           | -5.50  |                   |
|                          | 2               | 1.41  |            | 6.20           | -6.10  |                   |
|                          | 4               | 2.00  |            | 7,00           | -6.90  |                   |
|                          | 9               | 3.00  |            | 8.40           | -8.30  |                   |
|                          | 16              | 4.00  |            | 9.60           | -9.50  |                   |
|                          | 30              | 5.48  |            | 10.70          | -10.60 |                   |
|                          | 64              | 8.00  |            | 11.50          | -11.40 |                   |
|                          | 120             | 10.95 |            | 11.85          |        |                   |
|                          |                 |       |            |                | -11.75 |                   |
|                          | 240             | 15.49 |            | 12.10          | -12.00 |                   |
|                          | 360             | 18.97 |            | 12.20          | -12.10 |                   |
|                          |                 |       |            |                |        |                   |
| Initial Height (in)      |                 | 3.084 |            | Init. Vol. (CC | 2)     | 324.04            |
| Height Change (in)       |                 | 0.027 |            | Vol. Change    |        | 36.40             |
| Ht. After Cons. (in)     |                 | 3.057 |            | Cell Exp. (C   |        | 13.57             |
| Initial Area (sq in)     |                 | 6.411 |            | Net Change     |        | 22.83             |
| Area After Cons. (sq in) |                 | 6.012 |            | Cons. Vol. (   |        | 301.22            |
|                          |                 | 0.012 |            |                | ,      | AND TERRA TESTINO |
| Data entry by:           | DAW D           | ate:  | 09/27/2012 |                |        |                   |
|                          | Date: 9/21/101; |       | 50/21/20/2 |                |        |                   |
|                          |                 | F     |            |                |        |                   |

| Checked by | 1: <u>CA</u> | Date |
|------------|--------------|------|
| FileName:  | LKP05133     |      |

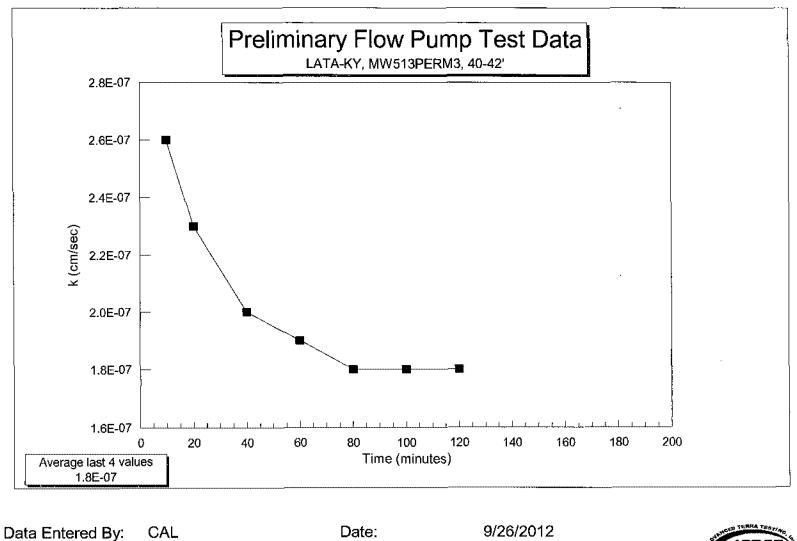
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Date Checked:

9/27/2012



Data Checked By:

File Name:

<u>م</u>عب LKFP5133 Grain Size Analysis

# ASTM D422

Advanced Terra Testing

| CLIENT LATA Ken  | tucky  | JOB NO. 2855-06  |   |
|--|--|--|---|
| BORING NO.<br>DEPTH<br>SAMPLE NO.<br>SOIL DESCR.<br>LOCATION | 211-B-007<br>8.0-12.0'<br>211B007GRNSZ1<br>ERI12-SW-SWMU211B<br>SW Plume RDSI Geotechnical | SAMPLED<br>DATE TESTED<br>WASH SIEVE<br>DRY SIEVE        | 10/16/12 KD<br>11/8/12 SKL<br>Yes<br>No |
|  |  |  |   |
| MOISTURE DATA  |  | WASH SIEVE ANALY   | 515                                     |
| HYGROSCOPIC  | Yes  | Wt. Total Sample<br>Wet (g)                              | 973.66                                  |
| NATURAL  | No   | Weight of + #10<br>Before Washing (g)<br>Weight of + #10 | 0.00                                    |
| Wt. Wet Soil & Pan (g<br>Wt. Dry Soil & Pan (g)              |  | After Washing (g)<br>Weight of - #10                     | 0.00                                    |
| Wt. Lost Moisture (g)<br>Wt. of Pan Only (g)                 | 2.24<br>6.53   | Wet (g)<br>Weight of - #10                               | 973.66                                  |
| Wt. of Dry Soil (g)<br>Moisture Content %                    | 176.28<br>1.3  | Dry (g)<br>Wt. Total Sample                              | 961.44                                  |
|  |  | Dry (g)  | 961.44                                  |
| Wt. Hydrom. Sample V<br>Wt. Hydrom. Sample D                 |  | Calc. Wt. "W" (g)<br>Calc. Mass + #10                    | 65.18<br>0.00                           |

| Sieve  | Pan    | Indiv.    | Indiv.  | Cum.    | Cum.    | %      |
|--------|--------|-----------|---------|---------|---------|--------|
| Number | Weight | Wt. + Pan | Wt.     | WVt.    | %       | Finer  |
| (Size) | (g)    | (g)       | Retain. | Retain. | Retain. | By Wt. |
| 3"     | 0.00   | 0.00      | 0.00    | 0.00    | 0.0     | 100.0  |
| 1 1/2" | 0.00   | 0.00      | 0.00    | 0.00    | 0.0     | 100.0  |
| 3/4"   | 0.00   | 0.00      | 0.00    | 0.00    | 0.0     | 100.0  |
| 3/8"   | 0.00   | 0.00      | 0.00    | 0.00    | 0.0     | 100.0  |
| #4     | 0.00   | 0.00      | 0.00    | 0.00    | 0.0     | 100.0  |
| #10    | 0.00   | 0.00      | 0.00    | 0.00    | 0.0     | 100.0  |
|        |        |           |         |         |         |        |
| #20    | 3.18   | 3.33      | 0.15    | 0.15    | 0.2     | 99.8   |
| #40    | 3.02   | 3.30      | 0.29    | 0.44    | 0.7     | 99.3   |
| #60    | 3.12   | 4.59      | 1.47    | 1.91    | 2.9     | 97.1   |
| #100   | 3.17   | 6.77      | 3.60    | 5.52    | 8.5     | 91.5   |
| #200   | 3.02   | 5.61      | 2.59    | 8.11    | 12.4    | 87.6   |

Data entered by: MLM Data checked by: MLM FileName: LKHY07Z1



| CLIENT LATA  | Kentucky   | JOB NO. 2855-06   |   |
|--|--|---|---|
| BORING NO.<br>DEPTH<br>SAMPLE NO.<br>SOIL DESCR.<br>LOCATION   | 211-B-007<br>8.0-12.0'<br>211B007GRNSZ1<br>ERI12-SW-SWMU211B<br>SW Plume RDSI Geotechnical | SAMPLED<br>DATE TESTED<br>WASH SIEVE<br>DRY SIEVE                         | 10/16/12 KD<br>11/8/12 SKL<br>Yes<br>No |
| *  |  | (* .  |   |
| Hydrometer #<br>Sp. Gr. of Soil<br>Value of "alpha"<br>Deflocculant<br>Defloc. Corr'n<br>Meniscus Corr'n | ASTM 152 H<br>2.65<br>1.00<br>Sodium Hexametaphosphate<br>5.0<br>0.0                       | Temp., Deg. C<br>Temp. Coef. K<br>Wt. Dry Sample "W"<br>% of Total Sample | 22.6<br>0.01323<br>65.178<br>100.0      |

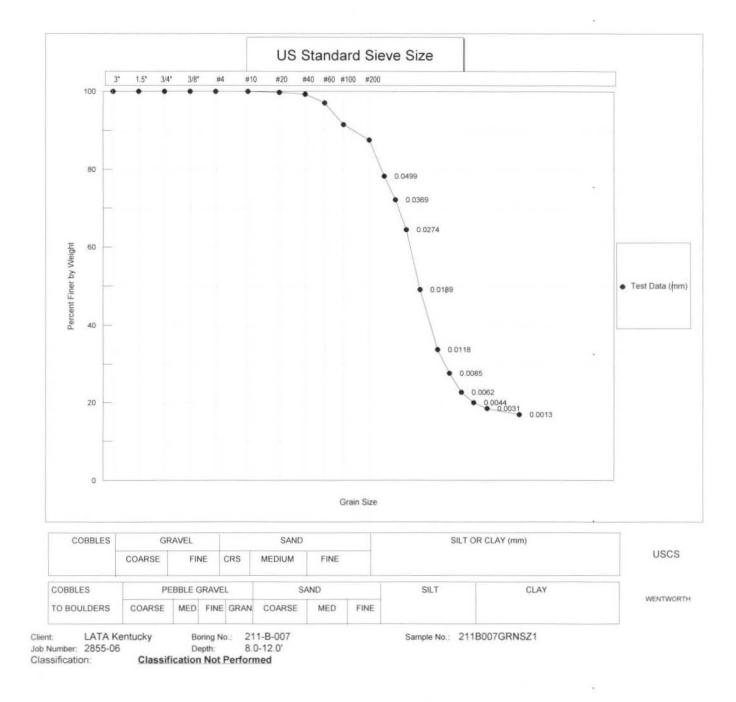
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| Elapsed<br>Time<br>(min) | Hydrometer<br>Original | Reading<br>Corrected<br>"R" | 100Ra/W | %<br>Total<br>Sample | Effective<br>Depth<br>L | Grain<br>Diameter<br>(mm) |
|--------------------------|------------------------|-----------------------------|---------|----------------------|-------------------------|---------------------------|
| 0.0                      |                        |                             |         | -                    |                         |                           |
| 0.5                      | 56.00                  | 51.00                       | 78.2    | 78.2                 | 7.11                    | 0.0499                    |
| 1.0                      | 52.00                  | 47.00                       | 72.1    | 72.1                 | 7.76                    | 0.0369                    |
| 2.0                      | 47.00                  | 42.00                       | 64.4    | 64.4                 | 8.58                    | 0.0274                    |
| 5.0                      | 37.00                  | 32.00                       | 49.1    | 49.1                 | 10.22                   | 0.0189                    |
| 15.0                     | 27.00                  | 22.00                       | 33.8    | 33.8                 | 11.86                   | 0.0118                    |
| 30.0                     | 23.00                  | 18.00                       | 27.6    | 27.6                 | 12.52                   | 0.0085                    |
| 60.0                     | 19.75                  | 14.75                       | 22.6    | 22.6                 | 13.05                   | 0.0062                    |
| 120.0                    | 18.00                  | 13.00                       | 19.9    | 19.9                 | 13.34                   | 0.0044                    |
| 250.0                    | 17.00                  | 12.00                       | 18.4    | 18.4                 | 13.50                   | 0.0031                    |
| 1440.0                   | 16.00                  | 11.00                       | 16.9    | 16.9                 | 13.67                   | 0.0013                    |

Grain Diameter = K\*(SQRT(L/T))

Data entered by: Data checked by: FileName: LKHY07Z1







| CLIENT LATA Ken  | tucky  | JOB NO. 2855-06                                   |   |
|--|--|---|---|
| BORING NO.<br>DEPTH<br>SAMPLE NO.<br>SOIL DESCR.<br>LOCATION | 211-B-007<br>27.5-31.5<br>211B007GRNSZ2<br>ERI12-SW-SWMU211B<br>SW Plume RDSI Geotechnical | SAMPLED<br>DATE TESTED<br>WASH SIEVE<br>DRY SIEVE | 10/16/12 KD<br>11/8/12 SKL<br>Yes<br>No |
| 2  |  |   |   |
| MOISTURE DATA  |  | WASH SIEVE ANALY                                  | SIS                                     |
| HYGROSCOPIC  | Yes  | Wt. Total Sample<br>Wet (g)                       | 863.29                                  |
| NATURAL  | No   | Weight of + #10                                   | 000.20                                  |
|  |  | Before Washing (g)<br>Weight of + #10             | 2.64                                    |
| Wt. Wet Soil & Pan (g)<br>Wt. Dry Soil & Pan (g)             | 113.21<br>111.93   | After Washing (g)<br>Weight of - #10              | 2.49                                    |
| Wt. Lost Moisture (g)<br>Wt. of Pan Only (g)                 | 1.28<br>8.34   | Wet (g)<br>Weight of - #10                        | 860.65                                  |
| Wt. of Dry Soil (g)<br>Moisture Content %                    | 103.59<br>1.2  | Dry (g)<br>Wt. Total Sample                       | 850.29                                  |
|  | 1.2  | Dry (g)   | 852.78                                  |
| Wt. Hydrom. Sample V   |  | Calc. Wt. "W" (g)                                 | 67.08                                   |
| Wt. Hydrom. Sample D   | ry (g) 66.89   | Calc. Mass + #10                                  | 0.20                                    |
|  |  |   |   |

| Sieve  | P  | an    | Indiv.    | Inc | liv. | Cum   |      | Cu   | m.   | %  | 6     |
|--------|----|-------|-----------|-----|------|-------|------|------|------|----|-------|
| Number | We | eight | Wt. + Pan | N   | /t.  | Wt.   |      | %    |      | Fi | ner   |
| (Size) | (  | g)    | (g)       | Ret | ain. | Retai | n.   | Reta | in.  | By | Wt.   |
| 3"     |    | 0.00  | 0.00      |     | 0.00 |       | 0.00 |      | 0.0  | 3  | 100.0 |
| 1 1/2" |    | 0.00  | 0.00      |     | 0.00 |       | 0.00 |      | 0.0  |    | 100.0 |
| 3/4"   |    | 0.00  | 0.00      |     | 0.00 |       | 0.00 |      | 0.0  | 1  | 100.0 |
| 3/8"   |    | 0.00  | 0.00      |     | 0.00 |       | 0.00 |      | 0.0  | 1  | 100.0 |
| #4     |    | 0.00  | 1.23      |     | 1.23 |       | 1.23 |      | 0.1  |    | 99.9  |
| #10    |    | 0.00  | 1.26      |     | 1.26 | 2     | 2.49 |      | 0.3  |    | 99.7  |
|        |    |       |           |     |      |       |      |      |      |    |       |
| #20    |    | 3.02  | 3.24      |     | 0.22 |       | 0.22 |      | 0.6  |    | 99.4  |
| #40    |    | 3.10  | 4.19      |     | 1.09 |       | 1.32 |      | 2.3  |    | 97.7  |
| #60    |    | 3.00  | 7.60      |     | 4.60 |       | 5.92 |      | 9.1  |    | 90.9  |
| #100   |    | 3.07  | 11.15     |     | 8.08 | 1     | 3.99 |      | 21.1 |    | 78.9  |
| #200   |    | 3.21  | 12.13     |     | 8.92 | 2     | 2.92 | 1    | 34.5 |    | 65.5  |

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Date: 11/12/2012 Date: 1([12](2



| CLIENT LATA K    | entucky                    | JOB NO. 2855-06    |             |
|------------------|----------------------------|--------------------|-------------|
| BORING NO.       | 211-B-007                  | SAMPLED            | 10/16/12 KD |
| DEPTH            | 27.5-31.5                  | DATE TESTED        | 11/8/12 SKL |
| SAMPLE NO.       | 211B007GRNSZ2              | WASH SIEVE         | Yes         |
| SOIL DESCR.      | ERI12-SW-SWMU211B          | DRY SIEVE          | No          |
| LOCATION         | SW Plume RDSI Geotechnical |                    |             |
|                  |                            |                    | × .         |
| Hydrometer #     | ASTM 152 H                 | Temp., Deg. C      | 22.6        |
| Sp. Gr. of Soil  | 2.65                       | Temp. Coef. K      | 0.01323     |
| Value of "alpha" | 1.00                       | Wt. Dry Sample "W" | 67.083      |
| Deflocculant     | Sodium Hexametaphosphate   | % of Total Sample  | 100.0       |
| Defloc. Corr'n   | 5.0                        |                    |             |
| Meniscus Corr'n  | 0.0                        |                    |             |
|                  |                            |                    |             |

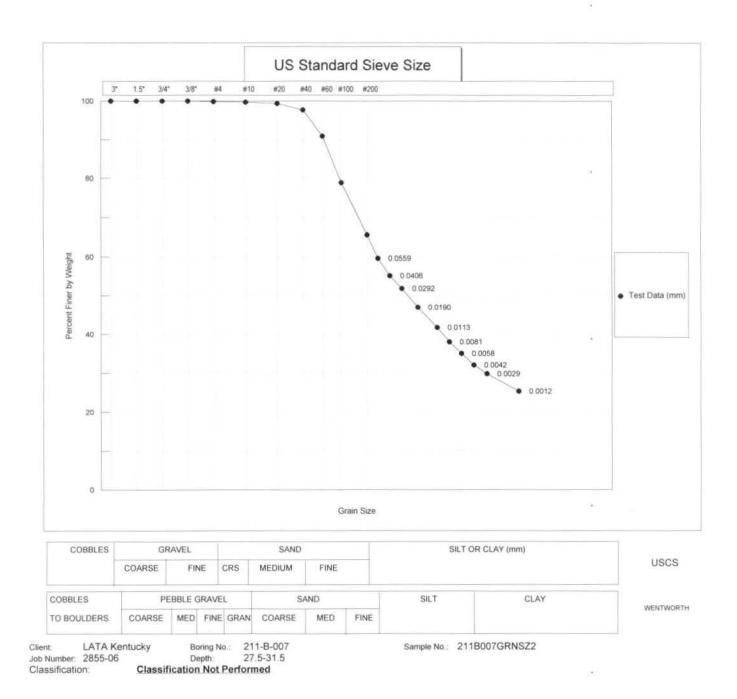
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| Elapsed<br>Time<br>(min) | Hydrometer<br>Original | Reading<br>Corrected<br>"R" | 100Ra/W | %<br>Total<br>Sample | Effective<br>Depth<br>L | Grain<br>Diameter<br>(mm) |
|--------------------------|------------------------|-----------------------------|---------|----------------------|-------------------------|---------------------------|
| 0.0                      |                        |                             |         | -                    |                         |                           |
| 0.5                      | 45.00                  | 40.00                       | 59.6    | 59.6                 | 8.91                    | 0.0559                    |
| 1.0                      | 42.00                  | 37.00                       | 55.2    | 55.2                 | 9.40                    | 0.0406                    |
| 2.0                      | 39.75                  | 34.75                       | 51.8    | 51.8                 | 9.77                    | 0.0292                    |
| 5.0                      | 36.50                  | 31.50                       | 47.0    | 47.0                 | 10.30                   | 0.0190                    |
| 15.0                     | 33.00                  | 28.00                       | 41.7    | 41.7                 | 10.88                   | 0.0113                    |
| 30.0                     | 30.50                  | 25.50                       | 38.0    | 38.0                 | 11.29                   | 0.0081                    |
| 60.0                     | 28.50                  | 23.50                       | 35.0    | 35.0                 | 11.62                   | 0.0058                    |
| 120.0                    | 26.50                  | 21.50                       | 32.0    | 32.0                 | 11.94                   | 0.0042                    |
| 250.0                    | 25.00                  | 20.00                       | 29.8    | 29.8                 | 12.19                   | 0.0029                    |
| 1440.0                   | 22.00                  | 17.00                       | 25.3    | 25.3                 | 12.68                   | 0.0012                    |

Grain Diameter = K\*(SQRT(L/T))

Data entered by: MLM Data checked by: All FileName: LKHY07Z2





| CLIENT LATA Ke   | ntucky  |  | JOB NO. 2855-06                                   |   |
|--|---------|--|---|---|
| BORING NO.<br>DEPTH<br>SAMPLE NO.<br>SOIL DESCR.<br>LOCATION |         | RNSZ3<br>SWMU211B<br>RDSI Geotechnical | SAMPLED<br>DATE TESTED<br>WASH SIEVE<br>DRY SIEVE | 10/16/12 KD<br>11/8/12 SKL<br>Yes<br>No |
| ×  | *       |  | - X   |   |
| MOISTURE DATA  |         |  | WASH SIEVE ANALY                                  | /SIS                                    |
| HYGROSCOPIC  | Yes     |  | Wt. Total Sample<br>Wet (g)                       | 890.19                                  |
| NATURAL  | No      |  | Weight of + #10                                   | 090.19                                  |
|  |         |  | Before Washing (g)<br>Weight of + #10             | 476.93                                  |
| Wt. Wet Soil & Pan (g<br>Wt. Dry Soil & Pan (g               |         | 108.24<br>107.11                       | After Washing (g)<br>Weight of - #10              | 463.85                                  |
| Wt. Lost Moisture (g)<br>Wt. of Pan Only (g)                 |         | 1.13<br>8.21                           | Wet (g)<br>Weight of - #10                        | 413.26                                  |
| Wt. of Dry Soil (g)<br>Moisture Content %                    |         | 98.90<br>1.1                           | Dry (g)<br>Wt. Total Sample                       | 421.52                                  |
|  |         |  | Dry (g)   | 885.37                                  |
| Wt. Hydrom. Sample   |         | 67.25                                  | Calc. Wt. "W" (g)                                 | 139.65                                  |
| Wt. Hydrom. Sample   | Dry (g) | 66.49                                  | Calc. Mass + #10                                  | 73.16                                   |
|  |         |  |   |   |
| Sieve Pan  | Indiv   | Indiv Cu                               | um Cum %  |   |

| Sieve  | Pan    | Indiv.    | Indiv.  | Cum.    | Cum.    | %      |
|--------|--------|-----------|---------|---------|---------|--------|
| Number | Weight | Wt. + Pan | Wt.     | Wt.     | %       | Finer  |
| (Size) | (g)    | (g)       | Retain. | Retain. | Retain. | By Wt. |
| 3"     | 0.00   | 0.00      | 0.00    | 0.00    | 0.0     | 100.0  |
| 1 1/2" | 0.00   | 0.00      | 0.00    | 0.00    | 0.0     | 100.0  |
| 3/4"   | 0.00   | 19.48     | 19.48   | 19.48   | 2.2     | 97.8   |
| 3/8"   | 0.00   | 139.98    | 139.98  | 159.46  | 18.0    | 82.0   |
| #4     | 0.00   | 167.21    | 167.21  | 326.67  | 36.9    | 63.1   |
| #10    | 0.00   | 137.18    | 137.18  | 463.85  | 52.4    | 47.6   |
|        |        |           |         |         |         |        |
| #20    | 3.25   | 15.75     | 12.50   | 12.50   | 61.3    | 38.7   |
| #40    | 3.08   | 14.50     | 11.42   | 23.93   | 69.5    | 30.5   |
| #60    | 3.29   | 14.99     | 11.70   | 35.62   | 77.9    | 22.1   |
| #100   | 3.12   | 10.27     | 7.16    | 42.78   | 83.0    | 17.0   |
| #200   | 2.98   | 6.45      | 3.47    | 46.25   | 85.5    | 14.5   |

Data entered by: Data checked by: \_\_\_\_\_\_ FileName: LKHY07Z3



| CLIENT LATA K  | entucky  | JOB NO. 2855-06   |   |
|--|--|---|---|
| BORING NO.<br>DEPTH<br>SAMPLE NO.<br>SOIL DESCR.<br>LOCATION   | 211-B-007<br>42.5-44.0<br>211B007GRNSZ3<br>ERI12-SW-SWMU211B<br>SW Plume RDSI Geotechnical | SAMPLED<br>DATE TESTED<br>WASH SIEVE<br>DRY SIEVE                         | 10/16/12 KD<br>11/8/12 SKL<br>Yes<br>No |
|  |  |   |   |
| Hydrometer #<br>Sp. Gr. of Soil<br>Value of "alpha"<br>Deflocculant<br>Defloc. Corr'n<br>Meniscus Corr'n | ASTM 152 H<br>2.65<br>1.00<br>Sodium Hexametaphosphate<br>5.0<br>0.0                       | Temp., Deg. C<br>Temp. Coef. K<br>Wt. Dry Sample "W"<br>% of Total Sample | 22.6<br>0.01323<br>139.649<br>100.0     |

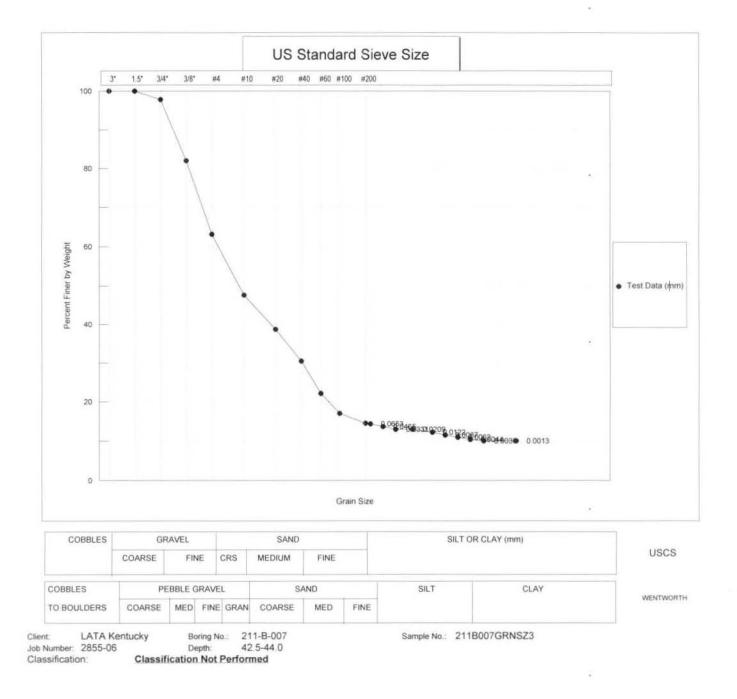
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|---|--|--|--|--|
|   |  |  |  |  |
|   |  |  |  |  |
|   |  |  |  |  |

| Elapsed<br>Time<br>(min) | Hydrometer<br>Original | Reading<br>Corrected<br>"R" | 100Ra/W | %<br>Total<br>Sample | Effective<br>Depth<br>L | Grain<br>Diameter<br>(mm) |
|--------------------------|------------------------|-----------------------------|---------|----------------------|-------------------------|---------------------------|
| 0.0                      |                        |                             |         |                      |                         |                           |
| 0.5                      | 25.00                  | 20.00                       | 14.3    | 14.3                 | 12.19                   | 0.0653                    |
| 1.0                      | 24.00                  | 19.00                       | 13.6    | 13.6                 | 12.35                   | 0.0465                    |
| 2.0                      | 23.00                  | 18.00                       | 12.9    | 12.9                 | 12.52                   | 0.0331                    |
| 5.0                      | 23.00                  | 18.00                       | 12.9    | 12.9                 | 12.52                   | 0.0209                    |
| 15.0                     | 22.00                  | 17.00                       | 12.2    | 12.2                 | 12.68                   | 0.0122                    |
| 30.0                     | 21.00                  | 16.00                       | 11.5    | 11.5                 | 12.85                   | 0.0087                    |
| 60.0                     | 20.25                  | 15.25                       | 10.9    | 10.9                 | 12.97                   | 0.0062                    |
| 120.0                    | 19.50                  | 14.50                       | 10.4    | 10.4                 | 13.09                   | 0.0044                    |
| 250.0                    | 19.00                  | 14.00                       | 10.0    | 10.0                 | 13.17                   | 0.0030                    |
| 1442.0                   | 19.00                  | 14.00                       | 10.0    | 10.0                 | 13.17                   | 0.0013                    |

Grain Diameter = K\*(SQRT(L/T))

Data entered by: MLM Date: Data checked by: Data Checked by: Date: Date:





| CLIENT LATA Ken  | tucky   | JOB NO. 2855-6                                    |   |
|--|---|---|---|
| BORING NO.<br>DEPTH<br>SAMPLE NO.<br>SOIL DESCR.<br>LOCATION | 211-B-004<br>5-7.5'<br>211B004GRNSZ1<br>ERI12-SW-SWMU211B<br>SW Plume RDSI Geotechnical | SAMPLED<br>DATE TESTED<br>WASH SIEVE<br>DRY SIEVE | 10/11/12 KD<br>11/8/12 SKL<br>Yes<br>No |
|  |   |   |   |
| MOISTURE DATA  |   | WASH SIEVE ANALY                                  | SIS                                     |
| HYGROSCOPIC  | Yes   | Wt. Total Sample                                  | 1005.05                                 |
| NATURAL  | No  | Wet (g)<br>Weight of + #10                        | 1085.85                                 |
|  |   | Before Washing (g)<br>Weight of + #10             | 2.34                                    |
| Wt. Wet Soil & Pan (g<br>Wt. Dry Soil & Pan (g)              |   | After Washing (g)<br>Weight of - #10              | 1.85                                    |
| Wt. Lost Moisture (g)<br>Wt. of Pan Only (g)                 | 0.35<br>3.04  | Wet (g)<br>Weight of - #10                        | 1083.51                                 |
| Wt. of Dry Soil (g)<br>Moisture Content %                    | 30.20<br>1.2  | Dry (g)<br>Wt. Total Sample                       | 1071.58                                 |
|  | 1.2   | Dry (g)   | 1073.43                                 |
| Wt. Hydrom. Sample V   | Vet (g) 70.23   | Calc. Wt. "W" (g)                                 | 69.54                                   |
| Wt. Hydrom. Sample D   |   | Calc. Mass + #10                                  | 0.12                                    |
|  |   |   |   |

| Sieve<br>Number<br>(Size) | Pan<br>Weight<br>(g) | Indiv.<br>Wt. + Pan<br>(g) | Indiv.<br>Wt.<br>Retain. | Cum.<br>Wt.<br>Retain. | Cum.<br>%<br>Retain. | %<br>Finer<br>By Wt. |
|---------------------------|----------------------|----------------------------|--------------------------|------------------------|----------------------|----------------------|
| 3"                        | 0.0                  | 0.00                       | 0.00                     | 0.00                   | 0.0                  | 100.0                |
| 1 1/2"                    | 0.0                  | 00.0 00                    | 0.00                     | 0.00                   | 0.0                  | 100.0                |
| 3/4"                      | 0.0                  | 00.0 00                    | 0.00                     | 0.00                   | 0.0                  | 100.0                |
| 3/8"                      | 0.0                  | 00.0 00                    | 0.00                     | 0.00                   | 0.0                  | 100.0                |
| #4                        | 0.0                  | 0.83                       | 0.83                     | 0.83                   | 0.1                  | 99.9                 |
| #10                       | 0.0                  | 1.02                       | 1.02                     | 1.85                   | 0.2                  | 99.8                 |
| #20                       | 3.0                  | 00 3.26                    | 0.25                     | 0.25                   | 0.5                  | 99.5                 |
| #40                       | 3.0                  |                            | 0.31                     | 0.56                   | 1.0                  | 99.0                 |
| #60                       | 3.0                  |                            | 0.91                     | 1.47                   | 2.3                  | 97.7                 |
| #100                      | 2.9                  |                            | 1.76                     | 3.24                   | 4.8                  | 95.2                 |
| #200                      | 3.0                  |                            | 1.14                     | 4.38                   | 6.5                  | 93.5                 |

Data entered by: MLM Data checked by: MLM FileName: LKHY04Z1



| CLIENT LATA K  | entucky   | JOB NO. 2855-6  |   |
|--|---|---|---|
| BORING NO.<br>DEPTH<br>SAMPLE NO.<br>SOIL DESCR.<br>LOCATION   | 211-B-004<br>5-7.5'<br>211B004GRNSZ1<br>ERI12-SW-SWMU211B<br>SW Plume RDSI Geotechnical | SAMPLED<br>DATE TESTED<br>WASH SIEVE<br>DRY SIEVE                         | 10/11/12 KD<br>11/8/12 SKL<br>Yes<br>No |
|  |   |   |   |
| Hydrometer #<br>Sp. Gr. of Soil<br>Value of "alpha"<br>Deflocculant<br>Defloc. Corr'n<br>Meniscus Corr'n | ASTM 152 H<br>2.65<br>1.00<br>Sodium Hexametaphosphate<br>5.0<br>0.0                    | Temp., Deg. C<br>Temp. Coef. K<br>Wt. Dry Sample "W"<br>% of Total Sample | 22.7<br>0.01322<br>69.543<br>100.0      |

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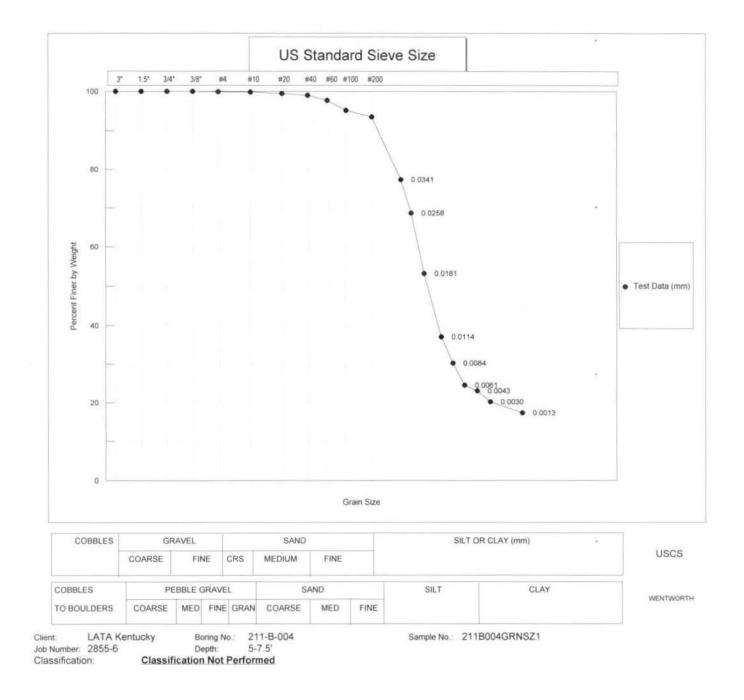
| Elapsed<br>Time<br>(min) | Hydrometer<br>Original | Reading<br>Corrected<br>"R" | 100Ra/W | %<br>Total<br>Sample | Effective<br>Depth<br>L | Grain<br>Diameter<br>(mm) |
|--------------------------|------------------------|-----------------------------|---------|----------------------|-------------------------|---------------------------|
| 0.0                      |                        |                             |         |                      |                         |                           |
| 0.5                      |                        |                             |         |                      |                         |                           |
| 1.0                      | 58.75                  | 53.75                       | 77.3    | 77.3                 | 6.66                    | 0.0341                    |
| 2.0                      | 52.75                  | 47.75                       | 68.7    | 68.7                 | 7.64                    | 0.0258                    |
| 5.0                      | 42.00                  | 37.00                       | 53.2    | 53.2                 | 9.40                    | 0.0181                    |
| 15.0                     | 30.75                  | 25.75                       | 37.0    | 37.0                 | 11.25                   | 0.0114                    |
| 30.0                     | 26.00                  | 21.00                       | 30.2    | 30.2                 | 12.03                   | 0.0084                    |
| 60.0                     | 22.00                  | 17.00                       | 24.4    | 24.4                 | 12.68                   | 0.0061                    |
| 120.0                    | 21.00                  | 16.00                       | 23.0    | 23.0                 | 12.85                   | 0.0043                    |
| 250.0                    | 19.00                  | 14.00                       | 20.1    | 20.1                 | 13.17                   | 0.0030                    |
| 1440.0                   | 17.00                  | 12.00                       | 17.3    | 17.3                 | 13.50                   | 0.0013                    |

Grain Diameter = K\*(SQRT(L/T))

Data entered by: MLM Data checked by: MLM FileName: LKHY04Z1

Date: 11/12/2012 Date: 1((12))





| CLIENT LATA Ken  | tucky  |   | JOB NO.                                      | 2855-6  |   |
|--|--|---|--|---|---|
| BORING NO.<br>DEPTH<br>SAMPLE NO.<br>SOIL DESCR.<br>LOCATION | 211-B-004<br>21.1-23.5'<br>211B004GRNSZ2<br>ERI12-SW-SWMU2<br>SW Plume RDSI Ge | 5 ( S. 1997) ( S. 1997) ( S. 1997) ( S. 1997) | SAMPLED<br>DATE TES<br>WASH SIE<br>DRY SIEVE | TED<br>VE   | 10/11/12 KD<br>11/5/12 SKL<br>Yes<br>No |
| MOISTURE DATA  |  |   | WASH SIE                                     | VE ANALYS   | IS                                      |
| HYGROSCOPIC  | Yes  |   | Wt. Total S<br>Wet                           | States of the second | 1098.78                                 |
| NATURAL  | No   |   | Weight of +                                  |   |   |
|  |  |   | Before Was<br>Weight of +                    |   | 530.91                                  |
| Wt. Wet Soil & Pan (g)<br>Wt. Dry Soil & Pan (g)             |  | 4.00<br>3.31                                  | After Wash<br>Weight of -                    |   | 507.08                                  |
| Wt. Lost Moisture (g)  |  | 0.69  | Wet  | (g)   | 567.87                                  |
| Wt. of Pan Only (g)  |  | 3.13  | Weight of -                                  |   | 505.04                                  |
| Wt. of Dry Soil (g)<br>Moisture Content %                    | 1  | 0.18<br>1.0                                   | Dry (<br>Wt. Total S                         |   | 585.94                                  |
| Moisture Content %   |  | 1.0   | Dry (  |   | 1093.02                                 |
| Wt. Hydrom. Sample V   | Vet (g) 7  | 1.67  | Calc. Wt. "                                  |   | 132.39                                  |
| Wt. Hydrom. Sample D   | ry (g) 7   | 0.97  | Calc. Mass                                   | s + #10   | 61.42                                   |

| Sieve<br>Number<br>(Size) | Pan<br>Weight<br>(g) | Indiv.<br>Wt. + Pan<br>(g) | Indiv.<br>Wt.<br>Retain. | Cum.<br>Wt.<br>Retain. | Cum.<br>%<br>Retain. | %<br>Finer<br>By Wt. |
|---------------------------|----------------------|----------------------------|--------------------------|------------------------|----------------------|----------------------|
| 3"                        | 0.00                 | 0.00                       | 0.00                     | 0.00                   | 0.0                  | 100.0                |
| 1 1/2"                    | 0.00                 | 0.00                       | 0.00                     | 0.00                   | 0.0                  | 100.0                |
| 3/4"                      | 0.00                 | 13.47                      | 13.47                    | 13.47                  | 1.2                  | 98.8                 |
| 3/8"                      | 0.00                 | 124.78                     | 124.78                   | 138.25                 | 12.6                 | 87.4                 |
| #4                        | 0.00                 | 202.57                     | 202.57                   | 340.82                 | 31.2                 | 68.8                 |
| #10                       | 0.00                 | 166.26                     | 166.26                   | 507.08                 | 46.4                 | 53.6                 |
| 512 U                     | 0.00                 |                            |                          |                        |                      |                      |
| #20                       | 3.05                 | 16.65                      | 13.59                    | 13.59                  | 56.7                 | 43.3                 |
| #40                       | 3.19                 | 20.53                      | 17.33                    | 30.92                  | 69.8                 | 30.2                 |
| #60                       | 2.99                 | 13.21                      | 10.22                    | 41.14                  | 77.5                 | 22.5                 |
| #100                      | 3.05                 | 7.42                       | 4.37                     | 45.52                  | 80.8                 | 19.2                 |
| #200                      | 3.24                 | 6.24                       | 3.00                     | 48.51                  | 83.0                 | 17.0                 |

Data entered by: Data checked by: FileName: LKHY04Z2

Date: 11/07/2012 Date: 11/7/12



| CLIENT LATA  | Kentucky  | JOB NO. 2855-6  |   |
|--|---|---|---|
| BORING NO.<br>DEPTH<br>SAMPLE NO.<br>SOIL DESCR.<br>LOCATION   | 211-B-004<br>21.1-23.5'<br>211B004GRNSZ2<br>ERI12-SW-SWMU211B<br>SW Plume RDSI Geotechnical | SAMPLED<br>DATE TESTED<br>WASH SIEVE<br>DRY SIEVE                         | 10/11/12 KD<br>11/5/12 SKL<br>Yes<br>No |
| Hydrometer #<br>Sp. Gr. of Soil<br>Value of "alpha"<br>Deflocculant<br>Defloc. Corr'n<br>Meniscus Corr'n | ASTM 152 H<br>2.65<br>1.00<br>Sodium Hexametaphosphate<br>5.0<br>0.0                        | Temp., Deg. C<br>Temp. Coef. K<br>Wt. Dry Sample "W"<br>% of Total Sample | 22.7<br>0.01322<br>132.394<br>100.0     |

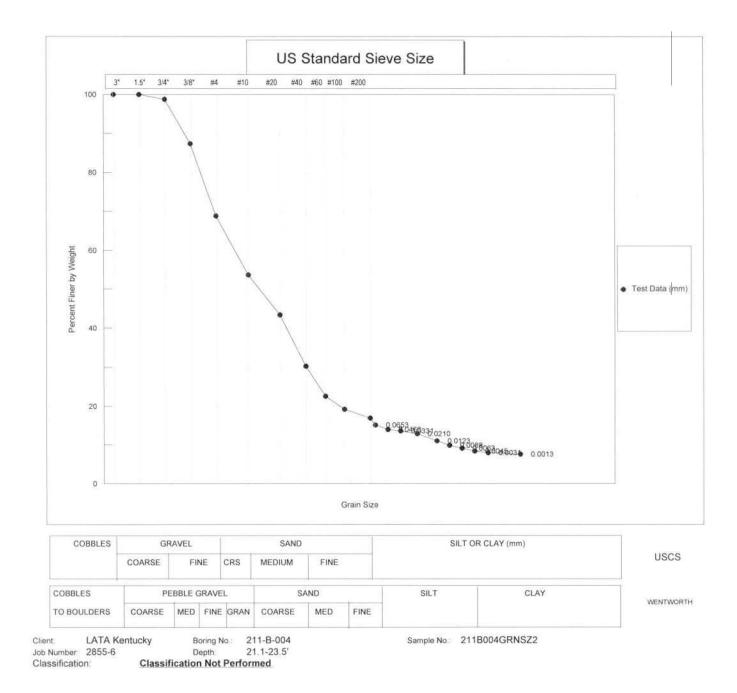
| T<br>Elapsed<br>Time<br>(min) | Hydrometer<br>Original | Reading<br>Corrected<br>"R" | 100Ra/W | %<br>Total<br>Sample | Effective<br>Depth<br>L | Grain<br>Diameter<br>(mm) |
|-------------------------------|------------------------|-----------------------------|---------|----------------------|-------------------------|---------------------------|
| 0.0                           |                        |                             | ,122    |                      |                         |                           |
| 0.5                           | 25.00                  | 20.00                       | 15.1    | 15.1                 | 12.19                   | 0.0653                    |
| 1.0                           | 23.50                  | 18.50                       | 14.0    | 14.0                 | 12.44                   | 0.0466                    |
| 2.0                           | 23.00                  | 18.00                       | 13.6    | 13.6                 | 12.52                   | 0.0331                    |
| 5.0                           | 22.00                  | 17.00                       | 12.8    | 12.8                 | 12.68                   | 0.0210                    |
| 15.0                          | 19.50                  | 14.50                       | 11.0    | 11.0                 | 13.09                   | 0.0123                    |
| 30.0                          | 18.00                  | 13.00                       | 9.8     | 9.8                  | 13.34                   | 0.0088                    |
| 60.0                          | 17.00                  | 12.00                       | 9.1     | 9.1                  | 13.50                   | 0.0063                    |
| 120.0                         | 16.00                  | 11.00                       | 8.3     | 8.3                  | 13.67                   | 0.0045                    |
| 250.0                         | 15.50                  | 10.50                       | 7.9     | 7.9                  | 13.75                   | 0.0031                    |
| 1440.0                        | 15.00                  | 10.00                       | 7.6     | 7.6                  | 13.83                   | 0.0013                    |

Grain Diameter = K\*(SQRT(L/T))

Data entered by: MLM Data checked by: All FileName: LKHY04Z2

Date: 11/07/2012 Date: 11/7/12





| CLIENT LATA Kent   | ucky  | JOB NO. 2855-6   |   |
|--|---|--|---|
| BORING NO.<br>DEPTH<br>SAMPLE NO.<br>SOIL DESCR.<br>LOCATION | 211-B-004<br>36-38'<br>211B004GRNSZ3<br>ERI12-SW-SWMU211B<br>SW Plume RDSI Geotechnical | SAMPLED<br>DATE TESTED<br>WASH SIEVE<br>DRY SIEVE        | 10/11/12 KD<br>11/5/12 SKL<br>Yes<br>No |
| MOISTURE DATA  |   | WASH SIEVE ANALY   | SIS                                     |
| HYGROSCOPIC  | Yes   | Wt. Total Sample<br>Wet (g)                              | 1104.43                                 |
| NATURAL  | No  | Weight of + #10<br>Before Washing (g)<br>Weight of + #10 | 3.63                                    |
| Wt. Wet Soil & Pan (g)<br>Wt. Dry Soil & Pan (g)             | 78.44<br>77.30  | After Washing (g)<br>Weight of - #10                     | 3.41                                    |
| Wt. Lost Moisture (g)<br>Wt. of Pan Only (g)                 | 1.14<br>3.07  | Wet (g)<br>Weight of - #10                               | 1100.80                                 |
| Wt. of Dry Soil (g)<br>Moisture Content %                    | 74.23<br>1.5  | Dry (g)<br>Wt. Total Sample                              | 1084.37                                 |
|  |   | Dry (g)  | 1087.78                                 |
| Wt. Hydrom. Sample W   |   | Calc. Wt. "W" (g)  | 62.18                                   |
| Wt. Hydrom. Sample D   | ry (g) 61.98  | Calc. Mass + #10   | 0.19                                    |

| Sieve<br>Number<br>(Size) | Pan<br>Weight<br>(g) | Indiv.<br>Wt. + Pan<br>(g) | Indiv.<br>Wt.<br>Retain. | Cum.<br>Wt.<br>Retain. | Cum.<br>%<br>Retain. | %<br>Finer<br>By Wt. |
|---------------------------|----------------------|----------------------------|--------------------------|------------------------|----------------------|----------------------|
| 3"                        | 0.00                 | 0.00                       | 0.00                     | 0.00                   | 0.0                  | 100.0                |
| 1 1/2"                    | 0.00                 | 0.00                       | 0.00                     | 0.00                   | 0.0                  | 100.0                |
| 3/4"                      | 0.00                 | 0.00                       | 0.00                     | 0.00                   | 0.0                  | 100.0                |
| 3/8"                      | 0.00                 | 0.00                       | 0.00                     | 0.00                   | 0.0                  | 100.0                |
| #4                        | 0.00                 | 1.45                       | 1.45                     | 1.45                   | 0.1                  | 99.9                 |
| #10                       | 0.00                 | 1.96                       | 1.96                     | 3.41                   | 0.3                  | 99.7                 |
|                           | 0.00                 |                            | 0.00                     | 0.00                   | 0.0                  | 00.0                 |
| #20                       | 2.99                 | 3.32                       | 0.33                     | 0.33                   | 0.8                  | 99.2                 |
| #40                       | 3.01                 | 4.82                       | 1.81                     | 2.14                   | 3.8                  | 96.2                 |
| #60                       | 3.10                 | 7.97                       | 4.87                     | 7.01                   | 11.6                 | 88.4                 |
| #100                      | 2.98                 | 9.11                       | 6.12                     | 13.13                  | 21.4                 | 78.6                 |
| #200                      | 2.97                 | 7.89                       | 4.91                     | 18.04                  | 29.3                 | 70.7                 |

Data entered by: MLM Data checked by: <u>MLM</u> FileName: LKHY04Z3

Date: 11/07/2012 Date: 11/7/12



| CLIENT LATA K  | entucky   | JOB NO. 2855-6  |   |
|--|---|---|---|
| BORING NO.<br>DEPTH<br>SAMPLE NO.<br>SOIL DESCR.<br>LOCATION   | 211-B-004<br>36-38'<br>211B004GRNSZ3<br>ERI12-SW-SWMU211B<br>SW Plume RDSI Geotechnical | SAMPLED<br>DATE TESTED<br>WASH SIEVE<br>DRY SIEVE                         | 10/11/12 KD<br>11/5/12 SKL<br>Yes<br>No |
| Hydrometer #<br>Sp. Gr. of Soil<br>Value of "alpha"<br>Deflocculant<br>Defloc. Corr'n<br>Meniscus Corr'n | ASTM 152 H<br>2.65<br>1.00<br>Sodium Hexametaphosphate<br>5.0<br>0.0                    | Temp., Deg. C<br>Temp. Coef. K<br>Wt. Dry Sample "W"<br>% of Total Sample | 22.7<br>0.01322<br>62.176<br>100.0      |

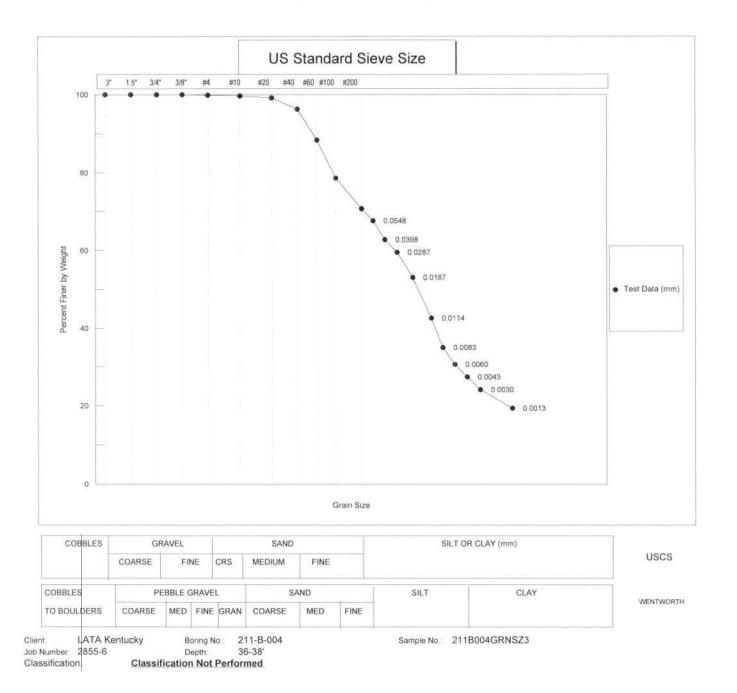
| т       |            |           |         |        |           |          |
|---------|------------|-----------|---------|--------|-----------|----------|
| Elapsed | Hydrometer | Reading   |         | %      | Effective | Grain    |
| Time    | Original   | Corrected |         | Total  | Depth     | Diameter |
| (min)   |            | "R"       | 100Ra/W | Sample | L         | (mm)     |
| 0.0     | -          |           |         |        |           |          |
| 0.5     | 47.00      | 42.00     | 67.6    | 67.6   | 8.58      | 0.0548   |
| 1.0     | 44.00      | 39.00     | 62.7    | 62.7   | 9.07      | 0.0398   |
| 2.0     | 42.00      | 37.00     | 59.5    | 59.5   | 9.40      | 0.0287   |
| 5.0     | 38.00      | 33.00     | 53.1    | 53.1   | 10.06     | 0.0187   |
| 15.0    | 31.50      | 26.50     | 42.6    | 42.6   | 11.12     | 0.0114   |
| 30.0    | 26.75      | 21.75     | 35.0    | 35.0   | 11.90     | 0.0083   |
| 60.0    | 24.00      | 19.00     | 30.6    | 30.6   | 12.35     | 0.0060   |
| 120.0   | 22.00      | 17.00     | 27.3    | 27.3   | 12.68     | 0.0043   |
| 250.0   | 20.00      | 15.00     | 24.1    | 24.1   | 13.01     | 0.0030   |
| 1440.0  | 17.00      | 12.00     | 19.3    | 19.3   | 13.50     | 0.0013   |

Grain Diameter = K\*(SQRT(L/T))

Data entered by: MLM Data checked by:\_\_\_\_\_ FileName: LKHY04Z3 Date: 11/07/2012 Date:\_\_\_\_\_ AT T

F-101

11



| BORING NO.<br>DEPTH211-B-001<br>8.0-10.0'SAMPLED<br>DATE TESTED10/9/12 MK<br>DATE TESTEDSAMPLE NO.<br>SOIL DESCR.<br>LOCATION211B001GRNSZ1<br>ERI12-SW-SWMU211B<br>SW Plume RDSI GeotechnicalWASH SIEVE<br>DRY SIEVEYes<br>NoMOISTURE DATAVASH SIEVE ANALYSISHYGROSCOPIC<br>NATURALYes<br>NoWt. Total Sample<br>Wet (g)103.70<br>103.70<br>Weight of + #10<br>Before Washing (g)Wt. Wet Soil & Pan (g)36.85<br>36.27After Washing (g)<br>Weight of - #10<br>Weight of - #100.00<br>Weight of - #10<br>Weight of - #10 |
|---|
| HYGROSCOPIC         Yes         Wt. Total Sample<br>Wet (g)         103.70           NATURAL         No         Weight of + #10<br>Before Washing (g)         0.00<br>Weight of + #10           Wt. Wet Soil & Pan (g)         36.85         After Washing (g)         0.00           Wt. Dry Soil & Pan (g)         36.27         Weight of - #10  |
| HYGROSCOPIC         Yes         Wt. Total Sample<br>Wet (g)         103.70           NATURAL         No         Weight of + #10<br>Before Washing (g)         0.00<br>Weight of + #10           Wt. Wet Soil & Pan (g)         36.85         After Washing (g)         0.00           Wt. Dry Soil & Pan (g)         36.27         Weight of - #10  |
| Wet (g)         103.70           NATURAL         No         Weight of + #10           Before Washing (g)         0.00           Weight of + #10         0.00           Weight of + #10         0.00           Wt. Wet Soil & Pan (g)         36.85         After Washing (g)         0.00           Wt. Dry Soil & Pan (g)         36.27         Weight of - #10         0.00   |
| NATURAL         No         Weight of + #10           Before Washing (g)         0.00           Weight of + #10         Weight of + #10           Wt. Wet Soil & Pan (g)         36.85         After Washing (g)         0.00           Wt. Dry Soil & Pan (g)         36.27         Weight of - #10         0.00  |
| Before Washing (g)         0.00           Weight of + #10         Weight of + #10           Wt. Wet Soil & Pan (g)         36.85         After Washing (g)         0.00           Wt. Dry Soil & Pan (g)         36.27         Weight of - #10         0.00   |
| Wt. Wet Soil & Pan (g)         36.85         After Washing (g)         0.00           Wt. Dry Soil & Pan (g)         36.27         Weight of - #10         0.00   |
|   |
| VA/t Lost Maisture (a) 0.59 VAlat (a)   |
| Wt. Lost Moisture (g) 0.58 Wet (g) 103.70   |
| Wt. of Pan Only (g) 3.02 Weight of - #10  |
| Wt. of Dry Soil (g) 33.25 Dry (g) 101.92  |
| Moisture Content % 1.7 Wt. Total Sample   |
| Dry (g) 101.92  |
| Wt. Hydrom. Sample Wet (g)         69.89         Calc. Wt. "W" (g)         68.69  |
| Wt. Hydrom. Sample Dry (g)         68.69         Calc. Mass + #10         0.00  |

| Sieve<br>Number<br>(Size) | Pan<br>Weight<br>(g) | Indiv.<br>Wt. + Pan<br>(g) | Indiv.<br>Wt.<br>Retain. | Cum.<br>Wt.<br>Retain. | Cum.<br>%<br>Retain. | %<br>Finer<br>By Wt. |
|---------------------------|----------------------|----------------------------|--------------------------|------------------------|----------------------|----------------------|
| 3"                        | 0.00                 | 0.00                       | 0.00                     | 0.00                   | 0.0                  | 100.0                |
| 1 1/2"                    | 0.00                 | 0.00                       | 0.00                     | 0.00                   | 0.0                  | 100.0                |
| 3/4"                      | 0.00                 | 0.00                       | 0.00                     | 0.00                   | 0.0                  | 100.0                |
| 3/8"                      | 0.00                 | 0.00                       | 0.00                     | 0.00                   | 0.0                  | 100.0                |
| #4                        | 0.00                 | 0.00                       | 0.00                     | 0.00                   | 0.0                  | 100.0                |
| #10                       | 0.00                 | 0.00                       | 0.00                     | 0.00                   | 0.0                  | 100.0                |
| #20                       | 2.98                 | 3.01                       | 0.03                     | 0.03                   | 0.0                  | 100.0                |
| #20                       | 3.13                 | 3.33                       | 0.03                     | 0.03                   | 0.0                  | 99.7                 |
| #40                       | 3.04                 | 3.97                       | 0.20                     | 1.16                   | 1.7                  | 99.7                 |
|                           | E10.3                |                            |                          |                        |                      |                      |
| #100                      | 2.98                 | 4.62                       | 1.64                     | 2.80                   | 4.1                  | 95.9                 |
| #200                      | 3.04                 | 4.07                       | 1.03                     | 3.83                   | 5.6                  | 94.4                 |

Data entered by: MLM Data checked by: Jul FileName: LKHY01Z1 Date: 11/12/2012 Date: 11/12/12



| CLIENT LATA   | Kentucky   | JOB NO. 2855-6  |  |
|---|--|---|--|
| BORING NO.<br>DEPTH<br>SAMPLE NO.<br>SOIL DESCR.<br>LOCATION  | 211-B-001<br>8.0-10.0'<br>211B001GRNSZ1<br>ERI12-SW-SWMU211B<br>SW Plume RDSI Geotechnical | SAMPLED<br>DATE TESTED<br>WASH SIEVE<br>DRY SIEVE                         | 10/9/12 MK<br>11/8/12 SKL<br>Yes<br>No |
| ×.  |  |   | 2                                      |
| Hydrometer <b>#</b><br>Sp. Gr. of Soil<br>Value of "alpha"<br>Deflocculant<br>Defloc. Corr'n<br>Meniscus Corr'n | ASTM 152 H<br>2.65<br>1.00<br>Sodium Hexametaphosphate<br>5.0<br>0.0                       | Temp., Deg. C<br>Temp. Coef. K<br>Wt. Dry Sample "W"<br>% of Total Sample | 22.7<br>0.01322<br>68.687<br>100.0     |

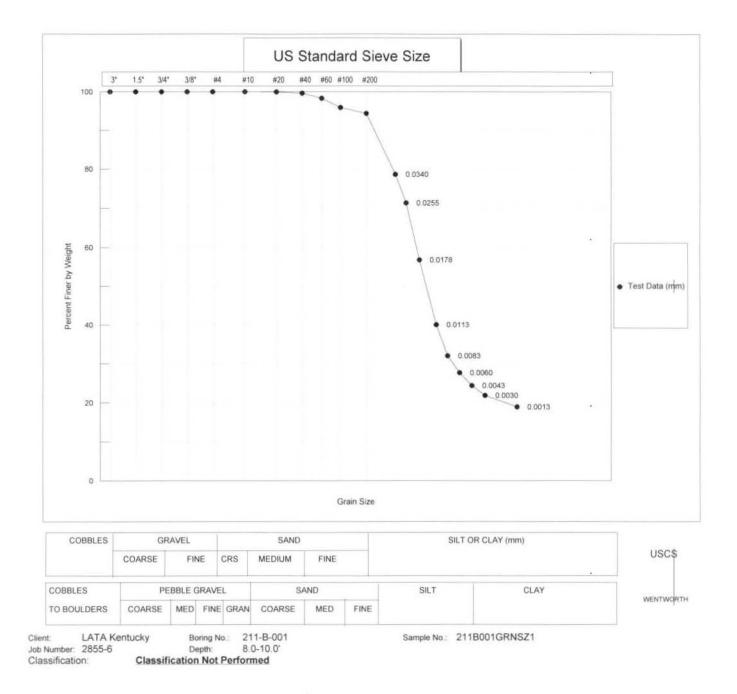
### Т

| Elapsed<br>Time<br>(min) | Hydrometer<br>Original | Reading<br>Corrected<br>"R" | 100Ra/W | %<br>Total<br>Sample | Effective<br>Depth<br>L | Grain<br>Diameter<br>(mm) |
|--------------------------|------------------------|-----------------------------|---------|----------------------|-------------------------|---------------------------|
| 0.0                      | -                      |                             |         | -                    |                         |                           |
| 0.5                      |                        |                             |         | -                    |                         |                           |
| 1.0                      | 59.00                  | 54.00                       | 78.6    | 78.6                 | 6.61                    | 0.0340                    |
| 2.0                      | 54.00                  | 49.00                       | 71.3    | 71.3                 | 7.43                    | 0.0255                    |
| 5.0                      | 44.00                  | 39.00                       | 56.8    | 56.8                 | 9.07                    | 0.0178                    |
| 15.0                     | 32.50                  | 27.50                       | 40.0    | 40.0                 | 10.96                   | 0.0113                    |
| 30.0                     | 27.00                  | 22.00                       | 32.0    | 32.0                 | 11.86                   | 0.0083                    |
| 60.0                     | 24.00                  | 19.00                       | 27.7    | 27.7                 | 12.35                   | 0.0060                    |
| 120.0                    | 21.75                  | 16.75                       | 24.4    | 24.4                 | 12.72                   | 0.0043                    |
| 250.0                    | 20.00                  | 15.00                       | 21.8    | 21.8                 | 13.01                   | 0.0030                    |
| 1440.0                   | 18.00                  | 13.00                       | 18.9    | 18.9                 | 13.34                   | 0.0013                    |

Grain Diameter = K\*(SQRT(L/T))

Data entered by: MLM Date: Data checked by: AL Date: FileName: LKHY01Z1





| CLIENT LATA K  | entucky   |  | JOB NO. 2855-6                                    |  |
|--|-----------|--|---|--|
| BORING NO.<br>DEPTH<br>SAMPLE NO.<br>SOIL DESCR.<br>LOCATION |           | RNSZ2<br>SWMU211B<br>RDSI Geotechnical | SAMPLED<br>DATE TESTED<br>WASH SIEVE<br>DRY SIEVE | 10/9/12 MK<br>11/8/12 SKL<br>Yes<br>No |
|  |           |  |   |  |
| MOISTURE DATA  |           |  | WASH SIEVE ANALY                                  | SIS                                    |
| HYGROSCOPIC  | Yes       |  | Wt. Total Sample                                  | 1002.47                                |
| NATURAL  | No        |  | Wet (g)<br>Weight of + #10                        | 1093.47                                |
|  |           |  | Before Washing (g)<br>Weight of + #10             | 545.18                                 |
| Wt. Wet Soil & Pan<br>Wt. Dry Soil & Pan                     |           | 35.10<br>34.56                         | After Washing (g)<br>Weight of - #10              | 493.40                                 |
| Wt. Lost Moisture (<br>Wt. of Pan Only (                     | g)        | 0.54                                   | Wet (g)<br>Weight of - #10                        | 548.29                                 |
| Wt. of Dry Soil (g)<br>Moisture Content %                    |           | 31.56<br>1.7                           | Dry (g)<br>Wt. Total Sample                       | 589.98                                 |
| worstore content 70  |           | 1.7                                    | Dry (g)   | 1083.38                                |
| Wt. Hydrom. Sample   | e Wet (g) | 90.81                                  | Calc. Wt. "W" (g)                                 | 163.96                                 |
| Wt. Hydrom. Sample   |           | 89.29                                  | Calc. Mass + #10                                  | 74.67                                  |

| Sieve<br>Number<br>(Size) | Pan<br>Weight<br>(g) | Indiv.<br>Wt. + Pan<br>(g) | Indiv.<br>Wt.<br>Retain. | Cum.<br>Wt.<br>Retain. | Cum.<br>%<br>Retain. | %<br>Finer<br>By Wt. |
|---------------------------|----------------------|----------------------------|--------------------------|------------------------|----------------------|----------------------|
| 3"                        | 0.00                 | 0.00                       | 0.00                     | 0.00                   | 0.0                  | 100.0                |
| 1 1/2"                    | 0.00                 | 0.00                       | 0.00                     | 0.00                   | 0.0                  | 100.0                |
| 3/4"                      | 0.00                 | 24.39                      | 24.39                    | 24.39                  | 2.3                  | 97.7                 |
| 3/8"                      | 0.00                 | 170.78                     | 170.78                   | 195.17                 | 18.0                 | 82.0                 |
| #4                        | 0.00                 | 176.89                     | 176.89                   | 372.06                 | 34.3                 | 65.7                 |
| #10                       | 0.00                 | 121.34                     | 121.34                   | 493.40                 | 45.5                 | 54.5                 |
| #20                       | 3.21                 | 15 50                      | 12.31                    | 12.31                  | 52.0                 | 47.0                 |
|                           |                      | 15.52                      |                          |                        | 53.0                 | 47.0                 |
| #40                       | 3.04                 | 18.65                      | 15.60                    | 27.91                  | 62.6                 | 37.4                 |
| #60                       | 3.04                 | 16.91                      | 13.87                    | 41.78                  | 71.0                 | 29.0                 |
| #100                      | 3.03                 | 8.86                       | 5.83                     | 47.61                  | 74.6                 | 25.4                 |
| #200                      | 3.00                 | 5.70                       | 2.70                     | 50.31                  | 76.2                 | 23.8                 |

Data entered by: MLM Data checked by: MLM FileName: LKHY01Z2



| CLIENT LATA K   | entucky   | JOB NO. 2855-6  |  |
|---|---|---|--|
| BORING NO.<br>DEPTH<br>SAMPLE NO.<br>SOIL DESCR.<br>LOCATION        | 211-B-001<br>18.0-20.0'<br>211B001GRNSZ2<br>ERI12-SW-SWMU211B<br>SW Plume RDSI Geotechnical | SAMPLED<br>DATE TESTED<br>WASH SIEVE<br>DRY SIEVE                         | 10/9/12 MK<br>11/8/12 SKL<br>Yes<br>No |
|   |   |   |  |
| Hydrometer #<br>Sp. Gr. of Soil<br>Value of "alpha"<br>Deflocculant | ASTM 152 H<br>2.65<br>1.00<br>Sodium Hexametaphosphate                                      | Temp., Deg. C<br>Temp. Coef. K<br>Wt. Dry Sample "W"<br>% of Total Sample | 22.6<br>0.01323<br>163.957<br>100.0    |
| Defloc. Corr'n<br>Meniscus Corr'n                                   | 5.0<br>0.0  |   |  |

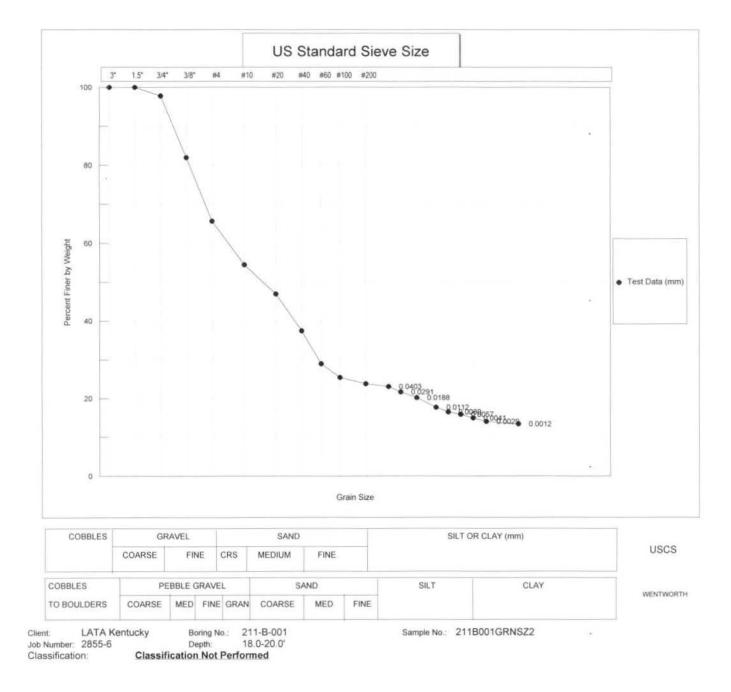
#### т

| Elapsed<br>Time<br>(min) | Hydrometer<br>Original | Reading<br>Corrected<br>"R" | 100Ra/W | %<br>Total<br>Sample | Effective<br>Depth<br>L | Grain<br>Diameter<br>(mm) |
|--------------------------|------------------------|-----------------------------|---------|----------------------|-------------------------|---------------------------|
| 0.0                      |                        |                             |         | -                    |                         |                           |
| 0.5                      |                        |                             |         | -                    |                         |                           |
| 1.0                      | 42.75                  | 37.75                       | 23.0    | 23.0                 | 9.28                    | 0.0403                    |
| 2.0                      | 40.50                  | 35.50                       | 21.7    | 21.7                 | 9.65                    | 0.0291                    |
| 5.0                      | 38.00                  | 33.00                       | 20.1    | 20.1                 | 10.06                   | 0.0188                    |
| 15.0                     | 34.00                  | 29.00                       | 17.7    | 17.7                 | 10.71                   | 0.0112                    |
| 30.0                     | 32.00                  | 27.00                       | 16.5    | 16.5                 | 11.04                   | 0.0080                    |
| 60.0                     | 31.00                  | 26.00                       | 15.9    | 15.9                 | 11.21                   | 0.0057                    |
| 120.0                    | 29.50                  | 24.50                       | 14.9    | 14.9                 | 11.45                   | 0.0041                    |
| 250.0                    | 28.00                  | 23.00                       | 14.0    | 14.0                 | 11.70                   | 0.0029                    |
| 1440.0                   | 27.00                  | 22.00                       | 13.4    | 13.4                 | 11.86                   | 0.0012                    |

Grain Diameter = K\*(SQRT(L/T))

Data entered by: MLM Data checked by: Chill FileName: LKHY01Z2





F-108

1

| CLIENT LATA Ken  | tucky   | JOB NO. 2855-6   |  |  |
|--|---|--|--|--|
| BORING NO.<br>DEPTH<br>SAMPLE NO.<br>SOIL DESCR.<br>LOCATION | 211-B-001<br>38.0-40.0'<br>211B001GRNSZ3<br>ERI12-SW-SWMU211B<br>SW Plume RDSI Geotechnical | SAMPLED<br>DATE TESTED<br>WASH SIEVE<br>DRY SIEVE        | 10/9/12 MK<br>11/5/12 SKL<br>Yes<br>No |  |
| MOISTURE DATA  |   | WASH SIEVE ANALYS  | IS                                     |  |
| HYGROSCOPIC  | Yes   | Wt. Total Sample<br>Wet (g)                              | 1383.18                                |  |
| NATURAL  | No  | Weight of + #10<br>Before Washing (g)<br>Weight of + #10 | 18.17                                  |  |
| Wt. Wet Soil & Pan (g)<br>Wt. Dry Soil & Pan (g)             | 58.82<br>58.15  | After Washing (g)<br>Weight of - #10                     | 16.14                                  |  |
| Wt. Lost Moisture (g)<br>Wt. of Pan Only (g)                 | 0.67<br>3.07  | Wet (g)<br>Weight of - #10                               | 1365.01                                |  |
| Wt. of Dry Soil (g)<br>Moisture Content %                    | 55.08<br>1.2  | Dry (g)<br>Wt. Total Sample                              | 1350.61                                |  |
|  |   | Dry (g)  | 1366.75                                |  |
| Wt. Hydrom. Sample V   |   | Calc. Wt. "W" (g)  | 64.24                                  |  |
| Wt. Hydrom. Sample D   | ry (g) 63.48  | Calc. Mass + #10 0                                       |  |  |

| Sieve<br>Number<br>(Size) | Pan<br>Weight<br>(g) | Indiv.<br>Wt. + Pan<br>(g) | Indiv.<br>Wt.<br>Retain. | Cum.<br>Wt.<br>Retain. | Cum.<br>%<br>Retain. | %<br>Finer<br>By Wt. |
|---------------------------|----------------------|----------------------------|--------------------------|------------------------|----------------------|----------------------|
| 3"                        | 0.00                 | 0.00                       | 0.00                     | 0.00                   | 0.0                  | 100.0                |
| 1 1/2"                    | 0.00                 | 0.00                       | 0.00                     | 0.00                   | 0.0                  | 100.0                |
| 3/4"                      | 0.00                 | 0.00                       | 0.00                     | 0.00                   | 0.0                  | 100.0                |
| 3/8"                      | 0.00                 | 0.00                       | 0.00                     | 0.00                   | 0.0                  | 100.0                |
| #4                        | 0.00                 | 7.63                       | 7.63                     | 7.63                   | 0.6                  | 99.4                 |
| #10                       | 0.00                 | 8.51                       | 8.51                     | 16.14                  | 1.2                  | 98.8                 |
|                           |                      |                            |                          |                        |                      |                      |
| #20                       | 3.08                 | 3.85                       | 0.77                     | 0.77                   | 2.4                  | 97.6                 |
| #40                       | 3.05                 | 6.59                       | 3.54                     | 4.31                   | 7.9                  | 92.1                 |
| #60                       | 3.02                 | 9.23                       | 6.21                     | 10.52                  | 17.6                 | 82.4                 |
| #100                      | 3.02                 | 12.10                      | 9.09                     | 19.61                  | 31.7                 | 68.3                 |
| #200                      | 3.08                 | 10.36                      | 7.29                     | 26.89                  | 43.0                 | 57.0                 |

Data entered by: MLM Data checked by: JU FileName: LKHY01Z3

Date: 11/07/2012 Date: 11/7/12



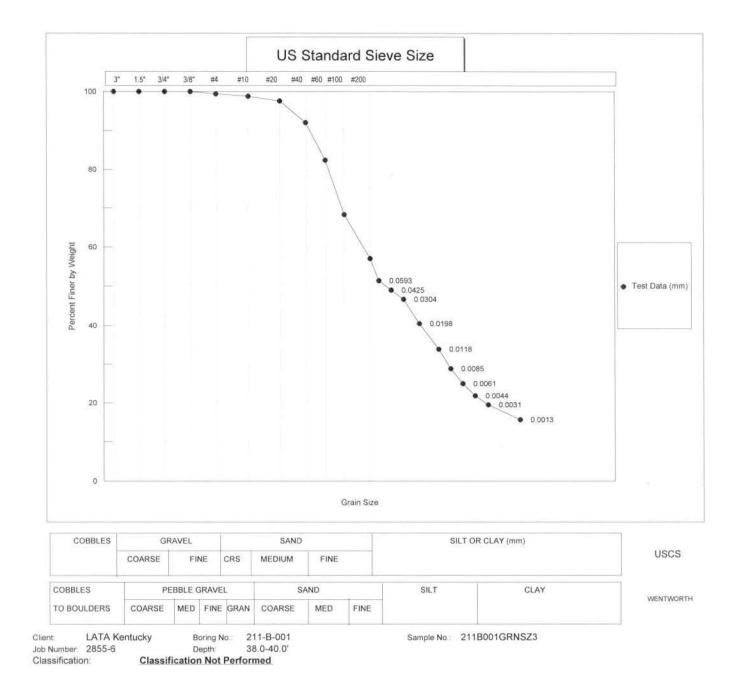
| BORING NO.<br>DEPTH         211-B-001<br>38.0-40.0'         SAMPLE D<br>211B001GRNSZ3         SAMPLE D<br>211B001GRNSZ3         10/9/12 MK<br>11/5/12 SKL           SAMPLE NO.<br>SOIL DESCR.         ERI12-SW-SWMU211B<br>SW Plume RDSI Geotechnical         DATE TESTED<br>DRY SIEVE         11/5/12 SKL<br>Yes           Hydrometer #<br>LOCATION         ASTM 152 H<br>Sodium Hexametaphosphate         Temp., Deg. C<br>Temp. Coef. K         22.6<br>0.01323           Value of "alpha"         1.00         Wt. Dry Sample "W"         64.239           Deflocc. Corr'n         5.0         Wt. Dry Sample<"W"         64.239           Meniscus Corr'n         0.0         Total         Sample         Diameter<br>L         (mm)           0.0         -         -         -         -         -         -           0.0         -         -         -         -         -         -           0.0         -         -         -         -         -         -           0.0         -         -         -         -         -         -           0.0         -         -         -         -         -         -           100Ra/W         Sample         Depth         Diameter<br>L         (mm)         -         -           0.0         -         -  | CLIENT   | LATA Kent               | ucky   |          |        | JOB NO.                   | 2855-6          |                    |
|---|--|-------------------------|--|----------|--------|---------------------------|-----------------|--------------------|
| Sp. Gr. of Soil       2.65       Temp. Coef. K       0.01323         Value of "alpha"       1.00       Wt. Dry Sample "W"       64.239         Deflocculant       Sodium Hexametaphosphate       % of Total Sample       100.0         Defloc. Corr'n       5.0       5.0       Meniscus Corr'n       0.0         Meniscus Corr'n       0.0       64.239       100.0         0       Image: Corrected test of the system of the | DEPTH<br>SAMPLE NO<br>SOIL DESC  | D.                      | 38.0-40.0'<br>211B001GR<br>ERI12-SW-S  | SWMU211B | nical  | DATE TEST<br>WASH SIEV    | /E              | 11/5/12 SKL<br>Yes |
| Elapsed<br>Time<br>(min)         Hydrometer Reading<br>Original         %<br>Corrected<br>"R"         Effective<br>100Ra/W         Effective<br>Sample         Grain<br>Depth         Diameter<br>(mm)           0.0         -  | Sp. Gr. of S<br>Value of "alp<br>Deflocculan<br>Defloc. Corr<br>Meniscus C | oil<br>oha''<br>t<br>'n | 2.65<br>1.00<br>Sodium Hex<br>5.0  |          | ate    | Temp. Coef<br>Wt. Dry San | . K<br>nple "W" | 0.01323<br>64.239  |
| Time<br>(min)Original<br>"R"Corrected<br>"R"Total<br>100Ra/WDepth<br>SampleDiameter<br>L0.00.538.0033.0051.451.410.060.05931.036.5031.5049.049.010.300.04252.035.0030.0046.746.710.550.03045.031.0026.0040.540.511.210.019815.026.7521.7533.933.911.900.011830.023.5018.5028.828.812.440.008560.021.0016.0024.924.912.850.0061120.019.0014.0021.821.813.170.0044250.017.5012.5019.519.513.420.0031  | · · · · · · · · · · · · · · · · · · ·                                      | Hvdrometer              | Reading  |          | %      | Effective                 | Grain           |                    |
| (min)         "R"         100Ra/W         Sample         L         (mm)           0.0         -   |  |                         |  |          | Total  | Depth                     | Diameter        |                    |
| 0.538.0033.0051.451.410.060.05931.036.5031.5049.049.010.300.04252.035.0030.0046.746.710.550.03045.031.0026.0040.540.511.210.019815.026.7521.7533.933.911.900.011830.023.5018.5028.828.812.440.008560.021.0016.0024.924.912.850.0061120.019.0014.0021.821.813.170.0044250.017.5012.5019.519.513.420.0031   | (min)  |                         | "R"  | 100Ra/W  | Sample | L                         | (mm)            |                    |
| 0.538.0033.0051.451.410.060.05931.036.5031.5049.049.010.300.04252.035.0030.0046.746.710.550.03045.031.0026.0040.540.511.210.019815.026.7521.7533.933.911.900.011830.023.5018.5028.828.812.440.008560.021.0016.0024.924.912.850.0061120.019.0014.0021.821.813.170.0044250.017.5012.5019.519.513.420.0031   | 0.0  |                         |  |          | -      |                           | _               |                    |
| 1.036.5031.5049.049.010.300.04252.035.0030.0046.746.710.550.03045.031.0026.0040.540.511.210.019815.026.7521.7533.933.911.900.011830.023.5018.5028.828.812.440.008560.021.0016.0024.924.912.850.0061120.019.0014.0021.821.813.170.0044250.017.5012.5019.519.513.420.0031   |  | 38.00                   | 33.00  | 51.4     | 51.4   | 10.06                     | 0.0593          |                    |
| 2.035.0030.0046.746.710.550.03045.031.0026.0040.540.511.210.019815.026.7521.7533.933.911.900.011830.023.5018.5028.828.812.440.008560.021.0016.0024.924.912.850.0061120.019.0014.0021.821.813.170.0044250.017.5012.5019.519.513.420.0031   |  |                         |  |          |        |                           |                 |                    |
| 5.031.0026.0040.540.511.210.019815.026.7521.7533.933.911.900.011830.023.5018.5028.828.812.440.008560.021.0016.0024.924.912.850.0061120.019.0014.0021.821.813.170.0044250.017.5012.5019.519.513.420.0031   |  |                         |  |          |        |                           |                 |                    |
| 15.026.7521.7533.933.911.900.011830.023.5018.5028.828.812.440.008560.021.0016.0024.924.912.850.0061120.019.0014.0021.821.813.170.0044250.017.5012.5019.519.513.420.0031   |  |                         |  |          |        |                           | (아파 아카 프로마 네가)  |                    |
| 30.023.5018.5028.828.812.440.008560.021.0016.0024.924.912.850.0061120.019.0014.0021.821.813.170.0044250.017.5012.5019.519.513.420.0031  |  |                         |  |          |        |                           |                 |                    |
| 60.021.0016.0024.924.912.850.0061120.019.0014.0021.821.813.170.0044250.017.5012.5019.519.513.420.0031   |  |                         |  |          |        |                           |                 |                    |
| 120.019.0014.0021.821.813.170.0044250.017.5012.5019.519.513.420.0031  |  |                         |  |          |        |                           |                 |                    |
| 250.0 17.50 12.50 19.5 19.5 13.42 0.0031  |  |                         |  |          |        |                           |                 |                    |
|   |  |                         | The second s |          |        |                           |                 |                    |
|   |  |                         | 10.00  |          |        |                           |                 |                    |

Grain Diameter = K\*(SQRT(L/T))

Data entered by: MLM Data checked by: MLM FileName: LKHY01Z3

Date: 11/07/2012 Date: 11





Permeability Tests

# ASTM D5084-10

Advanced Terra Testing

## PERMEABILITY TEST - BACK PRESSURE SATURATED - FLOW PUMP METHOD ASTM D 5084

| CLIENT   | LATA Env | ironmental Services of Ky  | JOB NO. 2855-06 |                  |
|----------|----------|----------------------------|-----------------|------------------|
| BORING N | 10.      | 211-B-001                  | SAMPLED         | 10/09/12 KD      |
| DEPTH    |          | 32.0-37.0' C               | TEST STARTED    | 11/21/12 CAL     |
| SAMPLE N | 10.      | 211B001PERM3               | TEST FINISHED   | 12/02/12 CAL     |
| SOIL DES | CR.      | ERI12-SW-SWMU211B          | CELL NUMBER     | 7P               |
| LOCATION | 4        | SW Plume RDSI Geotechnical | SATURATED TEST  | Yes              |
| CONF. PR | ES. PSF  | 4658                       | TEST TYPE       | TX/Pbp/Tap Water |

| MOISTURE/DENSITY<br>DATA   | BEFORE<br>TEST | AFTER<br>TEST |        |
|----------------------------|----------------|---------------|--------|
| Wt. Soil + Moisture (g)    | 211.1          | 206.3         |        |
| Wt. Wet Soil & Pan (g)     | 217.6          | 212.8         |        |
| Wt. Dry Soil & Pan (g)     | 182.3          | 182.3         |        |
| Wt. Lost Moisture (g)      | 35.3           | 30.5          |        |
| Wt. of Pan Only (g)        | 6.5            | 6.5           |        |
| Wt. of Dry Soil (g)        | 175.8          | 175.8         |        |
| Moisture Content %         | 20.1           | 17.4          |        |
| Wet Density PCF            | 130.2          | 136.9         |        |
| Dry Density PCF            | 108.4          | 116.6         |        |
| Init. Diameter (in)        | 1.613          | (cm)          | 4.097  |
| Init. Area (sq in)         | 2.043          | (sq cm)       | 13.184 |
| Init. Height (in)          | 3.022          | (cm)          | 7.676  |
| Vol. Bef. Consol. (cu ft)  | 0.00357        |               |        |
| Vol. After Consol. (cu ft) | 0.00332        |               |        |
| Porosity %                 | 32.41          |               |        |

## FLOW PUMP CALCULATIONS

| Pump Setting                  | 5        |
|-------------------------------|----------|
| Velocity CM/Sec               | 3.29E-05 |
| Q (cc/s)                      | 1.05E-06 |
| Height                        | 2.984    |
| Diameter                      | 1.565    |
| Pressure (psi)                | 4.740    |
| Area after consol. (cm*cm)    | 12.415   |
| Gradient                      | 43.969   |
| Permeability k (cm/s)         | 1.9E-09  |
| Permeability k (m/s)          | 1.9E-11  |
| Back Pressure (psi)           | 68.0     |
| Cell Pressure (psi)           | 100.3    |
| Ave. Effective Stress (psi)   | 29.930   |
| Average temperature degree C: | 22.4     |

| Data entry by:     | MLM           | Date: |
|--------------------|---------------|-------|
| Checked by: CH-    | Date: 12/4/12 |       |
| FileName: LKP00013 | - / /         |       |

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12/04/2012

# TRIAXAL COMPRESSION TEST DATA

| CLIENT LATA E   | nvironmental Services of Ky | JOB NO. 2855-06 |                  |
|-----------------|-----------------------------|-----------------|------------------|
| BORING NO.      | 211-B-001                   | SAMPLED         | 10/09/12 KD      |
| DEPTH           | 32.0-37.0' C                | TEST STARTED    | 11/21/12 CAL     |
| SAMPLE NO.      | 211B001PERM3                | TEST FINISHED   | 12/02/12 CAL     |
| SOIL DESCR.     | ERI12-SW-SWMU211B           | SETUP NO.       | 7P               |
| LOCATION        | SW Plume RDSI Geotechnical  | SATURATED TEST  | Yes              |
| CONF. PRES. PSF | 4658                        | TEST TYPE       | TX/Pbp/Tap Water |
|                 | *                           |                 |                  |

## SATURATION DATA

| Cell<br>Pres.<br>(PSI) | Back<br>Pres.<br>(PSI) | Burette<br>Reading<br>(CC) |      | Pore<br>Pressure<br>(PSI) | C    | Change | В    |
|------------------------|------------------------|----------------------------|------|---------------------------|------|--------|------|
|                        |                        | Close                      | Open | Close                     | Open |        |      |
| 40.0                   | 38.0                   | 1.5                        | 10.2 |                           |      |        |      |
| 50.0                   | 48.0                   | 14.4                       | 15.4 | 38.5                      | 47.8 | 9.3    | 0.93 |
| 60.0                   | 58.0                   | 16.2                       | 17.1 | 48.5                      | 57.9 | 9.4    | 0.94 |
| 70.0                   | 68.0                   | 17.3                       | 18.2 | 58.5                      | 67.8 | 9.3    | 0.93 |
| 80.0                   |                        | 18.9                       | 18.9 | 68.1                      | 77.9 | 9.8    | 0.98 |

# CONSOLIDATION DATA

| Elapsed | SQRT  | Burette        | Volume |
|---------|-------|----------------|--------|
| Time    | Time  | Reading        | Defl.  |
| (Min)   | (Min) | (CC)           | (cc)   |
| 0.00    | 0.00  | 0.30           | 0.00   |
| 0.25    | 0.50  | 3.00           | -2.70  |
| 0.5     | 0.71  | 3.10           | -2.80  |
| 1       | 1.00  | 3.15           | -2.85  |
| 2       | 1.41  | 3.20           | -2.90  |
| 4       | 2.00  | 3.30           | -3.00  |
| 9       | 3.00  | 3.50           | -3.20  |
| 16      | 4.00  | 3.70           | -3.40  |
| 30      | 5.48  | 3.90           | -3.60  |
| 60      | 7.75  | 4.50           | -4.20  |
| 138     | 11.75 | 5.30           | -5.00  |
| 240     | 15.49 | 6.10           | -5.80  |
| 360     | 18.97 | 6.80           | -6.50  |
|         |       |                |        |
|         | 3.022 | Init. Vol. (CC | C)     |
|         | 0.038 | Vol. Change    |        |
|         |       |                |        |

| Initial Height (in)      |
|--------------------------|
| Height Change (in)       |
| Ht. After Cons. (in)     |
| Initial Area (sq in)     |
| Area After Cons. (sq in) |



101.21

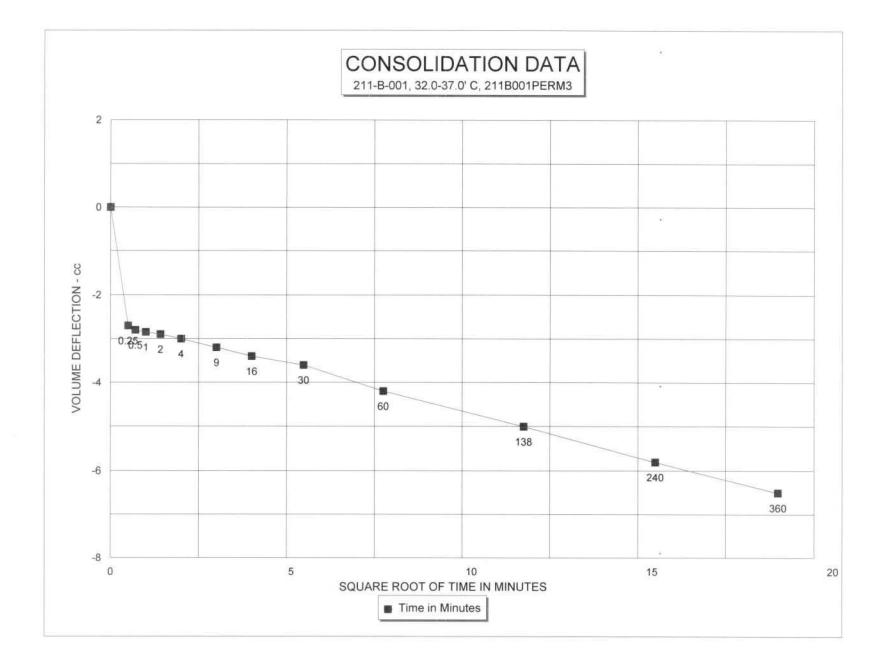
| Data entry by:     | MLM Date:     |
|--------------------|---------------|
| Checked by: etc.   | Date: 12/4/12 |
| FileName: LKP00013 |               |

12/04/2012

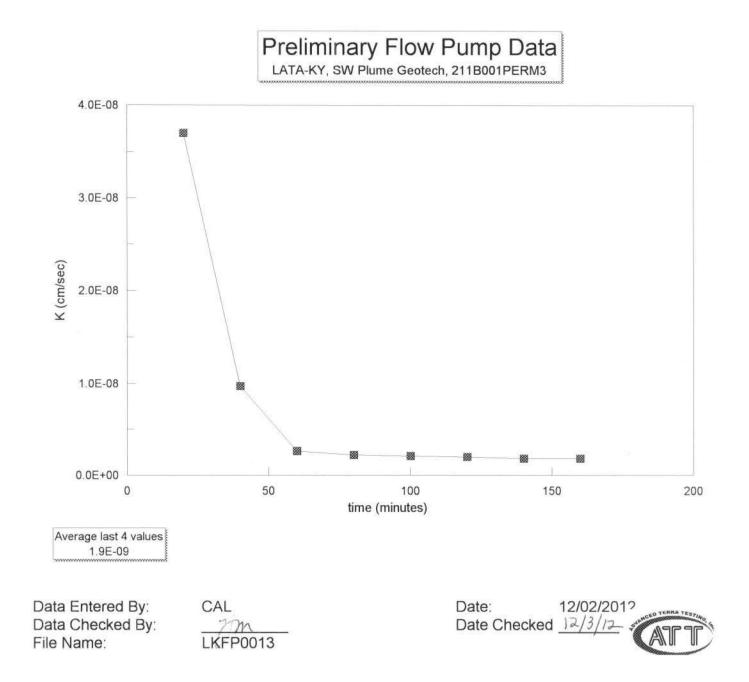
2.984

2.043

1.924



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Client LATTA ENV. SERVICES of KY Job No. 2855-06 Boring No. 211-8-001 Boring No. 211-B-001 Depth 35-37 C Sample No. 211BOOI PERM 3 Project SW Plume ROSI Geotechnical Sampled 1019 / 12 by KD Prepped 11 21 12 by CHE Project No. ERIZ-SW-SWMUZIB Tx/Pbp T3 4658 psf LK2855/LKDP0013 12/03/12

## PERMEABILITY TEST - BACK PRESSURE SATURATED - FLOW PUMP METHOD ASTM D 5084

| CLIENT LATA En  | vironmental Services of KY | JOB NO. 2855-06 |                  |
|-----------------|----------------------------|-----------------|------------------|
| BORING NO.      | 211-B-001                  | SAMPLED         | 10/09/12 KD      |
| DEPTH           | 5.0-7.0' B                 | TEST STARTED    | 11/14/12 CAL     |
| SAMPLE NO.      | 211B001PERM1               | TEST FINISHED   | 11/28/12 CAL     |
| SOIL DESCR.     | ERI12-SW-SWMU211B          | CELL NUMBER     | 9P               |
| LOCATION        | SW Plume RDSI Geotechnical | SATURATED TEST  | Yes              |
| CONF. PRES. PSF | 776                        | TEST TYPE       | TX/Pbp/Tap Water |

| BEFORE  | AFTER  |   |
|---------|--|---|
| TEST    | TEST   |   |
| 229.1   | 229.1  |   |
| 235.6   | 235.6  |   |
| 194.8   | 194.8  |   |
| 40.8    | 40.8   |   |
| 6.5     | 6.5  |   |
| 188.3   | 188.3  |   |
| 21.7    | 21.7   |   |
| 127.6   | 124.2  |   |
| 104.8   | 102.1  |   |
| 1.654   | (cm)   | 4.201   |
| 2.149   | (sq cm)  | 13.863  |
| 3.184   | (cm)   | 8.087   |
| 0.00396 |  |   |
| 0.00407 |  |   |
| 35.47   |  |   |
|         | TEST<br>229.1<br>235.6<br>194.8<br>40.8<br>6.5<br>188.3<br>21.7<br>127.6<br>104.8<br>1.654<br>2.149<br>3.184<br>0.00396<br>0.00407 | TEST         TEST           229.1         229.1           235.6         235.6           194.8         194.8           40.8         40.8           6.5         6.5           188.3         188.3           21.7         21.7           127.6         124.2           104.8         102.1           1.654         (cm)           2.149         (sq cm)           3.184         (cm)           0.00396         0.00407 |

## FLOW PUMP CALCULATIONS

| Pump Setting                  | 25       |
|-------------------------------|----------|
| Velocity CM/Sec               | 1.64E-04 |
| Q (cc/s)                      | 5.25E-06 |
| Height                        | 3.163    |
| Diameter                      | 1.682    |
| Pressure (psi)                | 1.160    |
| Area after consol. (cm*cm)    | 14.333   |
| Gradient                      | 10.151   |
| Permeability k (cm/s)         | 3.6E-08  |
| Permeability k (m/s)          | 3.6E-10  |
| Back Pressure (psi)           | 98.0     |
| Cell Pressure (psi)           | 103.4    |
| Ave. Effective Stress (psi)   | 4.820    |
| Average temperature degree C: | 22.5     |

## Average temperature degree C:

DAW Data entry by: Date: Checked by: \_\_\_\_\_\_ FileName: LKP00011 Date: 11/30/12

11/29/2012



## TRIAXAL COMPRESSION TEST DATA

| CLIENT LATA Env  | vironmental Services of KY   | JOB NO. 2855-06   |  |
|--|--|---|--|
| BORING NO.<br>DEPTH<br>SAMPLE NO.<br>SOIL DESCR.<br>LOCATION | 211-B-001<br>5.0-7.0' B<br>211B001PERM1<br>ERI12-SW-SWMU211B<br>SW Plume RDSI Geotechnical | SAMPLED<br>TEST STARTED<br>TEST FINISHED<br>SETUP NO.<br>SATURATED TEST | 10/09/12 KD<br>11/14/12 CAL<br>11/28/12 CAL<br>9P<br>Yes |
| CONF. PRES. PSF  | 776  | TEST TYPE   | TX/Pbp/Tap Water   |

#### SATURATION DATA

| Cell  | Back  | Burette |      | Pore     |       |        |   |      |
|-------|-------|---------|------|----------|-------|--------|---|------|
| Pres. | Pres. | Reading |      | Pressure |       |        |   |      |
| (PSI) | (PSI) | (CC)    |      | (PSI)    | (     | Change | В |      |
|       |       | Close   | Open | Close    | Open  |        |   |      |
| 40.0  | 38.0  | 4.1     | 9.3  |          |       |        |   |      |
| 50.0  | 48.0  | 9.8     | 11.0 | 38.7     | 47.0  | 8.3    |   | 0.83 |
| 60.0  | 58.0  | 11.0    | 11.9 | 48.8     | 57.1  | 8.3    |   | 0.83 |
| 70.0  | 68.0  | 12.0    | 12.9 | 58.6     | 67.1  | 8.5    |   | 0.85 |
| 80.0  | 78.0  | 13.6    | 14.4 | 68.7     | 77.6  | 8.9    |   | 0.89 |
| 90.0  | 88.0  | 14.7    | 15.5 | 78.7     | 88.0  | 9.3    |   | 0.93 |
| 100.0 | 98.0  | 15.4    | 16.2 | 88.7     | 97.9  | 9.2    |   | 0.92 |
| 110.0 |       | 16.3    | 16.4 | 98.7     | 108.2 | 9.5    |   | 0.95 |

## CONSOLIDATION DATA

|                          | Elapsed | SQRT  | Burette Volume   |
|--------------------------|---------|-------|------------------|
|                          | Time    | Time  | Reading Defl.    |
|                          | (Min)   | (Min) | (CC) (cc)        |
|                          | 0.00    | 0.00  | 16.40 0.00       |
|                          | 0.25    | 0.50  | 16.70 -0.30      |
|                          | 0.5     | 0.71  | 16.70 -0.30      |
|                          | 1       | 1.00  | 16.75 -0.35      |
|                          | 2       | 1.41  | 16.75 -0.35      |
|                          | 4       | 2.00  | 16.80 -0.40      |
|                          | 4<br>9  | 3.00  | 16.80 -0.40      |
|                          | 16      | 4.00  | 16.85 -0.45      |
|                          | 30      | 5.48  | 16.90 -0.50      |
|                          | 60      | 7.75  | 16.95 -0.55      |
|                          | 120     | 10.95 | 17.05 -0.65      |
|                          | 240     | 15.49 | 17.05 -0.65      |
|                          | 360     | 18.97 | 17.05 -0.65      |
| Initial Height (in)      |         | 3.184 | Init. Vol. (CC)  |
| Height Change (in)       |         | 0.021 | Vol. Change (CC) |
| Ht. After Cons. (in)     |         | 3.163 | Cell Exp. (CC)   |
| Initial Area (sq in)     |         | 2.149 | Net Change (CC)  |
| Area After Cons. (sq in) |         | 2.222 | Cons. Vol. (CC)  |
| (-1···)                  |         |       |                  |



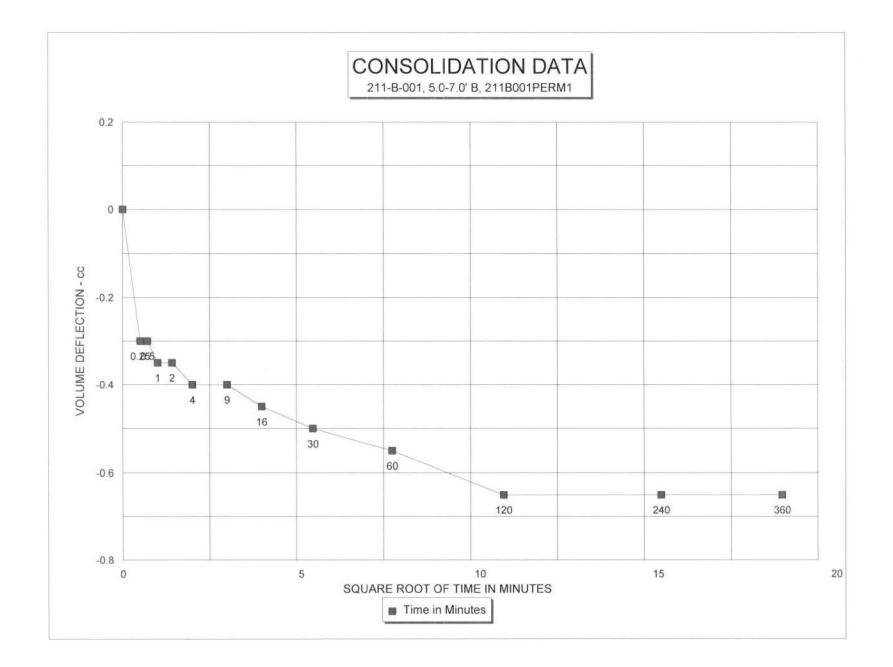
112.13 13.10 16.15

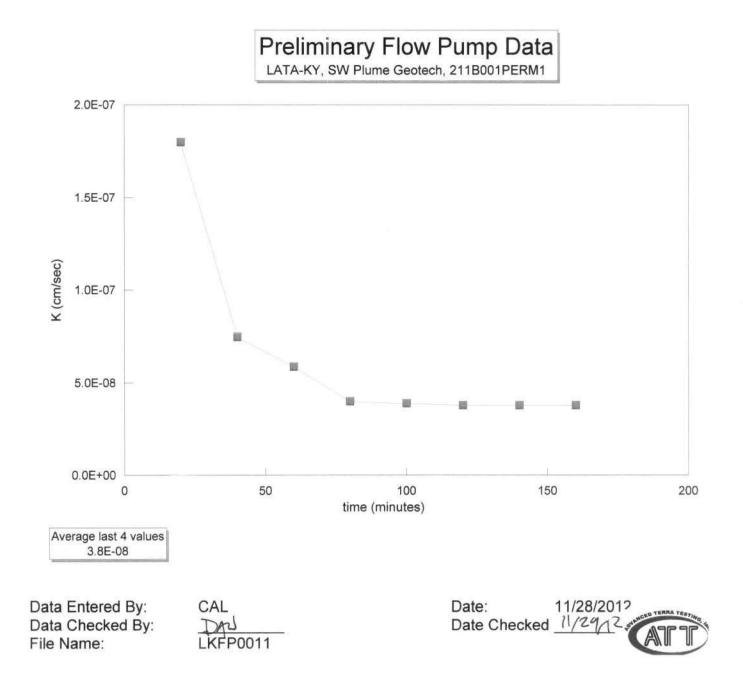
-3.05

115.18

| Data entry by:     | DAW          | Date:    |
|--------------------|--------------|----------|
| Checked by: On     | Date:        | 11/30/12 |
| FileName: LKP00011 | NO STITE CAR | / .      |

11/29/2012





Client LATA Environmental Services Job No. 2855-06 Boring No. 211-8-001 Depth 5.0-7.0' B Sample No. 2116001 PERM 1 Project SW Plume RDST Geotechnical Sampled 10/ 9 / 12 by KD Prepped 11 / 14 / 12 by cz Project No. ERIIZ-SW-SWMUZIB Tx/Pbp 5 76psf LK2855/LKDP0011 129/12

| CLIENT  | LATA Envir      | ronmental Services - KY  | JOB NO. 2855-06  |   |
|---|-----------------|--|--|---|
| BORING N<br>DEPTH<br>SAMPLE N<br>SOIL DES<br>LOCATION<br>CONF. PR | NO.<br>CR.<br>N | 211-B-001<br>15-17' A<br>211B001PERM2<br>ERI12-SW-SWMU211B<br>SW Plume RDSI Geotechnical<br>2070 | SAMPLED<br>TEST STARTED<br>TEST FINISHED<br>CELL NUMBER<br>SATURATED TEST<br>TEST TYPE | 10/09/12 KD<br>11/13/12 CAL<br>11/19/12 CAL<br>13S<br>Yes<br>TX/Pbp/Tap Water |

| MOISTURE/DENSITY           | BEFORE  | AFTER   |        |
|----------------------------|---------|---------|--------|
| DATA                       | TEST    | TEST    |        |
| Wt. Soil + Moisture (g)    | 231.9   | 237.0   |        |
| Wt. Wet Soil & Pan (g)     | 238.3   | 243.5   |        |
| Wt. Dry Soil & Pan (g)     | 214.3   | 214.3   |        |
| Wt. Lost Moisture (g)      | 24.1    | 29.2    |        |
| Wt. of Pan Only (g)        | 6.5     | 6.5     |        |
| Wt. of Dry Soil (g)        | 207.8   | 207.8   |        |
| Moisture Content %         | 11.6    | 14.1    |        |
| Wet Density PCF            | 134.0   | 140.1   |        |
| Dry Density PCF            | 120.1   | 122.8   |        |
| Init. Diameter (in)        | 1.617   | (cm)    | 4.107  |
| Init. Area (sq in)         | 2.054   | (sq cm) | 13.250 |
| Init. Height (in)          | 3.210   | (cm)    | 8.153  |
| Vol. Bef. Consol. (cu ft)  | 0.00381 |         |        |
| Vol. After Consol. (cu ft) | 0.00373 |         |        |
| Porosity %                 | 27.66   |         |        |

## FLOW PUMP CALCULATIONS

| Pump Setting (gear number)  | 9        |
|-----------------------------|----------|
| Percentage of Pump setting  | 100      |
| Q (cc/s)                    | 2.28E-04 |
| Height                      | 3.189    |
| Diameter                    | 1.604    |
| Pressure (psi)              | 0.716    |
| Area after consol. (cm*cm)  | 13.041   |
| Gradient                    | 6.215    |
| Permeability k (cm/s)       | 2.8E-06  |
| Permeability k (m/s)        | 2.8E-08  |
| Back Pressure (psi)         | 58.0     |
| Cell Pressure (psi)         | 72.4     |
| Ave. Effective Stress (psi) | 14.042   |

Average temperature degree C: 21.6 NOTE: Filling required on top, bottom and sides to fill gravel voids.

| Data entry by:     | DAW        | Date: | 11/26/2012 |
|--------------------|------------|-------|------------|
| Checked by:        | Date: ///z | 7/12  |            |
| FileName: LKP00012 | 1          |       |            |



| CLIENT LATA Env | vironmental Services - KY  | JOB NO. 2855-06 |                  |
|-----------------|----------------------------|-----------------|------------------|
| BORING NO.      | 211-B-001                  | SAMPLED         | 10/09/12 KD      |
| DEPTH           | 15-17' A                   | TEST STARTED    | 11/13/12 CAL     |
| SAMPLE NO.      | 211B001PERM2               | TEST FINISHED   | 11/19/12 CAL     |
| SOIL DESCR.     | ERI12-SW-SWMU211B          | SETUP NO.       | 13S              |
| LOCATION        | SW Plume RDSI Geotechnical | SATURATED TEST  | Yes              |
| CONF. PRES. PSF | 2070                       | TEST TYPE       | TX/Pbp/Tap Water |

### SATURATION DATA

| Cell<br>Pres.<br>(PSI) | Back<br>Pres.<br>(PSI) | Burette<br>Reading<br>(CC) | I            | Pore<br>Pressure<br>(PSI) | С    | hange | В    |
|------------------------|------------------------|----------------------------|--------------|---------------------------|------|-------|------|
| 40.0                   | 38.0                   | Close<br>11.7              | Open<br>17.9 | Close                     | Open |       |      |
| 50.0                   | 48.0                   | 18.6                       | 19.4         | 38.7                      | 46.4 | 7.7   | 0.77 |
| 60.0                   | 58.0                   | 19.5                       | 20.2         | 48.6                      | 56.9 | 8.3   | 0.83 |
| 70.0                   |                        | 20.3                       | 20.4         | 58.5                      | 68.0 | 9.5   | 0.95 |

#### CONSOLIDATION DATA

|                         | Elapsed | SQRT  |            | Burette        | Volume |       |
|-------------------------|---------|-------|------------|----------------|--------|-------|
|                         | Time    | Time  |            | Reading        | Defl.  |       |
|                         | (Min)   | (Min) |            | (CC)           | (cc)   |       |
|                         | 0.00    | 0.00  |            | 0.50           | 0.00   |       |
|                         | 0.25    | 0.50  |            | 1.80           | -1.30  |       |
|                         | 0.5     | 0.71  |            | 1.90           | -1.40  |       |
|                         | 1       | 1.00  |            | 2.20           | -1.70  |       |
|                         | 2       | 1.41  |            | 2.45           | -1.95  |       |
|                         | 2<br>5  | 2.24  |            | 2.90           | -2.40  |       |
|                         | 9       | 3.00  |            | 3.15           | -2.65  |       |
|                         | 16      | 4.00  |            | 3.20           | -2.70  |       |
|                         | 30      | 5.48  |            | 3.45           | -2.95  |       |
|                         | 60      | 7.75  |            | 3.60           | -3.10  |       |
|                         | 120     | 10.95 |            | 3.70           | -3.20  |       |
|                         | 240     | 15.49 |            | 3.70           | -3.20  |       |
|                         | 360     | 18.97 |            | 3.70           | -3.20  |       |
|                         |         |       |            |                | - 97   |       |
| Initial Height (in)     |         | 3.210 |            | Init. Vol. (CC |        |       |
| Height Change (in)      |         | 0.021 |            | Vol. Change    |        |       |
| Ht. After Cons. (in)    |         | 3.189 |            | Cell Exp. (0   |        |       |
| Initial Area (sq in)    |         | 2.054 |            | Net Change     |        |       |
| Area After Cons. (sq in | )       | 2.021 |            | Cons. Vol. (   | CC)    |       |
|                         |         |       |            |                | CC)    | TERRA |
| Data entry by           | DAW     | Date: | 11/26/2012 |                | 2 10   | SP    |

| Data entry by:     | DAW        | Date: |
|--------------------|------------|-------|
| Checked by: Bre    | Date: 11/2 | 27/12 |
| FileName: LKP00012 | -1         |       |

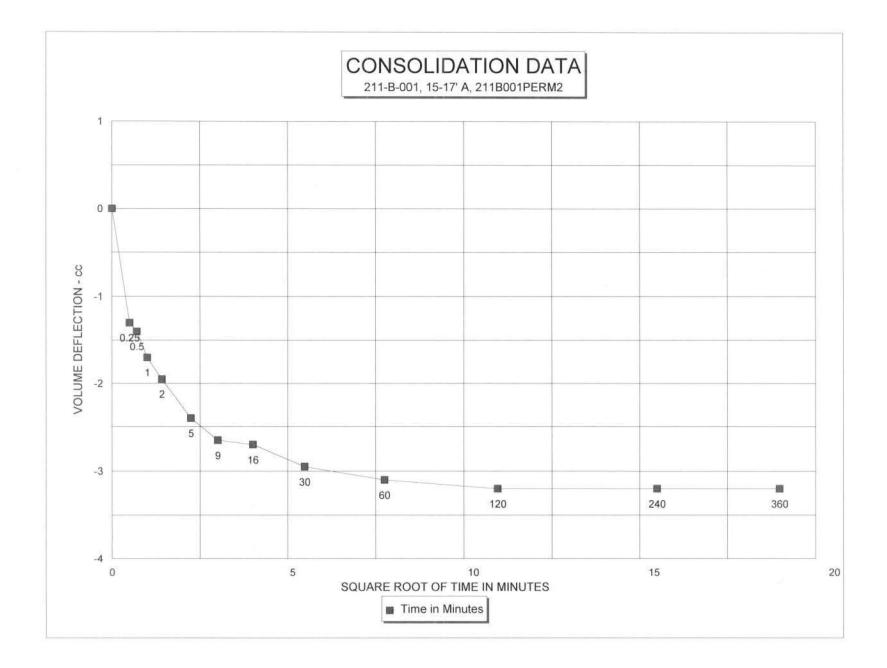
11/26/2012

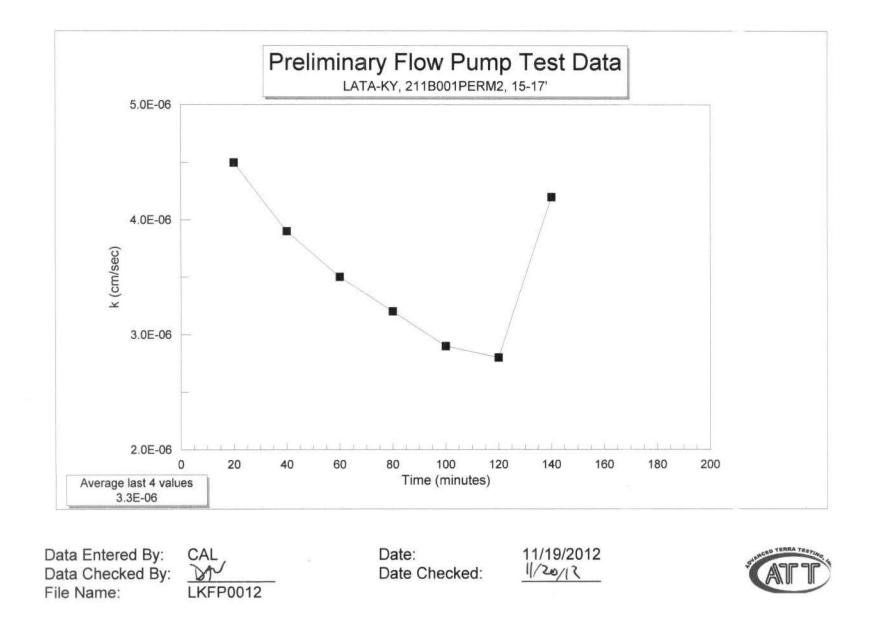


108.04 12.20

9.81

2.39





Client LATA ENV. Services - KY Job No. 2865-06 BoringNo. 211- 8-001 Depth\_ 15 -17 A Sample No. 211BOOLPERMZ Project Sw Plume RDSI Gestechnical Sampled 10 / 9 / 12 by KD Prepped 11/13/12 by CAL Project No. EREIZ-Sal-SWMUZIIB Tx/Pbp of 2070 pof LK2855/LKDP0012 11/20/12

| CLIENT L    | TA Environmental Services of Ky | JOB NO. 2855-06 |                  |
|-------------|---------------------------------|-----------------|------------------|
| BORING NO.  | SW Plume RDSI Geotechnical      | SAMPLED         | 10/11/12 KD      |
| DEPTH       |                                 | TEST STARTED    | 11/02/12 CAL     |
| SAMPLE NO.  |                                 | TEST FINISHED   | 11/17/12 CAL     |
| SOIL DESCR. |                                 | CELL NUMBER     | 7P               |
| LOCATION    |                                 | SATURATED TEST  | Yes              |
| CONF. PRES. |                                 | TEST TYPE       | TX/Pbp/Tap Water |

| BEFORE  | AFTER  |   |
|---------|--|---|
| TEST    | TEST   |   |
| 229.7   | 227.8  |   |
| 236.2   | 234.3  |   |
| 195.2   | 195.2  |   |
| 41.0    | 39.1   |   |
| 6.5     | 6.5  |   |
| 188.7   | 188.7  |   |
| 21.7    | 20.7   |   |
| 128.1   | 140.1  |   |
| 105.2   | 116.0  |   |
| 1.660   | (cm)   | 4.216   |
| 2.164   | (sq cm)  | 13.964  |
| 3.157   | (cm)   | 8.019   |
| 0.00395 |  |   |
| 0.00359 |  |   |
| 38.54   |  |   |
|         | TEST<br>229.7<br>236.2<br>195.2<br>41.0<br>6.5<br>188.7<br>21.7<br>128.1<br>105.2<br>1.660<br>2.164<br>3.157<br>0.00395<br>0.00359 | TEST         TEST           229.7         227.8           236.2         234.3           195.2         195.2           41.0         39.1           6.5         6.5           188.7         188.7           21.7         20.7           128.1         140.1           105.2         116.0           1.660         (cm)           2.164         (sq cm)           3.157         (cm)           0.00395         0.00359 |

## FLOW PUMP CALCULATIONS

| Pump Setting                  | 45       |
|-------------------------------|----------|
| Velocity CM/Sec               | 2.95E-04 |
| Q (cc/s)                      | 9.44E-06 |
| Height                        | 3.133    |
| Diameter                      | 1.587    |
| Pressure (psi)                | 0.166    |
| Area after consol. (cm*cm)    | 12.759   |
| Gradient                      | 1.467    |
| Permeability k (cm/s)         | 5.0E-07  |
| Permeability k (m/s)          | 5.0E-09  |
| Back Pressure (psi)           | 38.0     |
| Cell Pressure (psi)           | 46.1     |
| Ave. Effective Stress (psi)   | 8.017    |
| Average temperature degree C: | 22.1     |

| Data entry by:     | MLM   | Date:   |  |
|--------------------|-------|---------|--|
| Checked by: Che    | Date: | 1/19/12 |  |
| FileName: LKP00041 |       | 1       |  |

11/19/2012



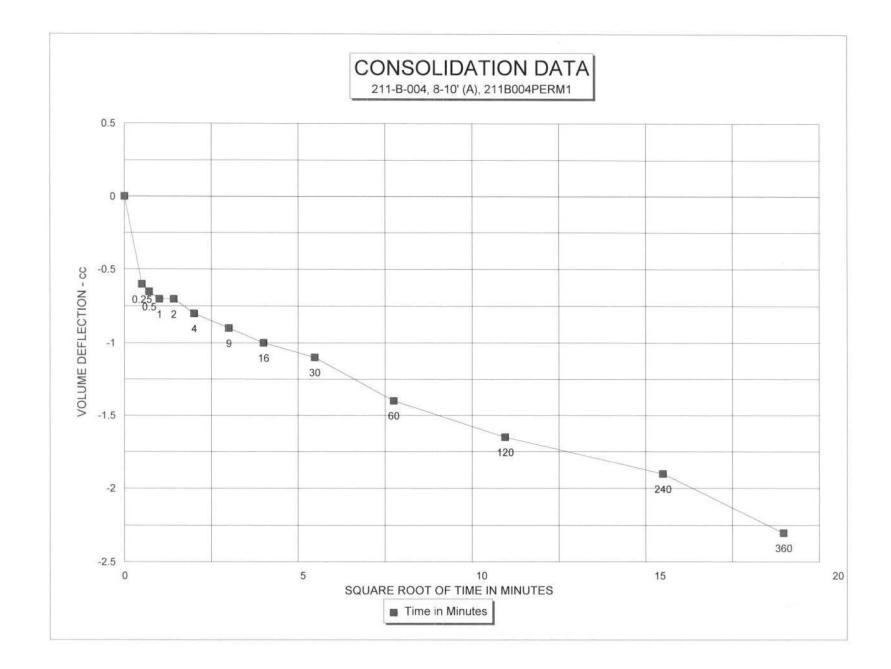
| CLIENT   | LATA Env   | ironmental Services of Ky   | JOB NO. 2855-06  |  |
|--|------------|---|--|--|
| BORING N<br>DEPTH<br>SAMPLE N<br>SOIL DES(<br>LOCATION<br>CONF. PR | NO.<br>CR. | 211-B-004<br>8-10' (A)<br>211B004PERM1<br>ERI12-SW-SWMU211B<br>SW Plume RDSI Geotechnical<br>1164 | SAMPLED<br>TEST STARTED<br>TEST FINISHED<br>SETUP NO.<br>SATURATED TEST<br>TEST TYPE | 10/11/12 KD<br>11/02/12 CAL<br>11/17/12 CAL<br>7P<br>Yes<br>TX/Pbp/Tap Water |

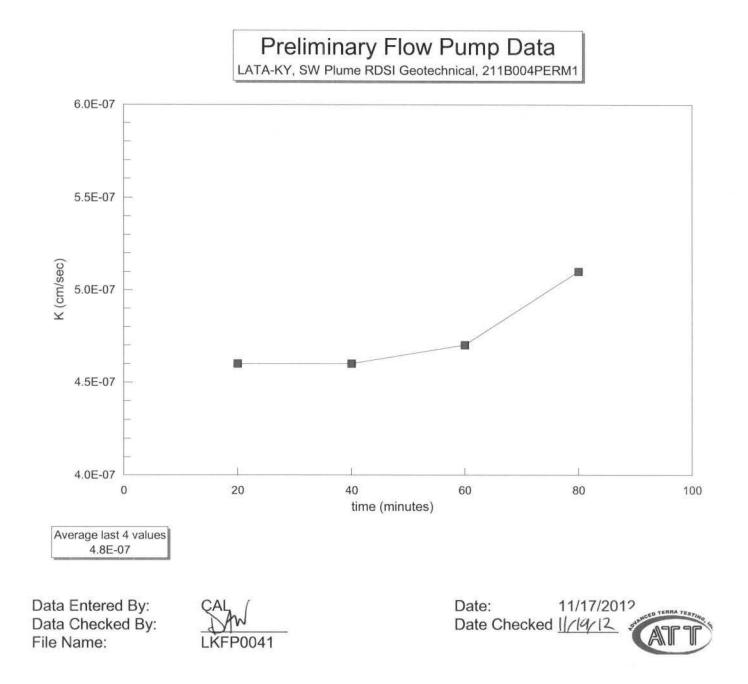
#### SATURATION DATA

| Cell<br>Pres.<br>(PSI) | Back<br>Pres.<br>(PSI) | Burette<br>Reading<br>(CC) |      | Pore<br>Pressure<br>(PSI) |      | Change | В |      |
|------------------------|------------------------|----------------------------|------|---------------------------|------|--------|---|------|
|                        |                        | Close                      | Open | Close                     | Open |        |   |      |
| 40.0                   | 38.0                   | 1.2                        | 9.7  |                           |      |        |   |      |
| 50.0                   |                        | 13.0                       | 13.2 | 38.8                      | 48.5 | 9.7    |   | 0.97 |

#### CONSOLIDATION DATA

| Elapsed<br>Time<br>(Min)   | SQRT<br>Time<br>(Min) | Burette Volume<br>Reading Defl.<br>(CC) (cc) |
|--|-----------------------|--|
| 0.00   | 0.00                  | 0.30 0.00                                    |
| 0.25   | 0.50                  | 0.90 -0.60                                   |
| 0.5  | 0.71                  | 0.95 -0.65                                   |
| 1  | 1.00                  | 1.00 -0.70                                   |
| 2 4  | 1.41                  | 1.00 -0.70                                   |
| 4  | 2.00                  | 1.10 -0.80                                   |
| 9  | 3.00                  | 1.20 -0.90                                   |
| 16   | 4.00                  | 1.30 -1.00                                   |
| 30   | 5.48                  | 1.40 -1.10                                   |
| 60   | 7.75                  | 1.70 -1.40                                   |
| 120  | 10.95                 | 1.95 -1.65                                   |
| 240  | 15.49                 | 2.20 -1.90                                   |
| 360  | 18.97                 | 2.60 -2.30                                   |
| Initial Height (in)  | 3.157                 | Init. Vol. (CC) 111.98                       |
| Height Change (in)   | 0.024                 | Vol. Change (CC) 24.20                       |
| Ht. After Cons. (in)   | 3.133                 | Cell Exp. (CC) 13.76                         |
| Initial Area (sq in)   | 2.164                 | Net Change (CC) 10.44                        |
| Area After Cons. (sq in)   | 1.978                 | Cons. Vol. (CC) 101.55                       |
| Data entry by: MLM<br>Checked by: Office Date: 11/19/1<br>FileName: LKP00041 | Date:                 | 11/19/2012                                   |





Client LATA ENV. Services of Ky Job No. 2855-06 BoringNo. 211-8-004 Depth 8-10' (A) Sample No. 211BCO4PERM1 Project SW Aume RD SI Gestechnical Sampled 10 / 11 / 12 by ED Prepped 11 / 02 / 12 by car Project No. ERID-SW-SWMUZIB TX/Pbp 53 1164 psf LK2855/LKDP810A 11/19/12

| CLIENT            | LATA Envir | onmental Services of KY    | JOB NO. 2855-06 |                              |
|-------------------|------------|----------------------------|-----------------|------------------------------|
| BORING N          | Ο.         | 211-B-004                  | SAMPLED         | 10/11/12 KD                  |
| DEPTH<br>SAMPLE N | 0          | 18-20' A<br>211B004PERM2   | TEST STARTED    | 11/02/12 CAL<br>11/14/12 CAL |
| SOIL DESC         |            | ERI12-SW-SWMU211B          | CELL NUMBER     | 9P                           |
| LOCATION          |            | SW Plume RDSI Geotechnical | SATURATED TEST  | Yes                          |
| CONF. PRE         | ES. PSF    | 2458                       | TEST TYPE       | TX/Pbp/Tap Water             |

| MOISTURE/DENSITY           | BEFORE  | AFTER   |        |
|----------------------------|---------|---------|--------|
| DATA                       | TEST    | TEST    |        |
| Wt. Soil + Moisture (g)    | 210.0   | 210.5   |        |
| Wt. Wet Soil & Pan (g)     | 216.5   | 217.1   |        |
| Wt. Dry Soil & Pan (g)     | 191.0   | 191.0   |        |
| Wt. Lost Moisture (g)      | 25.5    | 26.1    |        |
| Wt. of Pan Only (g)        | 6.6     | 6.6     |        |
| Wt. of Dry Soil (g)        | 184.4   | 184.4   |        |
| Moisture Content %         | 13.8    | 14.1    |        |
| Wet Density PCF            | 138.5   | 142.0   |        |
| Dry Density PCF            | 121.7   | 124.4   |        |
| Init. Diameter (in)        | 1.651   | (cm)    | 4.194  |
| Init. Area (sq in)         | 2.141   | (sq cm) | 13.813 |
| Init. Height (in)          | 2.697   | (cm)    | 6.850  |
| Vol. Bef. Consol. (cu ft)  | 0.00334 |         |        |
| Vol. After Consol. (cu ft) | 0.00327 |         |        |
| Porosity %                 | 28.16   |         |        |
|                            |         |         |        |

### FLOW PUMP CALCULATIONS

| Pump Setting                | 5        |
|-----------------------------|----------|
| Velocity CM/Sec             | 3.29E-05 |
| Q (cc/s)                    | 1.05E-06 |
| Height                      | 2.679    |
| Diameter                    | 1.639    |
| Pressure (psi)              | 4.700    |
| Area after consol. (cm*cm)  | 13.605   |
| Gradient                    | 48.562   |
| Permeability k (cm/s)       | 1.6E-09  |
| Permeability k (m/s)        | 1.6E-11  |
| Back Pressure (psi)         | 88.0     |
| Cell Pressure (psi)         | 105.1    |
| Ave. Effective Stress (psi) | 14.750   |

Average temperature degree C: NOTE: Filling required due to 1" gravel in sample.

| Data entry by:     | DAW   | Date:      | 11/19/2012 |
|--------------------|-------|------------|------------|
| Checked by: CHE    | Date: | 11/19/2012 |            |
| FileName: LKP00042 |       | / /        |            |



22.1

| BORING NO. 211-B-004 SAMPLED 10/11/12 KD  |            |
|---|------------|
| BORING NO.211-B-004SAMPLED10/11/12 KDDEPTH18-20' ATEST STARTED11/02/12 CALSAMPLE NO.211B004PERM2TEST FINISHED11/14/12 CALSOIL DESCR.ERI12-SW-SWMU211BSETUP NO.9PLOCATIONSW Plume RDSI GeotechnicalSATURATED TESTYesCONF. PRES. PSF2458TEST TYPETX/Pbp/Tap W | CAL<br>CAL |

#### SATURATION DATA

| Cell<br>Pres.<br>(PSI) | Back<br>Pres.<br>(PSI) | Burette<br>Reading<br>(CC) |      | Pore<br>Pressure<br>(PSI) |      | Change | в |      |
|------------------------|------------------------|----------------------------|------|---------------------------|------|--------|---|------|
|                        |                        | Close                      | Open | Close                     | Open |        |   |      |
| 40.0                   | 38.0                   | 1.2                        | 7.2  |                           |      |        |   |      |
| 50.0                   | 48.0                   | 9.6                        | 11.0 | 38.3                      | 45.9 | 7.6    |   | 0.76 |
| 60.0                   | 58.0                   | 11.4                       | 12.3 | 48.6                      | 56.5 | 7.9    |   | 0.79 |
| 70.0                   | 68.0                   | 13.0                       | 13.8 | 58.6                      | 67.2 | 8.6    |   | 0.86 |
| 80.0                   | 78.0                   | 14.3                       | 15.1 | 68.6                      | 77.5 | 8.9    |   | 0.89 |
| 90.0                   | 88.0                   | 15.6                       | 16.4 | 78.6                      | 87.6 | 9.0    |   | 0.90 |
| 100.0                  |                        | 16.8                       | 16.9 | 88.3                      | 97.9 | 9.6    |   | 0.96 |

## CONSOLIDATION DATA

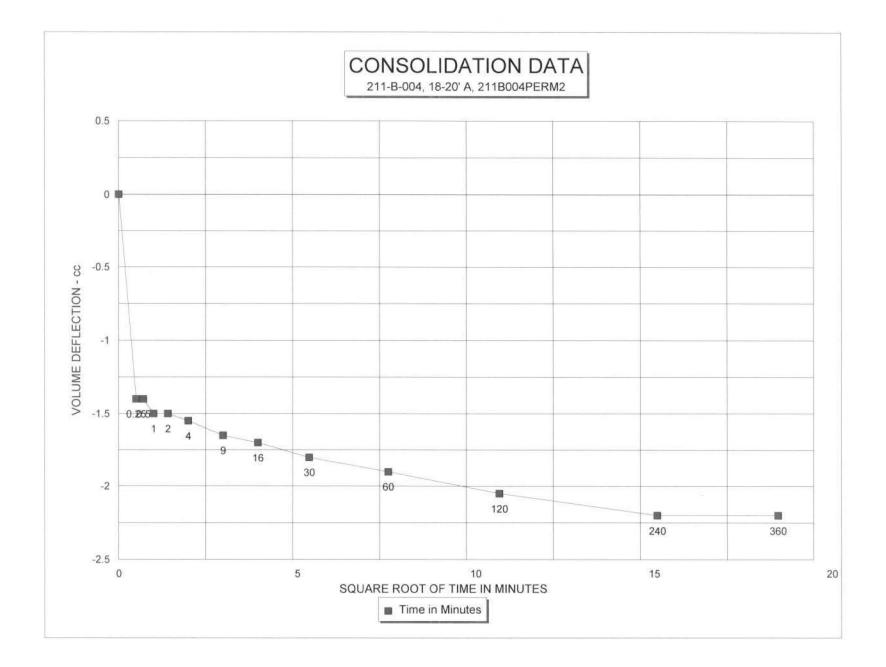
|                          | Elapsed<br>Time | SQRT<br>Time |            | Burette<br>Reading | Volume<br>Defl. |
|--------------------------|-----------------|--------------|------------|--------------------|-----------------|
|                          | (Min)           | (Min)        |            | (CC)               | (cc)            |
|                          | 0.00            | 0.00         |            | 0.40               | 0.00            |
|                          | 0.25            | 0.50         |            | 1.80               | -1.40           |
|                          | 0.5             | 0.71         |            | 1.80               | -1.40           |
|                          | 1               | 1.00         |            | 1.90               | -1.50           |
|                          | 2               | 1.41         |            | 1.90               | -1.50           |
|                          | 4<br>9          | 2.00         |            | 1.95               | -1.55           |
|                          | 9               | 3.00         |            | 2.05               | -1.65           |
|                          | 16              | 4.00         |            | 2.10               | -1.70           |
|                          | 30              | 5.48         |            | 2.20               | -1.80           |
|                          | 60              | 7.75         |            | 2.30               | -1.90           |
|                          | 120             | 10.95        |            | 2.45               | -2.05           |
|                          | 240             | 15.49        |            | 2.60               | -2.20           |
|                          | 360             | 18.97        |            | 2.60               | -2.20           |
| Initial Height (in)      |                 | 2.697        |            | Init. Vol. (CC     | 3               |
| Height Change (in)       |                 | 0.018        |            | Vol. Change        |                 |
| Ht. After Cons. (in)     |                 | 2.679        |            | Cell Exp. (C       |                 |
| Initial Area (sq in)     |                 | 2.141        |            | Net Change         |                 |
| Area After Cons. (sq in) |                 | 2.109        |            | Cons. Vol. (0      | CC)             |
| Data entry by:           | DAW .           | Date:        | 11/19/2012 |                    | *Saturces T     |

| INCED TERRA | ESTINO |
|-------------|--------|
| ANT         | TR     |
| 0-01 UI     | UI     |

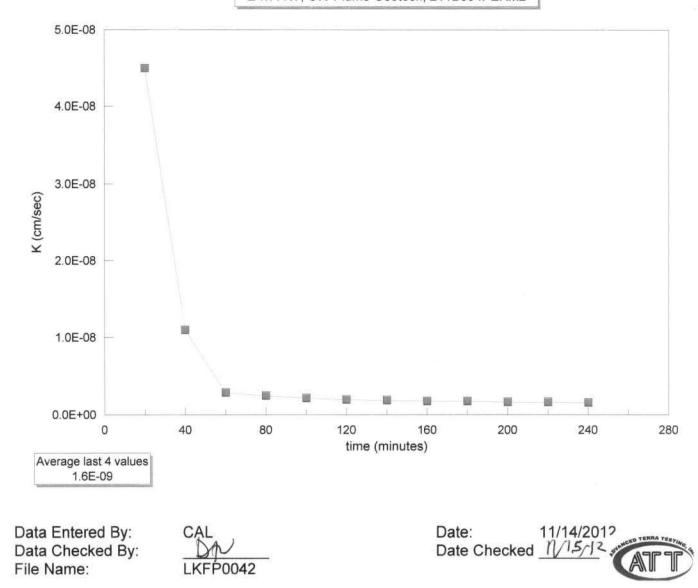
94.63 18.40 16.36

2.04 92.59

| Data entry by:     | DAW   | Date:      |
|--------------------|-------|------------|
| Checked by: Offer  | Date: | 11/19/2012 |
| FileName: LKP00042 |       | . ,        |



# Preliminary Flow Pump Data LATA-KY, SW Plume Geotech, 211B004PERM2



Client LATA Environmental Services-Ky Job No. <u>2855-72</u> Boring No. <u>241-R-004</u> Depth <u>181-20' A</u> Sample No. <u>216004 PEPMZ</u> Project SW Rume. RDST Geotechnical Sampled 10/11/12 by KD Project No. <u>ERTO.-5W SwMUZIIB</u> Project No. <u>ERTO.-5W SwMUZIIB</u> TR/Pbp J 17.1 psi = 2458 psf LK2855/LKDP0042 11/15/12

| CLIENT LATA En  | vironmental Services of Ky      | JOB NO. 2855-06 |                  |
|-----------------|---------------------------------|-----------------|------------------|
| BORING NO.      | 211-B-004                       | SAMPLED         | 10/11/12 KD      |
| DEPTH           | 38-40' (A)                      | TEST STARTED    | 11/02/12 CAL     |
| SAMPLE NO.      | 211B004PERM3                    | TEST FINISHED   | 11/13/12 CAL     |
| SOIL DESCR.     | ERI12-SW-SWMU211B               | CELL NUMBER     | 13S              |
| LOCATION        | SW Plume RDSI Geotechnical 5046 | SATURATED TEST  | Yes              |
| CONF. PRES. PSF |                                 | TEST TYPE       | TX/Pbp/Tap Water |

| MOISTURE/DENSITY           | BEFORE  | AFTER   |        |
|----------------------------|---------|---------|--------|
| DATA                       | TEST    | TEST    |        |
| Wt. Soil + Moisture (g)    | 236.9   | 233.1   |        |
| Wt. Wet Soil & Pan (g)     | 243.7   | 239.9   |        |
| Wt. Dry Soil & Pan (g)     | 203.0   | 203.0   |        |
| Wt. Lost Moisture (g)      | 40.8    | 36.9    |        |
| Wt. of Pan Only (g)        | 6.8     | 6.8     |        |
| Wt. of Dry Soil (g)        | 196.2   | 196.2   |        |
| Moisture Content %         | 20.8    | 18.8    |        |
| Wet Density PCF            | 131.8   | 133.8   |        |
| Dry Density PCF            | 109.1   | 112.6   |        |
| Init. Diameter (in)        | 1.662   | (cm)    | 4.221  |
| Init. Area (sq in)         | 2.169   | (sq cm) | 13.997 |
| Init. Height (in)          | 3.157   | (cm)    | 8.019  |
| Vol. Bef. Consol. (cu ft)  | 0.00396 |         |        |
| Vol. After Consol. (cu ft) | 0.00384 |         |        |
| Porosity %                 | 33.95   |         |        |

# FLOW PUMP CALCULATIONS

| Pump Setting                  | 5        |
|-------------------------------|----------|
| Velocity CM/Sec               | 3.29E-05 |
| Q (cc/s)                      | 1.05E-06 |
| Height                        | 3.090    |
| Diameter                      | 1.654    |
| Pressure (psi)                | 3.490    |
| Area after consol. (cm*cm)    | 13.863   |
| Gradient                      | 31.264   |
| Permeability k (cm/s)         | 2.4E-09  |
| Permeability k (m/s)          | 2.4E-11  |
| Back Pressure (psi)           | 48.0     |
| Cell Pressure (psi)           | 83.0     |
| Ave. Effective Stress (psi)   | 33.255   |
| Average temperature degree C: | 22.0     |

| Data entry by:     | MLM .    | Date:            | 11/14/2012 |
|--------------------|----------|------------------|------------|
| Checked by: CM     | Date: II | 14/12            |            |
| FileName: LKP00043 |          | Children Page 19 |            |

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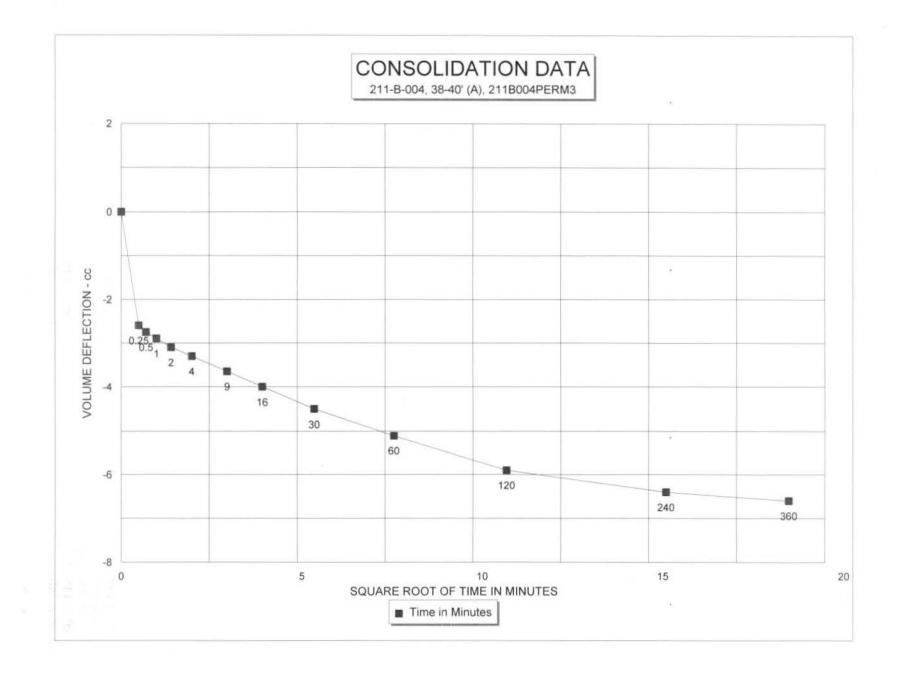
| CLIENT  | LATA Env        | vironmental Services of Ky   | JOB NO. 2855-06  |   |
|---|-----------------|--|--|---|
| BORING N<br>DEPTH<br>SAMPLE I<br>SOIL DES<br>LOCATIOI<br>CONF. PR | NO.<br>CR.<br>N | 211-B-004<br>38-40' (A)<br>211B004PERM3<br>ERI12-SW-SWMU211B<br>SW Plume RDSI Geotechnical<br>5046 | SAMPLED<br>TEST STARTED<br>TEST FINISHED<br>SETUP NO.<br>SATURATED TEST<br>TEST TYPE | 10/11/12 KD<br>11/02/12 CAL<br>11/13/12 CAL<br>13S<br>Yes<br>TX/Pbp/Tap Water |
|   | 24              | × .  | 343  | A   |

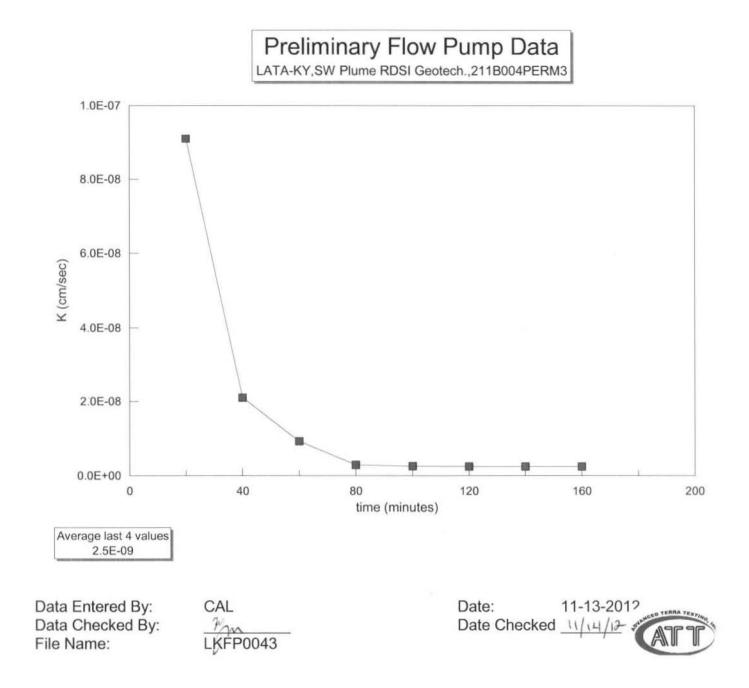
#### SATURATION DATA

| Cell<br>Pres.<br>(PSI) | Back<br>Pres.<br>(PSI) | Burette<br>Reading<br>(CC) |      | Pore<br>Pressure<br>(PSI) | C    | Change | В |      |
|------------------------|------------------------|----------------------------|------|---------------------------|------|--------|---|------|
|                        |                        | Close                      | Open | Close                     | Open |        |   |      |
| 40.0                   | 38.0                   | 1.8                        | 6.8  |                           |      |        |   |      |
| 50.0                   | 48.0                   | 7.3                        | 8.1  | 38.2                      | 47.5 | 9.3    |   | 0.93 |
| 60.0                   |                        | 8.3                        | 8.4  | 48.7                      | 58.2 | 9.5    |   | 0.95 |

### CONSOLIDATION DATA

| т  | psed<br>ïme<br>Min) | SQRT<br>Time<br>(Min) |            | Burette<br>Reading<br>(CC) | Volume<br>Defl.<br>(cc) |                      |
|--|---------------------|-----------------------|------------|----------------------------|-------------------------|----------------------|
|  | 0.00                | 0.00                  |            | 0.40                       | 0.00                    |                      |
|  | 0.25                | 0.50                  |            | 3.00                       | -2.60                   |                      |
|  | 0.5                 | 0.71                  |            | 3.15                       | -2.75                   |                      |
|  | 1                   | 1.00                  |            | 3.30                       | -2.90                   |                      |
|  | 2                   | 1.41                  |            | 3.50                       | -3.10                   |                      |
|  | 2<br>4<br>9         | 2.00                  |            | 3.70                       | -3.30                   |                      |
|  |                     | 3.00                  |            | 4.05                       | -3.65                   |                      |
|  | 16                  | 4.00                  |            | 4.40                       | -4.00                   |                      |
|  | 30                  | 5.48                  |            | 4.90                       | -4.50                   |                      |
|  | 60                  | 7.75                  |            | 5.50                       | -5.10                   |                      |
|  | 120                 | 10.95                 |            | 6.30                       | -5.90                   |                      |
|  | 240                 | 15.49                 |            | 6.80                       | -6.40                   |                      |
|  | 360                 | 18.97                 |            | 7.00                       | -6.60                   |                      |
| Initial Height (in)  |                     | 3.157                 |            | Init. Vol. (CC             |                         | 112.25               |
| Height Change (in)   |                     | 0.067                 |            | Vol. Change                |                         | 14.20                |
| Ht. After Cons. (in)   |                     | 3.090                 |            | Cell Exp. (C               |                         | 10.77                |
| Initial Area (sq in)   |                     | 2.169                 |            | Net Change                 |                         | 3.43                 |
| Area After Cons. (sq in)   |                     | 2.149                 |            | Cons. Vol. (               |                         | 108.82               |
| Allow Allor Obliat (ad III)  |                     | 2.140                 |            | 0013. 701. (               |                         |                      |
| Data entry by: MLM<br>Checked by: <u>CMP</u> Date:<br>FileName: LKP00043 | <u>- 11/14/12</u>   | eate:                 | 11/14/2012 |                            |                         | STATES TERRA TESTING |





Client LATA ENV. Services of Ky Job No. 2855-06 BoringNo. 211-B-004 Depth 38-40' A Sample No. 2118 004 PERM3 Project SW Plume RDSI Geotechnical Sampled 10 / 11 / 12 by KD Prepped 11 / 02 / 12 by CAL Project No. ERI 12-50- 5WMU 211 B Tx/Pbp 53 5046 psf LK2855/LKDP0043 11/14/12

| CLIENT  | LATA Envir | ronmental Services-Ky  | JOB NO.   | 2855-02                         |  |
|---|------------|--|---|---------------------------------|--|
| BORING NO<br>DEPTH<br>SAMPLE NO<br>PROJECT N<br>LOCATION<br>CONF. PRE | D.<br>10.  | MW516<br>10-12'<br>MW516Perm1<br>ERI12-SW-SWMU211B<br>SW Plume RDSI Geotechnical<br>1423 | SAMPLED<br>TEST STA<br>TEST FINI<br>CELL NUM<br>SATURAT<br>TEST TYP | RTED<br>SHED<br>MBER<br>ED TEST | 8/22/12 CB<br>9/13/12 CAL<br>9/22/12 CAL<br>27S<br>Yes<br>TX/Pbp/Tap Water |

| DATA         TEST         TEST           Wt. Soil + Moisture (g)         688.7         696.0           Wt. Wet Soil & Pan (g)         695.2         702.5           Wt. Dry Soil & Pan (g)         604.7         604.7           Wt. Dry Soil & Pan (g)         90.5         97.8           Wt. Lost Moisture (g)         90.5         97.8           Wt. of Pan Only (g)         6.5         6.5           Wt. of Dry Soil (g)         598.2         598.2           Moisture Content %         15.1         16.3           Wet Density PCF         134.1         137.6           Dry Density PCF         116.5         118.3           Init. Diameter (in)         2.847         (cm)         7.231           Init. Area (sq in)         6.366         (sq cm)         41.073           Init. Height (in)         3.073         (cm)         7.805           Vol. Bef. Consol. (cu ft)         0.01132         0.01115         7.805           Vol. After Consol. (cu ft)         0.01115         9.01115         7.805 | MOISTURE/DENSITY           | BEFORE  | AFTER   |        |
|---|----------------------------|---------|---------|--------|
| Wt. Wet Soil & Pan (g)       695.2       702.5         Wt. Dry Soil & Pan (g)       604.7       604.7         Wt. Lost Moisture (g)       90.5       97.8         Wt. of Pan Only (g)       6.5       6.5         Wt. of Pan Only (g)       598.2       598.2         Moisture Content %       15.1       16.3         Wet Density PCF       134.1       137.6         Dry Density PCF       116.5       118.3         Init. Diameter (in)       2.847       (cm)       7.231         Init. Area (sq in)       6.366       (sq cm)       41.073         Init. Height (in)       3.073       (cm)       7.805         Vol. Bef. Consol. (cu ft)       0.01132       Vol. After Consol. (cu ft)       0.01115   | DATA                       | TEST    | TEST    |        |
| Wt. Dry Soil & Pan (g)       604.7       604.7         Wt. Lost Moisture (g)       90.5       97.8         Wt. of Pan Only (g)       6.5       6.5         Wt. of Dry Soil (g)       598.2       598.2         Moisture Content %       15.1       16.3         Wet Density PCF       134.1       137.6         Dry Density PCF       116.5       118.3         Init. Diameter (in)       2.847       (cm)       7.231         Init. Area (sq in)       6.366       (sq cm)       41.073         Init. Height (in)       3.073       (cm)       7.805         Vol. Bef. Consol. (cu ft)       0.01132       Vol. After Consol. (cu ft)       0.01115  | Wt. Soil + Moisture (g)    | 688.7   | 696.0   |        |
| Wt. Lost Moisture (g)       90.5       97.8         Wt. of Pan Only (g)       6.5       6.5         Wt. of Dry Soil (g)       598.2       598.2         Moisture Content %       15.1       16.3         Wet Density PCF       134.1       137.6         Dry Density PCF       116.5       118.3         Init. Diameter (in)         Linit. Area (sq in)       6.366       (sq cm)       41.073         Init. Height (in)       3.073       (cm)       7.805         Vol. Bef. Consol. (cu ft)       0.01132       Vol. After Consol. (cu ft)       0.01115   | Wt. Wet Soil & Pan (g)     | 695.2   | 702.5   |        |
| Wt. of Pan Only (g)       6.5       6.5         Wt. of Dry Soil (g)       598.2       598.2         Moisture Content %       15.1       16.3         Wet Density PCF       134.1       137.6         Dry Density PCF       116.5       118.3         Init. Diameter (in)       2.847         Init. Area (sq in)       6.366       (sq cm)       41.073         Init. Height (in)       3.073       (cm)       7.805         Vol. Bef. Consol. (cu ft)       0.01132       Vol. After Consol. (cu ft)       0.01115  | Wt. Dry Soil & Pan (g)     | 604.7   | 604.7   |        |
| Wt. of Dry Soil (g)       598.2       598.2         Moisture Content %       15.1       16.3         Wet Density PCF       134.1       137.6         Dry Density PCF       116.5       118.3         Init. Diameter (in)       2.847       (cm)       7.231         Init. Area (sq in)       6.366       (sq cm)       41.073         Init. Height (in)       3.073       (cm)       7.805         Vol. Bef. Consol. (cu ft)       0.01132       Vol. After Consol. (cu ft)       0.01115   | Wt. Lost Moisture (g)      | 90.5    | 97.8    |        |
| Moisture Content %         15.1         16.3           Wet Density PCF         134.1         137.6           Dry Density PCF         116.5         118.3           Init. Diameter (in)         2.847         (cm)         7.231           Init. Area (sq in)         6.366         (sq cm)         41.073           Init. Height (in)         3.073         (cm)         7.805           Vol. Bef. Consol. (cu ft)         0.01132         Vol. After Consol. (cu ft)         0.01115   | Wt. of Pan Only (g)        | 6.5     | 6.5     |        |
| Wet Density PCF         134.1         137.6           Dry Density PCF         116.5         118.3           Init. Diameter (in)         2.847         (cm)         7.231           Init. Area (sq in)         6.366         (sq cm)         41.073           Init. Height (in)         3.073         (cm)         7.805           Vol. Bef. Consol. (cu ft)         0.01132         Vol. After Consol. (cu ft)         0.01115  | Wt. of Dry Soil (g)        | 598.2   | 598.2   |        |
| Dry Density PCF         116.5         118.3           Init. Diameter (in)         2.847         (cm)         7.231           Init. Area (sq in)         6.366         (sq cm)         41.073           Init. Height (in)         3.073         (cm)         7.805           Vol. Bef. Consol. (cu ft)         0.01132         Vol. After Consol. (cu ft)         0.01115  | Moisture Content %         | 15.1    | 16.3    |        |
| Init. Diameter (in)       2.847 (cm)       7.231         Init. Area (sq in)       6.366 (sq cm)       41.073         Init. Height (in)       3.073 (cm)       7.805         Vol. Bef. Consol. (cu ft)       0.01132       Vol. After Consol. (cu ft)  | Wet Density PCF            | 134.1   | 137.6   |        |
| Init. Area         (sq in)         6.366         (sq cm)         41.073           Init. Height         (in)         3.073         (cm)         7.805           Vol. Bef. Consol.         (cu ft)         0.01132         Vol. After Consol.         (cu ft)   | Dry Density PCF            | 116.5   | 118.3   |        |
| Init. Height         (in)         3.073         (cm)         7.805           Vol. Bef. Consol. (cu ft)         0.01132         0.01115         0.01115  | Init. Diameter (in)        | 2.847   | (cm)    | 7.231  |
| Vol. Bef. Consol. (cu ft)         0.01132           Vol. After Consol. (cu ft)         0.01115  | Init. Area (sq in)         | 6.366   | (sq cm) | 41.073 |
| Vol. After Consol. (cu ft) 0.01115  | Init. Height (in)          | 3.073   | (cm)    | 7.805  |
|   | Vol. Bef. Consol. (cu ft)  | 0.01132 |         |        |
| Porosity % 30.97  | Vol. After Consol. (cu ft) | 0.01115 |         |        |
|   | Porosity %                 | 30.97   |         |        |

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# FLOW PUMP CALCULATIONS

| D                           | 00       |
|-----------------------------|----------|
| Pump Setting                | 99       |
| Velocity CM/Sec             | 6.50E-04 |
| Q (cc/s)                    | 2.08E-05 |
| Height                      | 3.058    |
| Diameter                    | 2.832    |
| Pressure (psi)              | 0.064    |
| Area after consol. (cm*cm)  | 40.644   |
| Gradient                    | 0.579    |
| Permeability k (cm/s)       | 8.8E-07  |
| Permeability k (m/s)        | 8.8E-09  |
| Back Pressure (psi)         | 48.0     |
| Cell Pressure (psi)         | 57.9     |
| Ave. Effective Stress (psi) | 9.868    |
|                             |          |

# Average temperature degree C:

| Data entry by:     | MLM Date:                   |
|--------------------|-----------------------------|
| Checked by:        | Date: <u><b>9/25/12</b></u> |
| FileName: LKP05161 |                             |

09/24/2012

23.4



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| CLIENT LATA En   | vironmental Services-Ky    | JOB NO. 2855-02 |                  |
|------------------|----------------------------|-----------------|------------------|
| BORING NO.       | MW516                      | SAMPLED         | 8/22/12 CB       |
| DEPTH            | 10-12'                     | TEST STARTED    | 9/13/12 CAL      |
| SAMPLE NO.       | MW516Perm1                 | TEST FINISHED   | 9/22/12 CAL      |
| PROJECT NO.      | ERI12-SW-SWMU211B          | SETUP NO.       | 27S              |
| LOCATION         | SW Plume RDSI Geotechnical | SATURATED TEST  | Yes              |
| CONF. PRES. PSF. | 1423                       | TEST TYPE       | TX/Pbp/Tap Water |

#### SATURATION DATA

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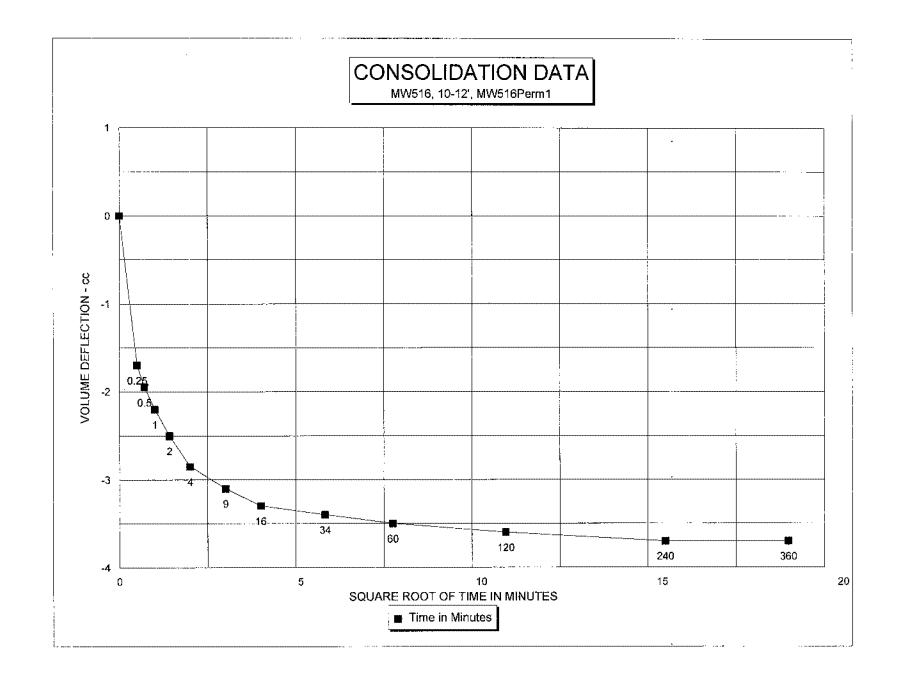
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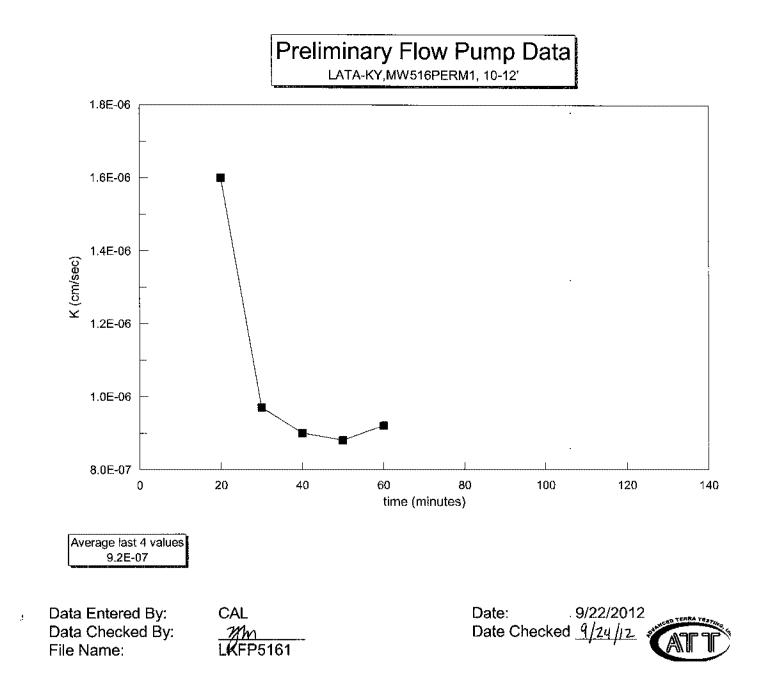
| Cell<br>Pres.<br>(PSI) | Back<br>Pres.<br>(PSI) | Burette<br>Reading<br>(CC) |              | Pore<br>Pressure<br>(PSI) |      | Change | в |      |
|------------------------|------------------------|----------------------------|--------------|---------------------------|------|--------|---|------|
| 40.0                   | 38.0                   | Close<br>3.4               | Open<br>15,4 | Close                     | Open |        |   |      |
| 50.0                   | 48.0                   | 17.2                       | 18.8         | 38.4                      | 47.7 | 9.3    |   | 0.93 |
| 60.0                   |                        | 19.8                       | 19.9         | 48.8                      | 58.7 | 9.9    |   | 0.99 |

#### CONSOLIDATION DATA

|  | Elapsed<br>Time<br>(Min)       | SQRT<br>Time<br>(Min) |            | Burette<br>Reading<br>(CC)  | Volume<br>Defl.<br>(cc) |                |
|--|--------------------------------|-----------------------|------------|-----------------------------|-------------------------|----------------|
|  | 0.00<br>0.25                   | 0.00<br>0.50          |            | 1.80<br>3.50                | 0.00<br>-1.70           |                |
|  | 0.5<br>1                       | 0.71<br>1.00          |            | 3.75<br>4.00                | -1.95<br>-2.20          |                |
|  | 2<br>4                         | 1.41<br>2.00          |            | 4.30<br>4.65                | -2.50<br>-2.85          |                |
|  | 9<br>16                        | 3.00<br>4.00          |            | 4.90<br>5.10                | -3.10<br>-3.30          |                |
|  | 34<br>60                       | 5.83<br>7.75          |            | 5.20<br>5.30                | -3.40<br>-3.50          |                |
|  | 120<br>240                     | 10.95<br>15.49        |            | 5.40<br>5.50                | -3.60<br>-3.70          |                |
|  | 360                            | 18.97                 |            | 5.50                        | -3.70                   |                |
| Initial Height (in)                              |                                | 3.073                 |            | Init. Vol. (CC              |                         | 320.63         |
| Height Change (in)<br>Ht. After Cons. (in)       |                                | 0.015<br>3.058        |            | Vol. Change<br>Cell Exp. (C | C)                      | 22.00<br>17.12 |
| Initial Area (sq in)<br>Area After Cons. (sq in) |                                | 6.366<br>6.300        |            | Net Change<br>Cons. Vol. (0 |                         | 4.88<br>315.75 |
|  | MLM Da<br>Date: <u>9/25/12</u> | ite:<br>-             | 09/24/2012 |                             |                         | ATT T          |
| Fliendine, ENPUSIOI                              |                                |                       | E 144      |                             |                         |                |



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| CLIENT  | LATA Enviro  | nmental Service   | s-Ky  |   | JOB NO.  | 2855-02                         |  |
|---|--|---|---|---|--|---------------------------------|--|
| BORING NO<br>DEPTH<br>SAMPLE NO<br>PROJECT N<br>LOCATION<br>CONF. PRE   | 0.<br>NO.  | MW-516<br>25-26'<br>MW516PERM2<br>ERI12-SW-SW<br>SW Plume RDS<br>3299 | MU211B  | ŧI  | SAMPLED<br>TEST STAI<br>TEST FINIS<br>CELL NUM<br>SATURATH<br>TEST TYP | RTED<br>SHED<br>IBER<br>ED TEST | 8/22/12 CB<br>9/13/12 CAL<br>9/25/12 CAL<br>26S<br>Yes<br>TX/Pbp/Tap Water |
| MOISTURE<br>DATA  |  |   | BEFORE<br>TEST  | AFTER<br>TEST   |  |                                 |  |
| Wt. Soil + M<br>Wt. Wet Soi<br>Wt. Dry Soil<br>Wt. Lost Mo<br>Wt. of Pan (<br>Wt. of Dry S<br>Moisture Co<br>Wet Density<br>Dry Density | il & Pan (g)<br>  & Pan (g)<br>bisture (g)<br>Dnly (g)<br>Soil (g)<br>bottent %<br>/ PCF |   | 647.0<br>653.5<br>569.2<br>84.3<br>6.5<br>562.7<br>15.0<br>127.0<br>110.4 | 654.8<br>661.3<br>569.2<br>92.1<br>6.5<br>562.7<br>16.4<br>137.3<br>117.9 |  |                                 |  |
| Init. Diamete   | er (in)  |   | 2.841   | (cm)  | ) 7.216  | i i                             |  |

| Init. Diameter (in)        | 2,841   | (cm)    | 7.216  |
|----------------------------|---------|---------|--------|
| Init. Area (sq in)         | 6.339   | (sq cm) | 40.900 |
| Init. Height (in)          | 3.062   | (cm)    | 7.777  |
| Vol. Bef. Consol. (cu ft)  | 0.01123 |         |        |
| Vol. After Consol. (cu ft) | 0.01052 |         |        |
| Porosity %                 | 30.92   |         |        |
|                            |         |         |        |

#### FLOW PUMP CALCULATIONS

Date:

| Pump Setting (gear number)<br>Percentage of Pump setting<br>Q (cc/s)<br>Height<br>Diameter<br>Pressure (psi)<br>Area after consol. (cm*cm)<br>Gradient<br>Permeability k (cm/s)<br><b>Permeability k (m/s)</b><br>Back Pressure (psi)<br>Cell Pressure (psi) | 12<br>100<br>2.30E-05<br>2.985<br>2.784<br>1.414<br>39.280<br>13.112<br>4.5E-08<br><b>4.5E-08</b><br><b>4.5E-10</b><br>48.0<br>71.0 |
|--|---|
| Cell Pressure (psi)<br>Ave. Effective Stress (psi)<br>Average temperature degree C:  | 22.293<br>22.9  |

| Data entry by:     | MLM , D       |
|--------------------|---------------|
| Checked by: 04     | Date: 9/26/12 |
| FileName: LKP05162 | • •           |

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09/26/2012



| CLIENT LATA En  | vironmental Services-Ky    | JOB NO. 2855-02 |                  |
|-----------------|----------------------------|-----------------|------------------|
| BORING NO.      | MW-516                     | SAMPLED         | 8/22/12 CB       |
| DEPTH           | 25-26'                     | TEST STARTED    | 9/13/12 CAL      |
| SAMPLE NO.      | MW516PERM2                 | TEST FINISHED   | 9/25/12 CAL      |
| PROJECT NO.     | ERI12-SW-SWMU211B          | SETUP NO.       | 26S              |
| LOCATION        | SW Plume RDSI Geotechnical | SATURATED TEST  | Yes              |
| CONF. PRES. PSF | 3299                       | TEST TYPE       | TX/Pbp/Tap Water |

#### SATURATION DATA

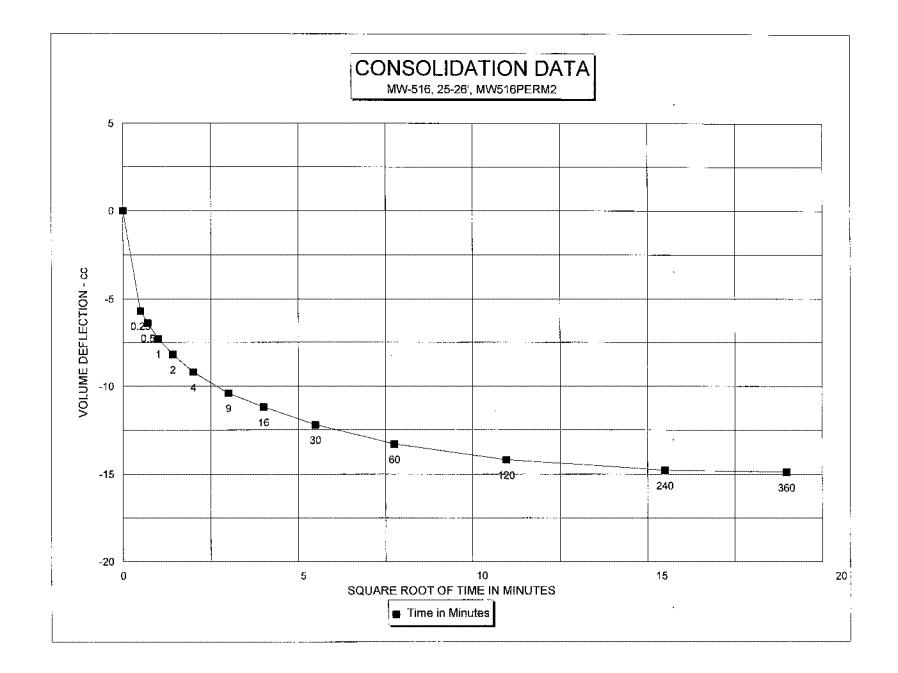
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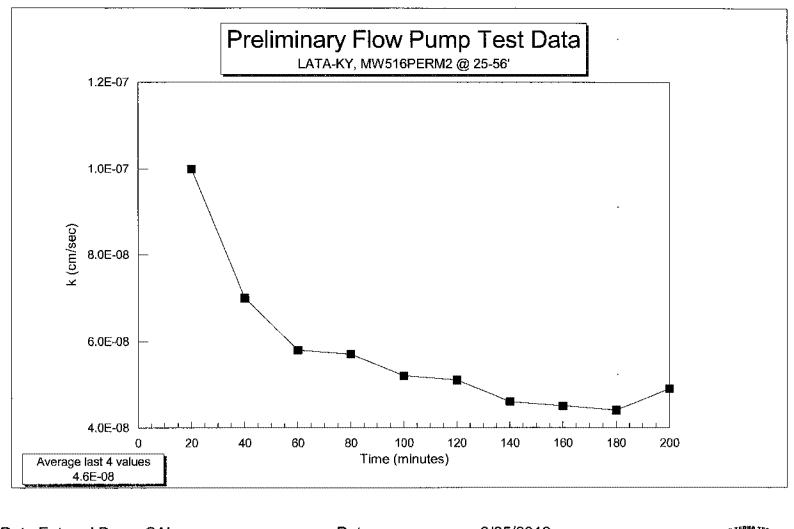
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| Cell<br>Pres.<br>(PSI) | Back<br>Pres.<br>(PSI) | Burette<br>Reading<br>(CC) |      | Pore<br>Pressure<br>(PSI) | ł    | Change | В |      |
|------------------------|------------------------|----------------------------|------|---------------------------|------|--------|---|------|
|                        |                        | Close                      | Open | Close                     | Open |        |   |      |
| 40.0                   | 38.0                   | 6.3                        | 21.9 |                           |      |        |   |      |
| 50.0                   | 48.0                   | 25.6                       | 26.9 | 38.6                      | 47.7 | 9.1    |   | 0.91 |
| 60.0                   |                        | 27.2                       | 27.4 | 48.8                      | 58.3 | 9.5    |   | 0.95 |

## CONSOLIDATION DATA

|   | Elapsed<br>Time<br>(Min)  | SQRT<br>Time<br>(Min)  |            | Burette<br>Reading<br>(CC)   | Volume<br>Defl.<br>(cc)   |   |
|---|---|--|------------|--|---|---|
| ,   | 0.00<br>0.25<br>0.5<br>1<br>2<br>4<br>9<br>16<br>30<br>60<br>120<br>240 | 0.00<br>0.50<br>0.71<br>1.00<br>1.41<br>2.00<br>3.00<br>4.00<br>5.48<br>7.75<br>10.95<br>15.49 |            | 0.20<br>5.90<br>6.60<br>7.50<br>8.40<br>9.40<br>10.60<br>11.40<br>12.40<br>13.50<br>14.40<br>15.00 | 0.00<br>-5.70<br>-6.40<br>-7.30<br>-8.20<br>-9.20<br>-10.40<br>-11.20<br>-12.20<br>-13.30<br>-14.20<br>-14.80 |   |
|   | 360   | 18.97  |            | 15.10  | -14.90  |   |
| Initial Height (in)<br>Height Change (in)<br>Ht. After Cons. (in)<br>Initial Area (sq in)<br>Area After Cons. (sq in) |   | 3.062<br>0.077<br>2.985<br>6.339<br>6.088  |            | Init. Vol. (CC<br>Vol. Change<br>Cell Exp. (C<br>Net Change<br>Cons. Vol. (                        | (CC)<br>C)<br>(CC)  | 318.14<br>38.20<br>17.93<br>20.27<br>297.87<br>297.87 |
|   | MLM Da<br>Date:_ <b>9/26/12</b> _                                       | ite:   | 09/26/2012 |  |   | ATT   |





Data Entered By:CALDate:9/25/2012Data Checked By: $\underline{\gamma}m$ Date Checked: $\underline{q} | \frac{2b}{l^2}$ File Name:LKFP5162Date Checked: $\underline{q} | \frac{2b}{l^2}$ 



| CLIENT  | LATA Envi       | ronmental Services-Ky  | JOB NO.  | 2855-02                         |  |
|---|-----------------|--|--|---------------------------------|--|
| BORING N<br>DEPTH<br>SAMPLE N<br>PROJECT<br>LOCATION<br>CONF. PRE | IO,<br>NO.<br>I | MW516<br>40-42'<br>MW516PERM3<br>ERI12-SW-SWMU211B<br>SW Plume RDSI Geotechnical<br>5305 | SAMPLED<br>TEST STA<br>TEST FINI<br>CELL NUM<br>SATURATI<br>TEST TYP | RTED<br>SHED<br>IBER<br>ED TEST | 8/23/12 KD<br>9/13/12 CAL<br>9/15/12 CAL<br>15S<br>Yes<br>TX/Pbp/Tap Water |

| MOISTURE/DENSITY           | BEFORE  | AFTER   |        |
|----------------------------|---------|---------|--------|
| DATA                       | TEST    | TEST    |        |
| Wt. Soil + Moisture (g)    | 706.5   | 704.6   |        |
| Wt. Wet Soil & Pan (g)     | 713.1   | 711.2   |        |
| Wt. Dry Soil & Pan_(g)     | 617.5   | 617.5   |        |
| Wt. Lost Moisture (g)      | 95.6    | 93.7    |        |
| Wt. of Pan Only (g)        | 6.6     | 6.6     |        |
| Wt. of Dry Soil (g)        | 610.9   | 610.9   |        |
| Moisture Content %         | 15.7    | 15.3    |        |
| Wet Density PCF            | 134.8   | 140.4   |        |
| Dry Density PCF            | 116.5   | 121.7   |        |
| Init. Diameter (in)        | 2.862   | (cm)    | 7.269  |
| Init. Area (sq in)         | 6.433   | (sq cm) | 41.507 |
| Init. Height (in)          | 3.104   | (cm)    | 7.884  |
| Vol. Bef. Consol. (cu ft)  | 0.01156 |         |        |
| Vol. After Consol. (cu ft) | 0.01106 |         |        |
| Porosity %                 | 29.92   |         |        |

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# FLOW PUMP CALCULATIONS

| Pump Setting<br>Velocity CM/Sec | 45<br>2.95E-04   |
|---------------------------------|------------------|
| Q (cc/s)                        | 9.44E-06         |
| Height                          | 3.081            |
| Diameter                        | 2.811            |
| Pressure (psi)                  | 0.240            |
| Area after consol. (cm*cm)      | 40.026           |
| Gradient                        | 2.156            |
| Permeability k (cm/s)           | 1.1 <b>E-</b> 07 |
| Permeability k (m/s)            | 1.1E-09          |
| Back Pressure (psi)             | 38.0             |
| Cell Pressure (psi)             | 74.8             |
| Ave. Effective Stress (psi)     | 36.680           |
| Average temperature degree C:   | 23.0             |

## Average temperature degree C:

| Data entry by:        | MLM   | Date:          |
|-----------------------|-------|----------------|
| Checked by: <u>C4</u> | Date: | <u>9/22//2</u> |
| FileName: LKP05163    | -     | <del>,,,</del> |

09/17/2012



| CLIENT LATA En  | vironmental Services-Ky    | JOB NO. 2855-02 |                  |
|-----------------|----------------------------|-----------------|------------------|
| BORING NO.      | MW516                      | SAMPLED         | 8/23/12 KD       |
| DEPTH           | 40-42'                     | TEST STARTED    | 9/13/12 CAL      |
| SAMPLE NO.      | MW516PERM3                 | TEST FINISHED   | 9/15/12 CAL      |
| PROJECT NO.     | ERI12-SW-SWMU211B          | SETUP NO.       | 15S              |
| LOCATION        | SW Plume RDSI Geotechnical | SATURATED TEST  | Yes              |
| CONF. PRES. PSF | 5305                       | TEST TYPE       | TX/Pbp/Tap Water |

# SATURATION DATA

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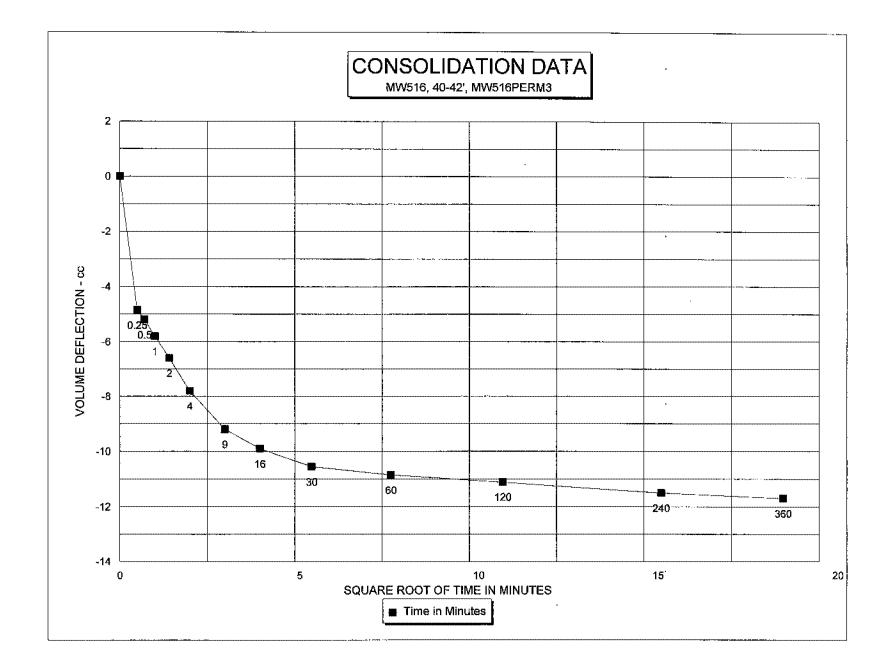
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| Cell<br>Pres.<br>(PSI) | Back<br>Pres.<br>(PSI) | Burette<br>Reading<br>(CC) | Pore<br>Pressure<br>(PSI) |       | (    | Change | в |      |
|------------------------|------------------------|----------------------------|---------------------------|-------|------|--------|---|------|
|                        |                        | Close                      | Open                      | Close | Open |        |   |      |
| 40.0                   | 38.0                   | 3.0                        | 12.8                      |       |      |        |   |      |
| 50.0                   |                        | 13.5                       | 13.7                      | 39.1  | 48.7 | 9.6    |   | 0.96 |

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## CONSOLIDATION DATA

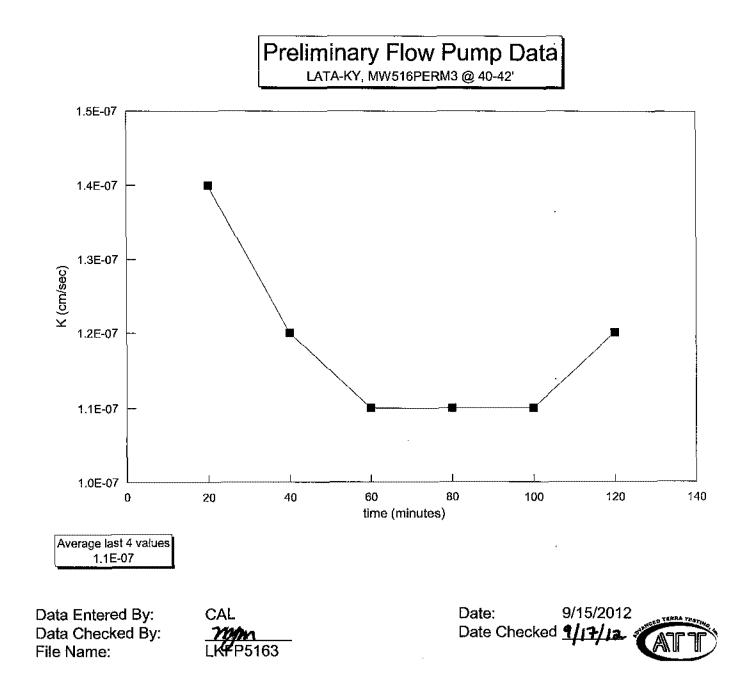
| Elapsed<br>Time<br>(Min)   | SQRT<br>Time<br>(Min)   | Burette Volume<br>Reading Defl.<br>(CC) (cc)         |                                      |
|--|---|--|--------------------------------------|
| 0.00<br>0.25<br>0.5<br>1<br>2<br>4<br>9<br>16<br>30<br>60<br>120<br>240<br>360 | 0.00<br>0.50<br>0.71<br>1.00<br>1.41<br>2.00<br>3.00<br>4.00<br>5.48<br>7.75<br>10.95<br>15.49<br>18.97 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ |                                      |
| <br>MLM Da<br>Date: <u>9/22//.</u>   | 3.104<br>0.023<br>3.081<br>6.433<br>6.204   | Vol. Change (CC)24Cell Exp.(CC)10Net Change(CC)14    | 7.29<br>4.00<br>0.00<br>4.00<br>3.29 |



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| DATE     | 10/23         | /2012          | TIME            | 11:40         |      | WELL ID | MW    | -511            |
|----------|---------------|----------------|-----------------|---------------|------|---------|-------|-----------------|
| ADJ WELL | MW            | -513           | TECH            | J. Brownfield |      | RECD BY | T. N  | Aills           |
|          |               |                |                 |               |      |         |       |                 |
| TIME     | FLOW<br>(gpm) | PRESS<br>(psi) | DTW Adj<br>Well |               | TIME | FLOW    | PRESS | DTW Adj<br>Well |
| 11:40    | 2.5           | 25             | 16.63           |               |      |         |       |                 |
| 11:43    | 2.2           | 25             | 13.31           |               |      |         |       |                 |
| 11:46    | 2.2           | 25             | 12.89           |               |      |         |       |                 |
| 11:49    | 2.2           | 25             | 12.78           |               |      |         |       |                 |
| 11:52    | 3.1           | 50             | 12.42           |               |      |         |       |                 |
| 11:55    | 3.1           | 50             | 11.85           |               |      |         |       |                 |
| 11:58    | 3.1           | 50             | 11.67           |               |      |         |       |                 |
| 12:01    | 3.9           | 75             | 11.14           |               |      |         |       |                 |
| 12:04    | 3.9           | 75             | 10.37           |               |      |         |       |                 |
| 12:07    | 3.9           | 75             | 9.79            |               |      |         |       |                 |
| 12:10    | 4.8           | 100            | 9.55            |               |      |         |       |                 |
| 12:13    | 4.8           | 100            | 9.42            |               |      |         |       |                 |
| 12:16    | 4.8           | 100            | 9.42            |               |      |         |       |                 |
| Te       | st Complete   | e per Ken Da   | ivis            |               |      |         |       |                 |
|          |               |                |                 |               |      |         |       |                 |
|          |               |                |                 |               |      |         |       |                 |
|          |               |                |                 |               |      |         |       |                 |
|          |               |                |                 |               |      |         |       |                 |
|          |               |                |                 |               |      |         |       |                 |
|          |               |                |                 |               |      |         |       |                 |
|          |               |                |                 |               |      |         |       |                 |

# WELL INJECTION TEST RECORD

| DATE                        | 10/23         | 3/2012         | TIME            | 12:30         |      | WELL ID | ELL ID MW-53 |                 |
|-----------------------------|---------------|----------------|-----------------|---------------|------|---------|--------------|-----------------|
| ADJ WELL                    | N,            | /A             | TECH            | J. Brownfield |      | RECD BY | T. Mills     |                 |
|                             |               |                |                 |               |      |         |              |                 |
| TIME                        | FLOW<br>(gpm) | PRESS<br>(psi) | DTW Adj<br>Well |               | TIME | FLOW    | PRESS        | DTW Adj<br>Well |
| 12:35                       | 2.3           | 25             | N/A             |               |      |         |              |                 |
| 12:38                       | 1.5           | 25             | N/A             |               |      |         |              |                 |
| 12:41                       | 1.5           | 25             | N/A             |               |      |         |              |                 |
| 12:44                       | 2.0           | 25             | N/A             |               |      |         |              |                 |
| 12:47                       | 2.2           | 25             | N/A             |               |      |         |              |                 |
| 12:50                       | 2.2           | 25             | N/A             |               |      |         |              |                 |
| 12:53                       | 2.2           | 25             | N/A             |               |      |         |              |                 |
| 12:56                       | 3.3           | 50             | N/A             |               |      |         |              |                 |
| 12:59                       | 3.3           | 50             | N/A             |               |      |         |              |                 |
| 13:02                       | 3.3           | 50             | N/A             |               |      |         |              |                 |
| 13:05                       | 4.1           | 75             | N/A             |               |      |         |              |                 |
| 13:08                       | 4.1           | 75             | N/A             |               |      |         |              |                 |
| 13:11                       | 4.2           | 75             | N/A             |               |      |         |              |                 |
| 13:14                       | 4.7           | 100            | N/A             |               |      |         |              |                 |
| 13:17                       | 4.7           | 100            | N/A             |               |      |         |              |                 |
| 13:20                       | 4.7           | 100            | N/A             |               |      |         |              |                 |
| Test Complete per Ken Davis |               |                |                 |               |      |         |              |                 |
|                             |               |                |                 |               |      |         |              |                 |
|                             |               |                |                 |               |      |         |              |                 |
|                             |               |                |                 |               |      |         |              |                 |
|                             |               |                |                 |               |      |         |              |                 |

# WELL INJECTION TEST RECORD

#### DATE 10/23/2012 TIME 9:00 WELL ID MW-513 MW-511 J. Brownfield T. Mills ADJ WELL TECH **RECD BY** FLOW PRESS DTW Adj DTW Adj PRESS TIME TIME FLOW (gpm) Well Well (psi) 9:30 1.5 25 7.48 9:33 0.5 25 7.48 0.7 25 6.03 9:36 9:39 0.9 25 5.96 9:42 1.0 25 5.90 9:45 1.0 25 5.89 9:48 1.0 25 5.87 9:51 1.9 50 5.81 9:54 1.9 50 5.81 Test Paused Due To Equipment Issue 10:10 1.9 50 5.97 2.0 5.97 10:13 50 2.1 10:16 50 6.01 10:19 3.0 75 5.27 10:22 3.0 75 4.11 10:25 3.1 75 0.00 Test Complete per Ken Davis

| DATE     | 10/23         | /2012          | TIME            | 15:     | 05      | WELL ID | MW    | /-514           |
|----------|---------------|----------------|-----------------|---------|---------|---------|-------|-----------------|
| ADJ WELL | MW-515        | MW-516         | TECH            | J. Brov | vnfield | RECD BY | T. I  | ∕∕ills          |
|          |               |                |                 |         |         | -       |       |                 |
| TIME     | FLOW<br>(gpm) | PRESS<br>(psi) | DTW Adj<br>Well |         | TIME    | FLOW    | PRESS | DTW Adj<br>Well |
| 15:10    | 2.3           | 25             | 1.20/14.28      |         |         |         |       |                 |
| 15:13    | 2.3           | 25             | 0.0/13.27       |         |         |         |       |                 |
| 15:16    | 2.3           | 25             | 0.0/12.91       |         |         |         |       |                 |
| 15:19    | 2.4           | 50             | 0.0/12.67       |         |         |         |       |                 |
| 15:22    | 2.4           | 50             | 0.0/12.42       |         |         |         |       |                 |
| 15:25    | 2.5           | 50             | 0.0/12.29       |         |         |         |       |                 |
| 15:28    | 3.1           | 75             | 0.0/11.99       |         |         |         |       |                 |
| 13:31    | 3.1           | 75             | 0.0/11.93       |         |         |         |       |                 |
| 15:34    | 3.1           | 75             | 0.0/11.86       |         |         |         |       |                 |
| 15:37    | 3.4           | 100            | 0.0/11.78       |         |         |         |       |                 |
| 15:40    | 3.4           | 100            | 0.0/11.76       |         |         |         |       |                 |
| 15:43    | 3.4           | 100            | 0.0/11.74       |         |         |         |       |                 |
| Test Con | nplete Per K  | Cen Davis      |                 |         |         |         |       |                 |
|          |               |                |                 |         |         |         |       |                 |
|          |               |                |                 |         |         |         |       |                 |
|          |               |                |                 |         |         |         |       |                 |
|          |               |                |                 |         |         |         |       |                 |
|          |               |                |                 |         |         |         |       |                 |
|          |               |                |                 |         |         |         |       |                 |
|          |               |                |                 |         |         |         |       |                 |
|          |               |                |                 |         |         |         |       |                 |

| DATE     | 10/23         | /2012          | TIME            | 13:     | 35      | WELL ID | MW    | /-515           |
|----------|---------------|----------------|-----------------|---------|---------|---------|-------|-----------------|
| ADJ WELL | MW-514        | MW-516         | TECH            | J. Brov | vnfield | RECD BY | T. I  | ∕∕ills          |
|          |               |                | -               |         |         | -       |       |                 |
| TIME     | FLOW<br>(gpm) | PRESS<br>(psi) | DTW Adj<br>Well |         | TIME    | FLOW    | PRESS | DTW Adj<br>Well |
| 13:38    | 2.5           | 25             | 8.49/22.31      |         |         |         |       |                 |
| 13:41    | 1.7           | 25             | 8.37/20.91      |         |         |         |       |                 |
| 13:44    | 1.6           | 25             | 5.95/20.98      |         |         |         |       |                 |
| 13:47    | 1.7           | 25             | 0.0/21.46       |         |         |         |       |                 |
| 13:50    | 2.8           | 50             | 0.0/21.62       |         |         |         |       |                 |
| 13:53    | 2.9           | 50             | 0.0/21.73       |         |         |         |       |                 |
| 13:56    | 2.9           | 50             | 0.0/21.82       |         |         |         |       |                 |
| 13:59    | 3.8           | 75             | 0.0/21.90       |         |         |         |       |                 |
| 14:02    | 3.7           | 75             | 0.0/21.98       |         |         |         |       |                 |
| 14:05    | 3.7           | 75             | 0.0/22.02       |         |         |         |       |                 |
| 14:08    | 4.5           | 100            | 0.0/22.10       |         |         |         |       |                 |
| 14:11    | 4.5           | 100            | 0.0/22.14       |         |         |         |       |                 |
| 14:14    | 4.5           | 100            | 0.0/22.16       |         |         |         |       |                 |
| Tes      | st Complete   | e per Ken Da   | avis            |         |         |         |       |                 |
|          |               |                |                 |         |         |         |       |                 |
|          |               |                |                 |         |         |         |       |                 |
|          |               |                |                 |         |         |         |       |                 |
|          |               |                |                 |         |         |         |       |                 |
|          |               |                |                 |         |         |         |       |                 |
|          |               |                |                 |         |         |         |       |                 |
|          |               |                |                 |         |         |         |       |                 |

| DATE     | 10/23         | /2012          | TIME            | 14      | :20     | WELL ID | MM    | /-516           |
|----------|---------------|----------------|-----------------|---------|---------|---------|-------|-----------------|
| ADJ WELL | MW-515        | MW-514         | TECH            | J. Brov | vnfield | RECD BY | Т. Г  | ∕Iills          |
|          |               |                |                 |         |         |         |       |                 |
| TIME     | FLOW<br>(gpm) | PRESS<br>(psi) | DTW Adj<br>Well |         | TIME    | FLOW    | PRESS | DTW Adj<br>Well |
| 14:20    | 2.0           | 25             | 4.21/5.25       |         |         |         |       |                 |
| 14:23    | 1.9           | 25             | 0.0/0.81        |         |         |         |       |                 |
| 14:26    | 1.9           | 25             | 0.0/0.81        |         |         |         |       |                 |
| 14:29    | 1.9           | 25             | 0.0/0.79        |         |         |         |       |                 |
| 14:32    | 3.1           | 50             | 0.0/0.80        |         |         |         |       |                 |
| 14:35    | 3.1           | 50             | 0.0/0.84        |         |         |         |       |                 |
| 14:38    | 3.1           | 50             | 0.0/0.85        |         |         |         |       |                 |
| 14:41    | 3.1           | 75             | 0.0/0.81        |         |         |         |       |                 |
| 14:44    | 3.1           | 75             | 0.0/<0.70       |         |         |         |       |                 |
| 14:47    | 3.1           | 75             | 0.0/<0.50       |         |         |         |       |                 |
| 14:50    | 3.3           | 100            | 0.0/0.0         |         |         |         |       |                 |
| 14:53    | 3.3           | 100            | 0.0/0.0         |         |         |         |       |                 |
| 14:56    | 4.3           | 100            | 0.0/0.0         |         |         |         |       |                 |
| 14:59    | 4.3           | 100            | 0.0/0.0         |         |         |         |       |                 |
| 15:02    | 4.3           | 100            | 0.0/0.0         |         |         |         |       |                 |
| Tes      | st Complete   | e Per Ken Da   | ivis            |         |         |         |       |                 |
|          |               |                |                 |         |         |         |       |                 |
|          |               |                |                 |         |         |         |       |                 |
|          |               |                |                 |         |         |         |       |                 |
|          |               |                |                 |         |         |         |       |                 |
|          |               |                |                 |         |         |         |       |                 |

**APPENDIX G** 

SUMMARY OF SOILS VOC DATA FOR SWMU 211-B

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| Station   | Date<br>Collected | Sample<br>Depth<br>[ft bls] | TCE<br>[µg/kg]  | l | 1,1-DC<br>[µg/kậ |   | cis-1,2<br>DCE<br>[µg/kg | 1 | trans-1<br>DCE<br>[µg/kg |   | V(<br>[µg/l |   |
|-----------|-------------------|-----------------------------|-----------------|---|------------------|---|--------------------------|---|--------------------------|---|-------------|---|
|           |                   | 4.9                         | 27              |   | 1.5              | U | 0.56                     | U | 0.87                     | U | 0.4         | U |
|           |                   | 8.5                         | 78              |   | 1.8              | U | 0.71                     | J | 1.1                      | U | 0.49        | U |
|           |                   | 10.5                        | 150             |   | 1.6              | U | 0.78                     | J | 0.93                     | U | 0.42        | U |
|           |                   | (10.5)DUP                   | 100             |   | 1.7              | U | 0.62                     | U | 0.98                     | U | 0.45        | U |
|           |                   | 19.5                        | <mark>91</mark> |   | 1.4              | U | 0.52                     | U | 0.81                     | U | 0.37        | U |
|           |                   | 23                          | 1,700           |   | 22               | U | 9.5                      | U | 7.4                      | U | 25          | U |
|           | 10/9/2012         | 25.1                        | 19              |   | 1.9              | U | 0.7                      | U | 1.1                      | U | 0.5         | U |
| 211-B-001 | 10/9/2012         | 34                          | 15              |   | 2                | U | 0.74                     | U | 1.2                      | U | 0.53        | U |
|           |                   | 39.5                        | 93              |   | 1.6              | U | 0.61                     | U | 0.95                     | U | 0.43        | U |
|           |                   | 44                          | 310             |   | 25               | U | 11                       | U | 8.3                      | U | 28          | U |
|           |                   | 49.5                        | 61              |   | 1.6              | U | 0.59                     | U | 0.92                     | U | 0.42        | U |
|           |                   | 53                          | <mark>84</mark> |   | 1.8              | U | 0.68                     | U | 1.1                      | U | 0.49        | U |
|           |                   | 55.5                        | 24              |   | 2                | U | 0.73                     | U | 1.1                      | U | 0.52        | U |
|           |                   | 60.5                        | 1.2             | J | 1.7              | U | 0.62                     | U | 0.97                     | U | 0.44        | U |
|           |                   | Average                     | 197             |   | ***              |   | 1                        |   | ***                      |   | ***         |   |
|           |                   | 3                           | 0.41            | U | 1.7              | U | 0.63                     | U | 0.99                     | U | 0.45        | U |
|           |                   | 9                           | 0.36            | U | 1.5              | U | 0.56                     | U | 0.87                     | U | 0.4         | U |
|           |                   | 14                          | 0.35            | U | 1.4              | U | 0.53                     | U | 0.83                     | U | 0.38        | U |
|           |                   | 18.5                        | 2.2             | J | 2.1              | U | 0.77                     | U | 1.2                      | U | 0.55        | U |
|           |                   | 21                          | 170             | J | 23               | U | 9.8                      | U | 7.6                      | U | 26          | U |
|           |                   | 29                          | 1.8             | J | 1.5              | U | 0.55                     | U | 0.87                     | U | 0.4         | U |
| 211-B-002 | 10/10/2012        | 31.5                        | 52              |   | 1.8              | U | 0.68                     | U | 1.1                      | U | 0.49        | U |
| 211-D-002 |                   | 35.5                        | 210             |   | 1.7              | U | 0.64                     | U | 1                        | U | 0.46        | U |
|           |                   | 44.5                        | 93              |   | 1.6              | U | 0.61                     | U | 0.95                     | U | 0.43        | U |
|           |                   | 47.5                        | 23              |   | 1.5              | U | 0.58                     | U | 0.9                      | U | 0.41        | U |
|           |                   | 50.5                        | 0.39            | U | 1.6              | U | 0.6                      | U | 0.94                     | U | 0.43        | U |
|           |                   | 59.5                        | 4.1             | J | 1.9              | U | 0.72                     | U | 1.1                      | U | 0.52        | U |
|           |                   | 62.5                        | 1.8             | J | 2.1              | U | 0.78                     | U | 1.2                      | U | 0.56        | U |
|           |                   | Average                     | 43              |   | ***              |   | ***                      |   | ***                      |   | ***         |   |

#### Summary of Soils VOC Data for SWMU 211-B

| Station   | Date<br>Collected | Sample<br>Depth<br>[ft bls] | TCE<br>[µg/kg] |   | 1,1-D(<br>[μg/k |   | cis-1,2<br>DCE<br>[µg/kş | 1 | trans-1<br>DCE<br>[µg/kg | 1 | V<br>[µg/] |   |
|-----------|-------------------|-----------------------------|----------------|---|-----------------|---|--------------------------|---|--------------------------|---|------------|---|
|           |                   | 4                           | 0.41           | U | 1.7             | U | 0.63                     | U | 0.98                     | U | 0.45       | U |
|           |                   | 9                           | 0.41           | U | 1.7             | U | 0.63                     | U | 0.98                     | U | 0.45       | U |
|           |                   | 14.5                        | 1              | J | 1.6             | U | 0.6                      | U | 0.93                     | U | 0.43       | U |
|           |                   | 19.5                        | 0.46           | J | 1.4             | U | 0.51                     | U | 0.8                      | U | 0.37       | U |
|           |                   | (19.5)DUP                   | 0.5            | J | 1.5             | U | 0.56                     | U | 0.88                     | U | 0.4        | U |
| 211-B-003 | 10/10/2012        | 23                          | 0.35           | U | 1.4             | U | 0.54                     | U | 0.84                     | U | 0.38       | U |
|           |                   | 28.5                        | 0.33           | U | 1.4             | U | 0.51                     | U | 0.79                     | U | 0.36       | U |
|           |                   | 34                          | 0.87           | J | 1.3             | U | 0.5                      | U | 0.78                     | U | 0.36       | U |
|           |                   | 39                          | 17             |   | 1.6             | U | 0.61                     | U | 0.95                     | U | 0.43       | U |
|           |                   | 40.5                        | 19             |   | 1.4             | U | 0.51                     | U | 0.8                      | U | 0.37       | U |
|           |                   |                             |                |   |                 |   |                          |   |                          |   |            |   |
|           |                   | 49.5                        | 17             |   | 1.7             | U | 0.64                     | U | 1                        | U | 0.46       | U |
|           |                   | 52                          | 61             |   | 1.7             | U | 0.63                     | U | 0.99                     | U | 0.45       | U |
|           |                   | 58.5                        | 9              | J | 1.5             | U | 0.55                     | U | 0.86                     | U | 0.39       | U |
|           |                   | Average                     | 10             |   | ***             |   | ***                      |   | ***                      |   | ***        |   |
|           |                   | 3.5                         | 12             |   | 1.4             | U | 1.4                      | J | 0.8                      | U | 0.37       | U |
|           |                   | 7                           | 30             |   | 1.6             | U | 20                       |   | 0.93                     | U | 0.42       | U |
|           |                   | 14.5                        | 1,800          |   | 25              | U | 66                       | J | 8.3                      | U | 28         | U |
|           |                   | 17.5                        | 72             |   | 1.6             | U | 4.2                      | J | 0.96                     | U | 0.44       | U |
|           |                   | 20.1                        | 380            |   | 25              | U | 11                       | U | 8.5                      | U | 29         | U |
|           |                   | 25.5                        | 920            |   | 21              | U | 9                        | U | 7                        | U | 24         | U |
| 211-B-004 | 10/11/2012        | 30.1                        | 900            |   | 27              | U | 11                       | U | 8.9                      | U | 30         | U |
| 211 D 004 |                   | 35.1                        | 250            |   | 24              | U | 10                       | U | 7.9                      | U | 27         | U |
|           |                   | 41                          | 620            |   | 24              | U | 10                       | U | 8                        | U | 27         | U |
|           |                   | 49.9                        | 270            |   | 23              | U | 9.8                      | U | 7.7                      | U | 26         | U |
|           |                   | 51                          | 19             | U | 26              | U | 11                       | U | 8.8                      | U | 30         | U |
|           |                   | 55.1                        | 75             |   | 1.5             | U | 0.57                     | U | 0.9                      | U | 0.41       | U |
|           |                   | 62                          | 100            | J | 23              | U | 10                       | U | 7.8                      | U | 26         | U |
|           |                   | Average                     | <b>418</b>     |   | ***             |   | 10                       |   | ***                      |   | ***        |   |

Summary of Soils VOC Data for SWMU 211-B (Continued)

| Station   | Date<br>Collected | Sample<br>Depth<br>[ft bls] | TCE<br>[µg/kg] |   | 1,1-DC<br>[µg/kş |   | cis-1,2<br>DCE<br>[µg/kg |   | trans-1,<br>DCE<br>[µg/kg |   | V(<br>[µg/l |   |
|-----------|-------------------|-----------------------------|----------------|---|------------------|---|--------------------------|---|---------------------------|---|-------------|---|
|           |                   | 4.9                         | 46             |   | 1.8              | U | 6.8                      | J | 1                         | U | 0.47        | U |
|           |                   | 5.1                         | 71             |   | 1.7              | U | 8.3                      | J | 0.97                      | U | 0.45        | U |
|           |                   | 13.5                        | 340            |   | 26               | U | 11                       | U | 8.6                       | U | 29          | U |
|           |                   | 18                          | 130            |   | 1.8              | U | 0.66                     | U | 1                         | U | 0.47        | U |
|           |                   | 23                          | 3,100          |   | 24               | U | 10                       | U | 7.9                       | U | 27          | U |
|           |                   | (29.5)DUP                   | 2,900          |   | 33               | U | 14                       | U | 11                        | U | 38          | U |
|           | 10/15/2012        | 29.5                        | 700            |   | 23               | U | 10                       | U | 7.9                       | U | 27          | U |
| 211-B-005 | 10/13/2012        | 30.5                        | 1,400          |   | 32               | U | 14                       | U | 11                        | U | 36          | U |
|           |                   | 35.5                        | 380            |   | 26               | U | 11                       | U | 8.6                       | U | 29          | U |
|           |                   | 40.5                        | 1,500          |   | 28               | U | 12                       | U | 9.6                       | U | 32          | U |
|           |                   | 48                          | 690            |   | 23               | U | 10                       | U | 7.8                       | U | 26          | U |
|           |                   | 50.5                        | 360            |   | 26               | U | 11                       | U | 8.7                       | U | 30          | U |
|           |                   | 59                          | 340            |   | 25               | U | 11                       | U | 8.5                       | U | 29          | U |
|           |                   | 60.1                        | 120            | J | 46               | U | 20                       | U | 15                        | U | 52          | U |
|           |                   | Average                     | 863            |   | ***              |   | 6                        |   | ***                       |   | ***         |   |
|           |                   | 4.5                         | 0.41           | U | 1.7              | U | 0.63                     | U | 0.98                      | U | 0.45        | U |
|           |                   | 9                           | 0.41           | U | 1.7              | U | 0.63                     | U | 0.99                      | U | 0.45        | U |
|           |                   | 13.5                        | 4.7            | J | 1.6              | U | 0.61                     | U | 0.95                      | U | 0.43        | U |
|           |                   | 17.5                        | 29             |   | 1.6              | U | 0.59                     | U | 0.92                      | U | 0.42        | U |
|           |                   | 21                          | 92             |   | 1.9              | U | 0.7                      | U | 1.1                       | U | 0.5         | U |
|           |                   | 29.5                        | 25             |   | 1.7              | U | 0.64                     | U | 1                         | U | 0.46        | U |
| 211-B-006 | 10/15/2012        | 31                          | 3.3            | J | 2                | U | 0.73                     | U | 1.1                       | U | 0.52        | U |
| 211-D-000 |                   | 37.5                        | 4              | J | 1.5              | U | 0.56                     | U | 0.87                      | U | 0.4         | U |
|           |                   | 44.9                        | 14             |   | 1.6              | U | 0.59                     | U | 0.93                      | U | 0.43        | U |
|           |                   | 49.5                        | 11             |   | 1.8              | U | 0.67                     | U | 1                         | U | 0.48        | U |
|           |                   | 52.5                        | 7.6            | J | 1.7              | U | 0.62                     | U | 0.98                      | U | 0.45        | U |
|           |                   | 59                          | 1.2            | J | 1.7              | U | 0.65                     | U | 1                         | U | 0.46        | U |
|           |                   | 62                          | 0.47           | U | 1.9              | U | 0.73                     | U | 1.1                       | U | 0.52        | U |
|           |                   | Average                     | 15             |   | ***              |   | ***                      |   | ***                       |   | ***         |   |

Summary of Soils VOC Data for SWMU 211-B (Continued)

| Station   | Date<br>Collected | Sample<br>Depth<br>[ft bls] | TCE<br>[µg/kg] | 1,1-DCE<br>[µg/kg] | <i>cis-</i> 1,2-<br>DCE<br>[µg/kg] | trans-1,2-<br>DCE<br>[μg/kg] | VC<br>[µg/kg] |
|-----------|-------------------|-----------------------------|----------------|--------------------|------------------------------------|------------------------------|---------------|
|           |                   | 2.5                         | 0.35 U         | 1.4 U              | 0.54 U                             | 0.85 U                       | 0.39 U        |
|           |                   | 5.5                         | 0.32 U         | 1.3 U              | 0.49 U                             | 0.77 U                       | 0.35 U        |
|           |                   | 11                          | 0.39 U         | 1.6 U              | 0.6 U                              | 0.94 U                       | 0.43 U        |
|           |                   | 17.5                        | 0.4 U          | 1.7 U              | 0.62 U                             | 0.97 U                       | 0.44 U        |
|           |                   | 23                          | 0.98 J         | 1.5 U              | 0.55 U                             | 0.86 U                       | 0.39 U        |
|           |                   | (23)DUP                     | 0.73 J         | 1.4 U              | 0.52 U                             | 0.82 U                       | 0.37 U        |
|           | 10/16/2012        | 25.1                        | 0.51 J         | 1.4 U              | 0.53 U                             | 0.83 U                       | 0.38 U        |
| 211-B-007 | 10/10/2012        | 33.5                        | 15             | 1.6 U              | 0.61 U                             | 0.95 U                       | 0.44 U        |
|           |                   | 35.5                        | 7.4 J          | 1.5 U              | 0.56 U                             | 0.88 U                       | 0.4 U         |
|           |                   | 44.5                        | 9.7 J          | 1.6 U              | 0.59 U                             | 0.93 U                       | 0.42 U        |
|           |                   | 49                          | 0.35 U         | 1.4 U              | 0.54 U                             | 0.84 U                       | 0.39 U        |
|           |                   | 53.5                        | 7.3 J          | 1.7 U              | 0.64 U                             | 0.99 U                       | 0.46 U        |
|           |                   | 55.1                        | 6.3 J          | 1.7 U              | 0.63 U                             | 0.99 U                       | 0.45 U        |
|           |                   | 60.1                        | 5.1 J          | 1.6 U              | 0.61 U                             | 0.96 U                       | 0.44 U        |
|           |                   | Average                     | 4              | ***                | ***                                | ***                          | ***           |
|           |                   | 0.5                         | 0.42 U         | 1.7 U              | 0.65 U                             | 1 U                          | 0.46 U        |
|           |                   | (8)DUP                      | 0.37 U         | 1.5 U              | 0.57 U                             | 0.89 U                       | 0.41 U        |
|           |                   | 8                           | 0.39 U         | 1.6 U              | 0.6 U                              | 0.95 U                       | 0.43 U        |
|           |                   | 12.5                        | 0.38 U         | 1.6 U              | 0.58 U                             | 0.91 U                       | 0.42 U        |
|           |                   | 16.5                        | 0.35 U         | 1.5 U              | 0.54 U                             | 0.85 U                       | 0.39 U        |
|           |                   | 24                          | 5.2 J          | 1.7 U              | 0.63 U                             | 0.99 U                       | 0.45 U        |
|           | 10/9/2012         | 28.5                        | 0.36 U         | 1.5 U              | 0.55 U                             | 0.86 U                       | 0.39 U        |
| 211-B-008 | 10/9/2012         | 32                          | 0.41 U         | 1.7 U              | 0.63 U                             | 0.98 U                       | 0.45 U        |
|           |                   | 37                          | 0.39 U         | 1.6 U              | 0.61 U                             | 0.95 U                       | 0.43 U        |
|           |                   | 40.1                        | 0.4 U          | 1.7 U              | 0.62 U                             | 0.97 U                       | 0.44 U        |
|           |                   | 48                          | 0.37 U         | 1.5 U              | 0.56 U                             | 0.88 U                       | 0.4 U         |
|           |                   | 50.5                        | 0.41 U         | 1.7 U              | 0.64 U                             | 1 U                          | 0.46 U        |
|           |                   | 58.5                        | 0.43 U         | 1.8 U              | 0.66 U                             | 1 U                          | 0.47 U        |
|           |                   | 62.5                        | 0.43 U         | 1.8 U              | 0.67 U                             | 1 U                          | 0.48 U        |
|           |                   | Average                     | 0.6            | ***                | ***                                | ***                          | ***           |

Summary of Soils VOC Data for SWMU 211-B (Continued)

| Station            | Date<br>Collected | Sample<br>Depth<br>[ft bls] | TCE<br>[µg/kg] | ] | 1,1-DC<br>[µg/kậ |   | cis-1,2<br>DCE<br>[µg/kg |   | trans-1<br>DCE<br>[µg/kg |   | V(<br>[µg/! |   |
|--------------------|-------------------|-----------------------------|----------------|---|------------------|---|--------------------------|---|--------------------------|---|-------------|---|
|                    |                   | 4                           | 3              | J | 1.8              | U | 0.66                     | U | 1                        | U | 0.47        | U |
|                    |                   | 6.5                         | 3.5            | J | 1.8              | U | 0.65                     | U | 1                        | U | 0.47        | U |
|                    |                   | 14.5                        | 10             |   | 1.6              | U | 0.87                     | J | 0.92                     | U | 0.42        | U |
|                    |                   | 16                          | 8.4            | J | 1.5              | U | 0.56                     | U | 0.88                     | U | 0.4         | U |
|                    |                   | 22                          | 0.38           | U | 1.6              | U | 0.58                     | U | 0.91                     | U | 0.42        | U |
|                    |                   | 28.5                        | 1.9            | J | 1.6              | U | 0.59                     | U | 0.93                     | U | 0.42        | U |
|                    | 10/8/2012         | (34.5)DUP                   | 0.46           | U | 1.9              | U | 0.7                      | U | 1.1                      | U | 0.5         | U |
| 211-B-009          | 10/0/2012         | 34.5                        | 0.4            | U | 1.7              | U | 0.62                     | U | 0.98                     | U | 0.45        | U |
|                    |                   | 36                          | 0.35           | U | 1.4              | U | 0.54                     | U | 0.84                     | U | 0.39        | U |
|                    |                   | 44                          | 0.41           | U | 1.7              | U | 0.63                     | U | 0.99                     | U | 0.45        | U |
|                    |                   | 49.5                        | 0.41           | U | 1.7              | U | 0.63                     | U | 0.98                     | U | 0.45        | U |
|                    |                   | 51.5                        | 0.39           | U | 1.6              | U | 0.6                      | U | 0.94                     | U | 0.43        | U |
|                    |                   | 59.5                        | 0.41           | U | 1.7              | U | 0.63                     | U | 0.99                     | U | 0.45        | U |
|                    |                   | 62                          | 0.4            | U | 1.6              | U | 0.61                     | U | 0.96                     | U | 0.44        | U |
|                    |                   | Average                     | 2              |   | ***              |   | 0.3                      |   | ***                      |   | ***         |   |
|                    |                   | 4                           | 0.38           | U | 1.6              | U | 0.58                     | U | 0.91                     | U | 0.42        | U |
|                    |                   | 9.9                         | 2.1            | J | 1.7              | U | 0.62                     | U | 0.97                     | U | 0.44        | U |
|                    |                   | 14                          | 8.4            | J | 1.5              | U | 0.63                     | J | 0.86                     | U | 0.39        | U |
|                    |                   | 16                          | 1.7            | J | 1.5              | U | 0.54                     | U | 0.85                     | U | 0.39        | U |
|                    |                   | 20.5                        | 2.4            | J | 1.5              | U | 0.57                     | U | 0.89                     | U | 0.41        | U |
|                    |                   | 28.5                        | 9.7            | J | 1.7              | U | 0.64                     | U | 1                        | U | 0.46        | U |
| 211-B-010          | 10/5/2012         | 31                          | 0.39           | U | 1.6              | U | 0.6                      | U | 0.94                     | U | 0.43        | U |
| 211- <b>D</b> -010 |                   | 39                          | 2.3            | J | 1.5              | U | 0.55                     | U | 0.86                     | U | 0.4         | U |
|                    |                   | 41                          | 3.2            | J | 1.6              | U | 0.59                     | U | 0.92                     | U | 0.42        | U |
|                    |                   | 46                          | 3              | J | 1.5              | U | 0.55                     | U | 0.86                     | U | 0.39        | U |
|                    |                   | 51.5                        | 4              | J | 1.5              | U | 0.55                     | U | 0.86                     | U | 0.39        | U |
|                    |                   | 59.5                        | 1.7            | J | 1.6              | U | 0.58                     | U | 0.91                     | U | 0.42        | U |
|                    |                   | 62                          | 0.62           | J | 1.7              | U | 0.63                     | U | 0.99                     | U | 0.45        | U |
|                    |                   | Average                     | 3              |   | ***              |   | 0.3                      |   | ***                      |   | ***         |   |

Summary of Soils VOC Data for SWMU 211-B (Continued)

| Station            | Date<br>Collected | Sample<br>Depth<br>[ft bls] | TCE<br>[µg/kg] |   | 1,1-DC<br>[µg/kį |   | cis-1,2<br>DCE<br>[µg/kg |   | trans-1<br>DCE<br>[µg/kg |   | V(<br>[µg/] |   |
|--------------------|-------------------|-----------------------------|----------------|---|------------------|---|--------------------------|---|--------------------------|---|-------------|---|
|                    |                   | 4                           | 0.41           | U | 1.7              | U | 0.63                     | U | 0.99                     | U | 0.45        | U |
|                    |                   | 9                           | 4.3            | J | 1.8              | U | 0.67                     | U | 1.1                      | U | 0.48        | U |
|                    |                   | 14.5                        | 15             |   | 1.4              | U | 0.54                     | U | 0.84                     | U | 0.38        | U |
|                    |                   | 19.5                        | 12             |   | 1.5              | U | 0.57                     | U | 0.9                      | U | 0.41        | U |
|                    |                   | 20.5                        | 15             |   | 1.3              | U | 0.5                      | U | 0.78                     | U | 0.36        | U |
|                    |                   | (20.5)DUP                   | 5.8            | J | 1.5              | U | 0.56                     | U | 0.87                     | U | 0.4         | U |
|                    | 10/8/2012         | 29.5                        | 1.6            | J | 1.7              | U | 0.63                     | U | 0.99                     | U | 0.45        | U |
| 211-B-011          | 10/0/2012         | 32                          | 0.36           | U | 1.5              | U | 0.55                     | U | 0.87                     | U | 0.4         | U |
|                    |                   | 39                          | 0.84           | J | 1.6              | U | 0.59                     | U | 0.92                     | U | 0.42        | U |
|                    |                   | 44                          | 1.5            | J | 1.5              | U | 0.56                     | U | 0.87                     | U | 0.4         | U |
|                    |                   | 45.1                        | 2.4            | J | 1.6              | U | 0.61                     | U | 0.96                     | U | 0.44        | U |
|                    |                   | 51                          | 2.2            | J | 1.4              | U | 0.53                     | U | 0.83                     | U | 0.38        | U |
|                    |                   | 59                          | 0.39           | U | 1.6              | U | 0.61                     | U | 0.95                     | U | 0.44        | U |
|                    |                   | 64.9                        | 2              | J | 1.7              | U | 0.64                     | U | 1                        | U | 0.46        | U |
|                    |                   | Average                     | 5              |   | ***              |   | ***                      |   | ***                      |   | ***         |   |
|                    |                   | 2                           | 0.38           | U | 1.6              | U | 0.59                     | U | 0.93                     | U | 0.42        | U |
|                    |                   | 5.5                         | 0.38           | U | 1.6              | U | 0.58                     | U | 0.92                     | U | 0.42        | U |
|                    |                   | 10.1                        | 0.4            | U | 1.7              | U | 0.62                     | U | 0.96                     | U | 0.44        | U |
|                    |                   | 15.1                        | 0.34           | U | 1.4              | U | 0.52                     | U | 0.82                     | U | 0.38        | U |
|                    |                   | 23.5                        | 0.43           | U | 1.8              | U | 0.67                     | U | 1                        | U | 0.48        | U |
|                    |                   | 29.5                        | 0.36           | U | 1.5              | U | 0.56                     | U | 0.88                     | U | 0.4         | U |
| 211-B-012          | 10/4/2012         | 32                          | 0.89           | J | 1.5              | U | 0.56                     | U | 0.88                     | U | 0.4         | U |
| 211- <b>D</b> -012 |                   | 39                          | 4.6            | J | 1.9              | U | 0.7                      | U | 1.1                      | U | 0.5         | U |
|                    |                   | 40.1                        | 5.9            | J | 1.5              | U | 0.54                     | U | 0.85                     | U | 0.39        | U |
|                    |                   | 49.9                        | 0.39           | U | 1.6              | U | 0.6                      | U | 0.93                     | U | 0.43        | U |
|                    |                   | 50.5                        | 0.39           | U | 1.6              | U | 0.6                      | U | 0.94                     | U | 0.43        | U |
|                    |                   | 59                          | 0.43           | U | 1.8              | U | 0.66                     | U | 1                        | U | 0.47        | U |
|                    |                   | 61                          | 0.39           | U | 1.6              | U | 0.6                      | U | 0.94                     | U | 0.43        | U |
|                    |                   | Average                     | 1.0            |   | ***              |   | ***                      |   | ***                      |   | ***         |   |

Summary of Soils VOC Data for SWMU 211-B (Continued)

| Station   | Date<br>Collected | Sample<br>Depth<br>[ft bls] | TCE<br>[µg/kg] |   | 1,1-D(<br>[µg/k |   | cis-1,2<br>DCE<br>[µg/kg | , | trans-1<br>DCE<br>[µg/kş |   | V(<br>[µg/l |   |
|-----------|-------------------|-----------------------------|----------------|---|-----------------|---|--------------------------|---|--------------------------|---|-------------|---|
|           |                   | 1.5                         | 0.38           | U | 1.6             | U | 0.58                     | U | 0.91                     | U | 0.42        | U |
|           |                   | 9                           | 0.41           | U | 1.7             | U | 0.63                     | U | 0.98                     | U | 0.45        | U |
|           |                   | 14                          | 0.44           | U | 1.8             | U | 0.67                     | U | 1.1                      | U | 0.48        | U |
|           |                   | (16)DUP                     | 0.39           | U | 1.6             | U | 0.6                      | U | 0.95                     | U | 0.43        | U |
|           |                   | 16                          | 0.43           | U | 1.8             | U | 0.66                     | U | 1                        | U | 0.48        | U |
|           |                   | 21                          | 0.47           | U | 1.9             | U | 0.72                     | U | 1.1                      | U | 0.52        | U |
|           | 10/4/2012         | 28                          | 0.33           | U | 1.4             | U | 0.51                     | U | 0.8                      | U | 0.37        | U |
| 211-B-013 | 10/4/2012         | 30.1                        | 0.35           | U | 1.5             | U | 0.54                     | U | 0.85                     | U | 0.39        | U |
|           |                   | 36.5                        | 0.35           | U | 1.4             | U | 0.54                     | U | 0.84                     | U | 0.38        | U |
|           |                   | 43.5                        | 1.2            | J | 1.5             | U | 0.57                     | U | 0.9                      | U | 0.41        | U |
|           |                   | 48                          | 0.31           | U | 1.3             | U | 0.47                     | U | 0.74                     | U | 0.34        | U |
|           |                   | 50.1                        | 0.42           | U | 1.7             | U | 0.64                     | U | 1                        | U | 0.46        | U |
|           |                   | 59.5                        | 0.37           | U | 1.5             | U | 0.57                     | U | 0.89                     | U | 0.41        | U |
|           |                   | 61.5                        | 0.39           | U | 1.6             | U | 0.61                     | U | 0.95                     | U | 0.43        | U |
|           |                   | Average                     | 0.3            |   | ***             |   | ***                      |   | ***                      |   | ***         |   |
|           |                   | 3                           | 1.6            | J | 1.9             | U | 4.5                      | J | 1.1                      | U | 0.5         | U |
|           |                   | 5.1                         | 2.2            | J | 1.7             | U | 2.5                      | J | 0.98                     | U | 0.45        | U |
|           |                   | 13.5                        | 4.9            | J | 1.6             | U | 0.73                     | J | 0.93                     | U | 0.43        | U |
|           |                   | 19.9                        | 1              | J | 1.5             | U | 0.56                     | U | 0.87                     | U | 0.4         | U |
|           |                   | 21.5                        | 170            |   | 1.5             | U | 6.1                      | J | 0.85                     | U | 0.39        | U |
|           |                   | 29.5                        | 120            |   | 1.5             | U | 4.7                      | J | 0.86                     | U | 0.39        | U |
| 211-B-015 | 10/16/2012        | 30.5                        | 5.4            | J | 2               | U | 0.74                     | U | 1.2                      | U | 0.53        | U |
| 211-D-015 |                   | 37                          | 5.5            | J | 1.4             | U | 0.53                     | U | 0.84                     | U | 0.38        | U |
|           |                   | 41.5                        | 37             |   | 1.7             | U | 0.91                     | J | 0.98                     | U | 0.45        | U |
|           |                   | 48.5                        | 17             |   | 1.5             | U | 0.57                     | U | 0.9                      | U | 0.41        | U |
|           |                   | 52                          | 39             |   | 1.7             | U | 0.63                     | U | 0.99                     | U | 0.45        | U |
|           |                   | 56                          | 42             |   | 1.7             | U | 0.63                     | U | 0.99                     | U | 0.45        | U |
|           |                   | 60.5                        | 67             |   | 1.6             | U | 0.61                     | U | 0.95                     | U | 0.43        | U |
|           |                   | Average                     | 39             |   | ***             |   | 2                        |   | ***                      |   | ***         |   |

Summary of Soils VOC Data for SWMU 211-B (Continued)

| Station   | Date<br>Collected | Sample<br>Depth<br>[ft bls] | TCE<br>[µg/kg] |   | 1,1-DC<br>[µg/kş |   | <i>cis</i> -1,2<br>DCE<br>[µg/kg |   | trans-1<br>DCE<br>[µg/kg |   | V(<br>[µg/] |   |
|-----------|-------------------|-----------------------------|----------------|---|------------------|---|----------------------------------|---|--------------------------|---|-------------|---|
|           |                   | 1                           | 0.43           | U | 1.8              | U | 0.65                             | U | 1                        | U | 0.47        | U |
|           |                   | 5.1                         | 0.43           | U | 1.8              | U | 0.67                             | U | 1                        | U | 0.48        | U |
|           |                   | 14                          | 7.7            | J | 1.4              | U | 0.53                             | U | 0.83                     | U | 0.38        | U |
|           |                   | (16)DUP                     | 0.33           | U | 1.4              | U | 0.52                             | U | 0.81                     | U | 0.37        | U |
|           |                   | 16                          | 3              | J | 1.6              | U | 0.6                              | U | 0.93                     | U | 0.43        | U |
|           |                   | 21.5                        | 19             |   | 1.4              | U | 0.52                             | U | 0.82                     | U | 0.37        | U |
|           | 10/17/2012        | 29.5                        | 23             |   | 1.5              | U | 1.1                              | J | 0.88                     | U | 0.4         | U |
| 211-B-016 | 10/17/2012        | 33.5                        | 16             |   | 1.8              | U | 0.87                             | J | 1                        | U | 0.47        | U |
|           |                   | 36.5                        | 18             |   | 1.6              | U | 0.6                              | U | 0.94                     | U | 0.43        | U |
|           |                   | 43.5                        | 23             |   | 1.6              | U | 0.58                             | U | 0.91                     | U | 0.42        | U |
|           |                   | 48.5                        | 31             |   | 1.7              | U | 0.64                             | U | 1                        | U | 0.46        | U |
|           |                   | 50.1                        | 42             |   | 1.8              | U | 0.67                             | U | 1                        | U | 0.48        | U |
|           |                   | 55.1                        | 20             |   | 1.8              | U | 0.69                             | U | 1.1                      | U | 0.49        | U |
|           |                   | 60.1                        | 4.3            | J | 1.7              | U | 0.63                             | U | 0.98                     | U | 0.45        | U |
|           |                   | Average                     | 15             |   | ***              |   | 0.4                              |   | ***                      |   | ***         |   |
|           |                   | 4                           | 6.1            | J | 1.5              | U | 2.4                              | J | 0.89                     | U | 0.41        | U |
|           |                   | 8                           | 26             |   | 1.7              | U | 1.3                              | J | 0.97                     | U | 0.44        | U |
|           |                   | 14                          | 28             |   | 1.8              | U | 0.69                             | U | 1.1                      | U | 0.49        | U |
|           |                   | 16                          | 13             |   | 1.5              | U | 0.55                             | U | 0.86                     | U | 0.39        | U |
|           |                   | 23.5                        | 13             |   | 1.5              | U | 0.55                             | U | 0.86                     | U | 0.39        | U |
|           |                   | 29.9                        | 16             |   | 1.7              | U | 0.64                             | U | 1                        | U | 0.46        | U |
| 211-B-017 | 10/17/2012        | 30.5                        | 39             |   | 2                | U | 0.73                             | U | 1.1                      | U | 0.53        | U |
| 211 0 017 |                   | 35.1                        | 8.9            | J | 1.7              | U | 0.63                             | U | 0.98                     | U | 0.45        | U |
|           |                   | 44.5                        | <b>120</b>     |   | 1.7              | U | 0.64                             | U | 1                        | U | 0.46        | U |
|           |                   | 48                          | 37             |   | 1.6              | U | 0.61                             | U | 0.96                     | U | 0.44        | U |
|           |                   | 52                          | 20             |   | 1.5              | U | 0.58                             | U | 0.9                      | U | 0.41        | U |
|           |                   | 56                          | 3.4            | J | 1.8              | U | 0.69                             | U | 1.1                      | U | 0.49        | U |
|           | -                 | 62.5                        | 0.38           | U | 1.6              | U | 0.59                             | U | 0.93                     | U | 0.42        | U |
|           |                   | Average                     | 25             |   | ***              |   | 0.6                              |   | ***                      |   | ***         |   |

Summary of Soils VOC Data for SWMU 211-B (Continued)

| Station   | Date<br>Collected | Sample<br>Depth<br>[ft bls] | TCE<br>[µg/kg] |   | 1,1-DC<br>[µg/kş |   | cis-1,2<br>DCE<br>[µg/kg] |   | trans-1<br>DCE<br>[µg/kg |   | V(<br>[µg/] |   |
|-----------|-------------------|-----------------------------|----------------|---|------------------|---|---------------------------|---|--------------------------|---|-------------|---|
|           |                   | 3.5                         | 2.5            | J | 1.7              | U | 0.62                      | U | 0.97                     | U | 0.45        | U |
|           |                   | 4.9                         | 3.3            | J | 1.7              | U | 0.64                      | U | 1                        | U | 0.46        | U |
|           |                   | 14                          | 0.59           | J | 1.4              | U | 0.53                      | U | 0.83                     | U | 0.38        | U |
|           |                   | 19.5                        | 0.36           | U | 1.5              | U | 0.55                      | U | 0.86                     | U | 0.39        | U |
|           |                   | 21                          | 28             |   | 1.4              | U | 0.52                      | U | 0.81                     | U | 0.37        | U |
|           |                   | 28                          | 13             |   | 2                | U | 0.76                      | U | 1.2                      | U | 0.54        | U |
| 211-B-018 | 10/18/2012        | 30.1                        | 2.2            | J | 1.5              | U | 0.57                      | U | 0.89                     | U | 0.41        | U |
| 211-D-016 |                   | 37.5                        | 1.9            | J | 1.7              | U | 0.63                      | U | 0.99                     | U | 0.45        | U |
|           |                   | 40.5                        | 2              | J | 1.7              | U | 0.62                      | U | 0.97                     | U | 0.45        | U |
|           |                   | 47.5                        | 0.37           | U | 1.5              | U | 0.57                      | U | 0.9                      | U | 0.41        | U |
|           |                   | 53.5                        | 0.46           | U | 1.9              | U | 0.71                      | U | 1.1                      | U | 0.51        | U |
|           |                   | 58                          | 0.38           | U | 1.6              | U | 0.58                      | U | 0.91                     | U | 0.41        | U |
|           |                   | 60.1                        | 0.82           | U | 3.4              | U | 1.3                       | U | 2                        | U | 0.9         | U |
|           |                   | Average                     | 4              |   | ***              |   | ***                       |   | ***                      |   | ***         |   |
|           |                   | 2.5                         | 10             |   | 1.5              | U | 1                         | J | 0.9                      | U | 0.41        | U |
|           |                   | (2.5)DUP                    | 6.7            | J | 1.7              | U | 0.66                      | J | 1                        | U | 0.46        | U |
|           |                   | 9.5                         | 28             |   | 1.5              | U | 7                         | J | 0.9                      | U | 0.41        | U |
|           |                   | 12                          | 110            |   | 1.8              | U | 26                        |   | 1.1                      | U | 0.49        | U |
|           |                   | 19.5                        | 3.2            | J | 1.3              | U | 0.5                       | U | 0.78                     | U | 0.36        | U |
|           |                   | 23                          | 2,700          |   | 22               | U | 9.3                       | U | 7.3                      | U | 25          | U |
|           | 10/18/2012        | 25.1                        | 13,000         |   | 54               | U | 23                        | U | 18                       | U | 62          | U |
| 211-B-019 | 10/10/2012        | 32                          | 170            |   | 1.4              | U | 2.4                       | J | 0.82                     | U | 0.37        | U |
|           |                   | 37                          | 100            |   | 1.4              | U | 1.4                       | J | 0.84                     | U | 0.38        | U |
|           |                   | 40.5                        | 170            |   | 1.9              | U | 1.6                       | J | 1.1                      | U | 0.52        | U |
|           |                   | 45.1                        | 130            |   | 1.5              | U | 0.58                      | J | 0.87                     | U | 0.4         | U |
|           |                   | 54                          | 44             |   | 1.5              | U | 0.57                      | U | 0.89                     | U | 0.41        | U |
|           |                   | 58                          | 22             |   | 1.5              | U | 0.56                      | U | 0.88                     | U | 0.4         | U |
|           |                   | 64.5                        | 0.46           | U | 1.9              | U | 0.71                      | U | 1.1                      | U | 0.51        | U |
|           |                   | Average                     | 1,178          |   | ***              |   | 4                         |   | ***                      |   | ***         |   |

Summary of Soils VOC Data for SWMU 211-B (Continued)

| Station   | Date<br>Collected | Sample<br>Depth<br>[ft bls] | TCE<br>[µg/kg] | 1,1-DCE<br>[µg/kg] | <i>cis</i> -1,2-<br>DCE<br>[µg/kg] | trans-1,2-<br>DCE<br>[μg/kg] | VC<br>[µg/kg] |
|-----------|-------------------|-----------------------------|----------------|--------------------|------------------------------------|------------------------------|---------------|
|           |                   | 4                           | 4.2 J          | 1.7 U              | 0.64 U                             | 1 U                          | 0.46 U        |
|           |                   | 9                           | 6.2 J          | 1.7 U              | 0.65 U                             | 1 U                          | 0.47 U        |
|           |                   | 13.5                        | 12             | 1.8 U              | 0.66 U                             | 1 U                          | 0.48 U        |
|           |                   | 19.5                        | 36             | 1.4 U              | 0.52 U                             | 0.81 U                       | 0.37 U        |
|           |                   | 22                          | 20             | 1.5 U              | 0.55 U                             | 0.86 U                       | 0.4 U         |
|           |                   | 28                          | 12             | 1.6 U              | 0.6 U                              | 0.94 U                       | 0.43 U        |
| 211-B-020 | 10/19/2012        | 30.1                        | 0.34 U         | 1.4 U              | 0.52 U                             | 0.81 U                       | 0.37 U        |
| 211-Б-020 |                   | 39.5                        | 9.2 J          | 1.6 U              | 0.6 U                              | 0.94 U                       | 0.43 U        |
|           |                   | 40.1                        | 12             | 1.6 U              | 0.6 U                              | 0.94 U                       | 0.43 U        |
|           |                   | 48.5                        | 12             | 1.6 U              | 0.61 U                             | 0.95 U                       | 0.44 U        |
|           |                   | 50.5                        | 7.3 J          | 1.5 U              | 0.58 U                             | 0.9 U                        | 0.41 U        |
|           |                   | 59.5                        | 1.6 J          | 1.5 U              | 0.55 U                             | 0.87 U                       | 0.4 U         |
|           |                   | 61                          | 4.6 J          | 1.8 U              | 0.67 U                             | 1.1 U                        | 0.48 U        |
|           |                   | Average                     | 11             | ***                | ***                                | ***                          | ***           |

Summary of Soils VOC Data for SWMU 211-B (Continued)

Notes:

Groundwater Protection Remediation Goals from Remedial Design Work Plan for Solid Waste Management Units 1, 211-A, and 211-B 1. Volatile Organic Compound Sources for the Southwest Groundwater Plume at the Paducah Gaseous Diffusion Plant, Paducah, Kentucky, (DOE 2012a).

J - Indicates an estimated value. 2.

3. U - Compound analyzed for but not detected at or below the lowest concentration reported.

- 4. DUP - Indicated that a duplicate sample was taken for the interval given in parentheses.
- 5. Sample depth represents the discrete depth at which an EnCore® sample was taken.

For "U" qualified samples a value of one half the concentration reported was used in calculating the average borehole concentration. 6.

\*\*\* - Indicates average concentration not calculated as all boring samples were "U" qualified for specific VOC. Yellow shading and bold text indicate an exceedance of Groundwater Protection Remediation Goals. 7.

8.

9. Soil boring 211-B-014 was collected and archived. Boring was not logged or screened for VOC impacts.

#### **APPENDIX H**

ADDENDUM TO THE FINAL CHARACTERIZATION REPORT FOR SOLID WASTE MANAGEMENT UNITS 211-A AND 211-B VOLATILE ORGANIC COMPOUND SOURCES FOR THE SOUTHWEST GROUNDWATER PLUME AT THE PADUCAH GASEOUS DIFFUSION PLANT THIS PAGE INTENTIONALLY LEFT BLANK

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## ACRONYMS

| CME           | Central Mine Equipment  |
|---------------|---|
| CSM           | conceptual site model   |
| DNAPL         | dense nonaqueous-phase liquid                                       |
| DOE           | U.S. Department of Energy   |
| EPA           | U.S. Environmental Protection Agency                                |
| FCR           | final characterization report                                       |
| FFA           | Federal Facility Agreement  |
| HSA           | hollow-stem auger   |
| KDWM          | Kentucky Division of Waste Management                               |
| LATA Kentucky | LATA Environmental Services of Kentucky, LLC                        |
| LUC           | land use control  |
| PEGASIS       | PPPO Environmental Geographic Analytical Spatial Information System |
| RDSI          | remedial design support investigation                               |
| RDWP          | remedial design work plan   |
| RGA           | Regional Gravel Aquifer   |
| ROD           | record of decision  |
| SWMU          | solid waste management unit   |
| UCRS          | Upper Continental Recharge System                                   |
| VOC           | volatile organic compound   |
|               |   |

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#### H.1. PROJECT DESCRIPTION

Solid Waste Management Units (SWMUs) 211-A and 211-B are areas of trichloroethene (TCE) contamination in soil to a depth of 65 ft on the north and south sides of the C-720 Maintenance and Stores Building. Identified remedies for SWMUs 211-A and 211-B in the Record of Decision (ROD) (DOE 2012) are *in situ* source treatment using enhanced *in situ* bioremediation with interim land use controls (LUCs) and long-term monitoring (Alternative 8) or long-term monitoring with interim LUCs (Alternative 2). The U.S. Department of Energy (DOE) issued a letter notification, Final Characterization Notification for Solid Waste Management Unit 211-A and Solid Waste Management Unit 211-B at the Paducah Gaseous Diffusion Plant, Paducah Kentucky, PPPO-02-1979222-13B, on July 10, 2013 (Blumenfeld 2013). This Final Characterization Notification identified DOE's recommendation for the remedy selection of SWMUs 211-A and 211-B as long-term monitoring with interim LUCs (Alternative 2). The recommendation was based on the results of a Remedial Design Support Investigation (RDSI) of SWMUs 211-A and 211-B that were summarized in Final Characterization Report for Solid Waste Management Units 211-A and 211-B Volatile Organic Compound Sources for the Southwest Plume the Paducah Gaseous Diffusion Groundwater at Plant, Paducah, Kentucky, DOE/LX/07-1288&D2 (FCR) (DOE 2013a).

The U.S. Environmental Protection Agency (EPA) requested additional groundwater data for the Regional Gravel Aquifer (RGA) to support the basis for the final selected remedy (Tufts 2013).<sup>1</sup> EPA issued an additional work request (Tufts 2014), as provided in the Paducah Gaseous Diffusion Plant Federal Facility Agreement (FFA), to collect the additional groundwater data as a follow-on phase of the SWMUs 211-A and 211-B RDSI. Negotiations among DOE, Kentucky Division of Waste Management (KDWM), and EPA followed to determine the type and location of groundwater sampling required to address the remaining concern. The resulting sampling and analysis plan is documented in the Appendix C Addendum of the Remedial Design Work Plan (RDWP) for SWMUs 211-A and 211-B (DOE 2015). LATA Environmental Services of Kentucky, LLC, (LATA Kentucky) and its subcontractors performed sampling for this phase of the SWMUs 211-A and 211-B RDSI during the period June 22, 2015, through July 1, 2015.

The following decision rules and guidelines for evaluating the results of the RGA groundwater investigation are documented in the Appendix C sampling and analysis plan of the Addendum to the RDWP (DOE 2015).

For SWMU 211-A, in the upper or middle RGA (in the zone of higher TCE):

- **IF** the average of downgradient minus upgradient TCE levels is less than approximately 400 ppb, **THEN** the conceptual site model (CSM) and the predicted TCE mass in the Upper Continental Recharge System (UCRS) are confirmed. The remedial action will be implementation of long-term monitoring with interim LUCs.
- **IF** the average of downgradient minus upgradient TCE levels is greater than approximately 400 ppb and less than 11,000 ppb, **THEN** the CSM is valid, but the TCE mass in the UCRS is greater than estimated. The remedial action will be implementation of enhanced bioremediation with interim LUCs and long-term monitoring.

<sup>&</sup>lt;sup>1</sup> The KDWM accepted DOE's recommendation in the Final Characterization Notification (letter from April Webb to Rachel Blumenfeld, dated December 17, 2013).

For SWMU 211-A, if investigation results indicate substantial contamination throughout the RGA in the downgradient location only, dispersed dense nonaqueous-phase liquid (DNAPL) ganglia are present throughout the RGA. The CSM is invalid. The FFA parties will confer to evaluate the impact of the discovered DNAPL.

For SWMU 211-B, in the upper or middle RGA (in the zone of higher TCE), where upgradient TCE levels are assumed to be negligible:

- **IF** the average of TCE levels beneath SWMU 211-B is less than approximately 400 ppb, **THEN** the CSM and the predicted TCE mass in the UCRS is confirmed. The remedial action will be implementation of long-term monitoring with interim LUCs.
- **IF** the average of TCE levels beneath SWMU 211-B is greater than approximately 400 ppb and less than 11,000 ppb, **THEN** the CSM is valid, but the TCE mass in the UCRS is greater than estimated. The remedial action will be implementation of enhanced bioremediation with interim LUCs and long-term monitoring.

For SWMU 211-B, if investigation results indicate substantial contamination in the upper or middle RGA, DNAPL may be present in either the UCRS or the RGA. The CSM is invalid, and the FFA parties will confer to evaluate the impact of the potential DNAPL.

Moreover, for SWMU 211-B, if investigation results indicate substantial contamination in the lower RGA only, an upgradient source is impacting TCE levels beneath the SWMU. The CSM may be invalid. The FFA parties will confer to evaluate the impact of the upgradient source.

DOE will evaluate the data and prepare a revised letter notification identifying DOE's recommendation for final remedy selection for SWMUs 211-A and 211-B.

## H.2. CONCEPTUAL SITE MODELS

DOE completed RDSI activities to characterize the concentration and extent of TCE [and related volatile organic compounds (VOCs)] in soils of the UCRS and upper RGA to a depth of approximately 65 ft over the period August 2012 through March 2013. The FCR (DOE 2013a) results are the basis of the revised CSM applicable to development of this investigation's decision rules. In the investigation results and the CSM, SWMU 211-A consists of a broad area with soil remediation goal exceedances (depth-average TCE concentration in soil greater than 75  $\mu$ g/kg) in the UCRS, covering approximately 34,000 ft<sup>2</sup> laterally with a depth interval of 6 to 65.1 ft below ground surface (bgs). The combined volume (mass) estimate of TCE in SWMU 211-A ranges from 0.2 gal (1 kg) to 2.2 gal (12 kg). Additional dissolved TCE concentrations derived from SWMU 211-A are not expected to exceed 400 ppb in the RGA on the downgradient side of SWMU 211-A.

The CSM for SWMU 211-B consists of a single area in the UCRS with soil remediation goal exceedances covering approximately 3,000 ft<sup>2</sup> laterally with a depth interval of 8.5 ft bgs to 64.5 ft bgs. The TCE volume (mass) estimate for SWMU 211-B ranges from 0.1 gal (0.6 kg) to 0.8 gal (4 kg). The dissolved TCE concentrations derived from SWMU 211-B are not expected to exceed 400 ppb in the upper and middle RGA below SWMU 211-B.

General groundwater flow is northward in the areas of SWMUs 211-A and 211-B. The upgradient side is anticipated to be the south side of SWMUs 211-A and 211-B: the downgradient side is anticipated to be the north side of SWMUs 211-A and 211-B.

## H.3. GROUNDWATER SAMPLING STRATEGY

For the 2015 RDSI groundwater investigation, the general strategy for SWMU 211-A was to characterize dissolved TCE concentrations throughout the thickness of the RGA in upgradient and downgradient locations to assess the downgradient impact of the SWMU. At SWMU 211-B, where upgradient dissolved TCE levels were assumed to be negligible and the near-downgradient area was inaccessible because of the presence to the C-720 Building, the general strategy was to characterize dissolved TCE concentrations throughout the thickness of the RGA immediately below the SWMU. The Addendum to the RDWP (DOE 2015) identified five locations to sample around SWMU 211-A, based on perceived upgradient and downgradient relationships, and one location to sample within SWMU 211-B.

Previous UCRS soil sampling and analysis as part of the SWMUs 211-A and 211-B RDSI of 2012 and 2013 characterized TCE levels from near surface to a depth of approximately 65 ft bgs. The 2015 RDSI sampled and analyzed dissolved TCE levels in RGA groundwater beginning at a depth of 65 ft bgs and continuing in 5-ft intervals to the base of the RGA, found at depths between 90 ft bgs and 100 ft bgs.

The sampling and analysis plan identified the use of direct push technology (DPT) to collect the groundwater samples, unless proven ineffective. A small-diameter, hollow-stem auger (HSA) system was the back-up sampling approach. Groundwater samples were analyzed for TCE and the related VOCs 1,1-dichloroethene (DCE) (1,1-DCE); *cis*-1,2-DCE; *trans*-1,2-DCE; and vinyl chloride.

## H.4. INVESTIGATION

The investigation fieldwork was completed primarily during the two weeks beginning June 22, 2015, and June 29, 2015, which was a scheduled break in the then current phase of field investigation of SWMU 4. Sampling efforts for the SWMU 4 investigation previously had documented that DPT was ineffective for sampling groundwater through the RGA. (The DPT rig, using a dual-tube sampling system, was able to penetrate to the base of the RGA, but the penetration resistance of the RGA gravels caused the dual-tube sampling system to fail.) Therefore, the SWMUs 211-A and 211-B investigation (as well as the SWMU 4 investigation) used HSAs to access the planned sample depths.

In most locations, a smaller, Central Mine Equipment (CME)-55 drill rig, using 4 <sup>1</sup>/<sub>4</sub>-inch inside diameter (8 <sup>1</sup>/<sub>4</sub>-inch outside diameter) augers pre-drilled locations to 65 ft depth and later abandoned the boreholes once sampling was completed. A larger, CME-75 drill rig, using the same augers, drilled through the RGA and placed the sampling pump. A pilot assembly with center head attached to a string of AWJ drill rod (1.75-inch outside diameter/0.625-inch inside diameter) within the augers kept soils out of the internal bore of the augers.

The project drilling subcontractor employed special steps and equipment to minimize disturbance of the RGA matrix that was exposed in the bottom of the augers. Upon reaching the depth of the sample interval, the driller immediately ceased operation of the augers (did not raise the auger string, as is customary, to create an open interval of borehole and did not over rotate the augers to clear the outer auger flights). The pilot assembly with center head that was used for the investigation was vented into the

string of AWJ rod to minimize suction on the RGA matrix<sup>2</sup> as the pilot assembly with center head was withdrawn. The driller intentionally extracted the pilot assembly with center head slowly (with hand rotation) to minimize further suction on the RGA matrix at the base of the augers.

The sampling system consisted of a bladder pump (Well Wizard T1100) with a packer (QSP Packers, LLC, PQ wireline packer) mounted above to isolate water that was accessible to the pump from water in the augers located above the packer. The packer minimized the volume of water to be purged prior to sampling. Compressed nitrogen provided the "air" supply for operation of both the pump and packer.

The investigation schedule necessitated a one-hour limit to the groundwater purge and sampling effort for most sampling intervals. At depths of 75 ft bgs and below in the RGA, samplers were able to purge one-to-two times the volume of groundwater in the augers below the packer before sampling. The purge efforts were less effective for the upper two sample intervals (65 ft bgs and 70 ft bgs) because the height of the water column above the pump was insufficient for effective pump operation. (Greater purge volumes are less important for the uppermost sample depths where less water column is available for mixing.) With one exception (the first sample borehole, 211-A-046), sampling ceased at the base of the RGA. The underlying McNairy Formation was recognized primarily by the presence of significantly lower water levels inside the auger string prior to purging and by the inability of the formation to sustain a minimal pumping rate.

The investigation crew collected most samples directly from the discharge stream of the pump. In a few cases where the entrained sediment load was greatest, the discharged groundwater was first collected in a precleaned, stainless steel cup and then poured into the sample vials. Prior to sample collection, field parameters were measured in a cup sample with a Hydrolab water quality meter. The entrained sediment load was too great to permit use of a flow cell for field parameter measurements. For the investigation, the field parameters consisted of conductivity, dissolved oxygen, temperature, pH, oxidation/reduction potential, and turbidity. The sample vial labels and chains-of-custody were completed and maintained "real time." The samples were stored in sample coolers with wet ice during the day and transferred to sample refrigerators for storage. Trip blanks were collected at the beginning of each day of the field investigation and maintained in the sample coolers and sample refrigerators, along with the groundwater samples. Samples were shipped to the laboratory on the next day, except for the following:

- Samples of 211-A-048, 70 ft to 90 ft (sampled on Friday and shipped on Monday);
- Samples of 211-A-048, 95 ft, and 211-B-021, 65 ft (sampled on Saturday and shipped on Monday); and
- Samples of 211-A-049, 70 to 90 ft (sampled and shipped on the same-day, Wednesday).

Following the sample collection effort at each sample interval, the pump and inside of the associated sample discharge tubing (Teflon) was decontaminated in a three-step process (soap water wash, followed by tap water and deionized water rinses), consistent with LATA Kentucky procedure *Decontamination of Sampling Equipment and Devices*, PAD-ENM-2702, R0. The packer and outside of the air supply and discharge tubing were rinsed with tap water and wiped down as the sampling assembly was extracted after each sampling effort. (All but the bottom of the packer and the interior of the tubing were isolated from the sample interval during the sample process.)

 $<sup>^{2}</sup>$  The importance of minimizing suction at the base of the augers is to limit the tendency of saturated sands of the RGA from flowing into the then-open augers, which would increase turbidity of the water and potentially prevent reseating of the pilot assembly in the HSAs.

#### H.5. DATA EVALUATION

Data verification, validation, and assessment were performed for the project data in accordance with CP3-ES-5003, "Quality Assured Data" (Fluor Federal Services 2015). The data evaluation results are stored in Paducah Project Environmental Measurements System and have been transferred with the data to the Paducah Oak Ridge Environmental Information System database. Results are available through the Paducah version of DOE's PPPO Environmental Geographic Analytical Spatial Information System (PEGASIS) Web site at <a href="http://padgis.latakentucky.com/padgis/">http://padgis.latakentucky.com/padgis/</a>.

The data evaluation for the 2015 groundwater investigation of the RDSI identified the following variances. At SWMU 211-A, a total of 40 groundwater samples (excluding quality control samples) was allotted (five soil borings with eight samples each, at depths of 65 to 100 ft). The investigation sampled each of the planned borings to the base of the RGA (the project objective). Due to the field-determined depth of the base of the RGA, the deepest groundwater sample was collected from 2 of the borings at a depth of approximately 100 ft, in 2 of the borings at a depth of approximately 95 ft, and in 1 of the borings from an approximate depth of 90 ft. A total of 36 groundwater samples was collected. At SWMU 211-B, 6 groundwater samples were collected from the lone soil boring, to 90 ft depth due to the field-determined depth of the base of the RGA.

All of the investigation groundwater analyses met the laboratory reporting limits required by the RDWP (DOE 2015). Data verification assured that the data was flagged correctly. Chains-of-custody were reviewed and found to be compliant. The data assessment determined that the data were of known quality and useable.

Results for 25 analyses were qualified "J" (indicating estimated values), of which two were for duplicate samples. Of the 25 "J" results, 23 were analyses below the required laboratory reporting limit. Two of the "J" results were associated with 1,1-DCE analyses that exceed the laboratory reporting limit: Sample 211-A-048 at 70 ft depth (21  $\mu$ g/L) and Sample 211-A-048 at 95 ft depth (22  $\mu$ g/L) where the matrix spike recovery was below the lower control limit.

Level IV data validation for the 2015 groundwater investigation of the RDSI was performed at a rate of 27% (12 of 45 samples<sup>3</sup>), which exceeded the requirements of the RDSI characterization plan (10% data validation). No data were rejected during data validation. The data validation qualified only 2 of 60 results where the matrix spike recovery was below the lower control limit, as summarized above. The analyses of the validated samples were compliant with quality control requirements set forth by the analytical methods.

Except for analyses that were qualified "U" (meaning "compound analyzed for but not detected at or below the lowest concentration reported"), the laboratory and validation process applied no other result qualifiers to the investigation data.

## H.6. DATA ASSESSMENT AND VERIFICATION

Data assessment and verification were performed on 100% of the data. Data verification includes checking methods, units, reporting limits, holding times, and analytical completeness. No exceptions were

<sup>&</sup>lt;sup>3</sup> The 12 samples included 1 duplicate sample, 1 field blank sample, 1 rinseate sample, and 2 trip blank samples.

identified for the project data during data verification. Data assessment considered results of data verification, laboratory data qualifiers, laboratory comments, and sampler's comments. All data were found to be of known quality, and it was determined that decisions could be made from the data based on the review.

The 2015 groundwater investigation of the RDSI achieved a high degree of completeness. All six of the planned soil borings were sampled for RGA groundwater beginning at 65 ft depth, as planned. Samples were collected in each 5-ft interval to the base of the RGA in all of the soil borings.

## H.7. UNCERTAINTY EVALUATION

Factors that may affect uncertainty in site characterization data sets include the following:

- Results and frequencies of quality control samples, quality control exceedances, and qualifiers;
- Biases and trends in the data; and
- Project completeness.

The field investigation collected two field blank samples, three equipment rinseate samples, and eight trip blank samples for analysis of quality control. All quality control samples were analyzed for TCE; 1,1-DCE; *cis*-1,2-DCE; *trans*-1,2-DCE; and vinyl chloride. All quality control analysis results were < 1 ppb, the lab reporting limit, indicating good quality control of the decontamination process and sample shipping and minimal, if any, bias from airborne VOC levels.

The investigation also collected three duplicate samples for analysis. In each case, the difference of the original sample and duplicate sample results were  $\leq \pm/-10\%$  of the value of the original sample analysis, indicating good repeatability of the sampling process and laboratory analysis.

As documented above, there were very few quality control exceedances and the occurrence of data qualifiers were limited primarily to estimated results below the laboratory-required reporting limit and nondetect results compliant with project requirements. These factors do not affect the utility of the data for assessing the level of the contribution of the SWMUs to RGA contaminant levels with regard to selection of the final remedy.

Sampling and analysis protocols identified in the sampling and analysis plan addendum for the 2015 groundwater investigation of the RDSI were selected to optimize the representativeness of the sample and minimize the loss of VOCs, thereby reducing the potential of uncertainty associated with underestimating the presence of VOCs. The field investigation followed the sampling and analysis plan addendum for sample technique and laboratory methods except for the following:

- The dual tube sampling system for DPT, the preferred drilling method, failed due to the significant penetration resistance of the gravels of the RGA. HSAs, identified in the sampling and analysis plan as the alternative drilling method, were used to access the sample intervals.
- The investigation schedule did not allow for the targeted purge volume (based on the flooded volume of the augers) prior to sampling, as specified in the sampling and analysis plan, due to the larger volume of the HSAs.

DPT was the preferred drilling system primarily due to the expectation that the drilling method would minimally disturb the RGA at the point of sampling. Steps were taken to minimize the disturbance of the

formation due to use of the HSAs. Upon reaching the sample depth, the augers were not over-rotated, a customary technique that clears the auger flights of soil, but mixes the formation matrix at the auger head and creates pathways to mingle groundwater from different depths. A vented pilot bit for the HSAs minimized the suction created (and soil disturbance) as the center rod assembly was withdrawn to permit sampling. Moreover, the driller intentionally withdrew the pilot bit slowly, with rotation, to further minimize suction.

Purging prior to sampling was intended to minimize the impact of the drilling system on the groundwater sample quality. Groundwater purging, prior to sampling, was implemented with the HSAs. The project schedule did not permit the targeted purge volume of three times the flooded volume of the augers, but a packer was used above the pump within the augers to minimize the effective volume to be purged. The pump/packer setting was adjusted based on field experience to minimize the entrained sediment load of the purge water<sup>4</sup> and minimize the effective flooded volume of the augers. Purge volumes achieved ranged from one to two flooded volumes of the augers.

Significantly lower water levels were measured inside the augers when the augers penetrated into the underlying McNairy Formation, as compared to the RGA. These measurements demonstrated that the seals between augers were effective at limiting inflow of water. The demonstrated integrity of the HSA system provided additional assurance that the water column inside the HSAs was representative of the sample depth and the achieved purge volume was sufficient to provide a quality sample.

## H.8. SAMPLE RESULTS AND ASSESSMENT

Six soil boring locations, documented in Table H.1 and shown in Figure H.1, were performed, with five locations around SWMU 211-A and one location within SWMU 211-B. (Relationships are assigned with the assumption that groundwater flows northerly, consistent with the broader site trends.) The investigation collected groundwater samples in each of the soil borings at 5-ft intervals, beginning at 65 ft depth and continuing to the base of the RGA (at depths of 90 to 100 ft).

Table H.2 presents the investigation analyses for TCE as well as the related VOCs 1,1-DCE; *cis*-1,2-DCE; *trans*-1,2-DCE; and vinyl chloride.

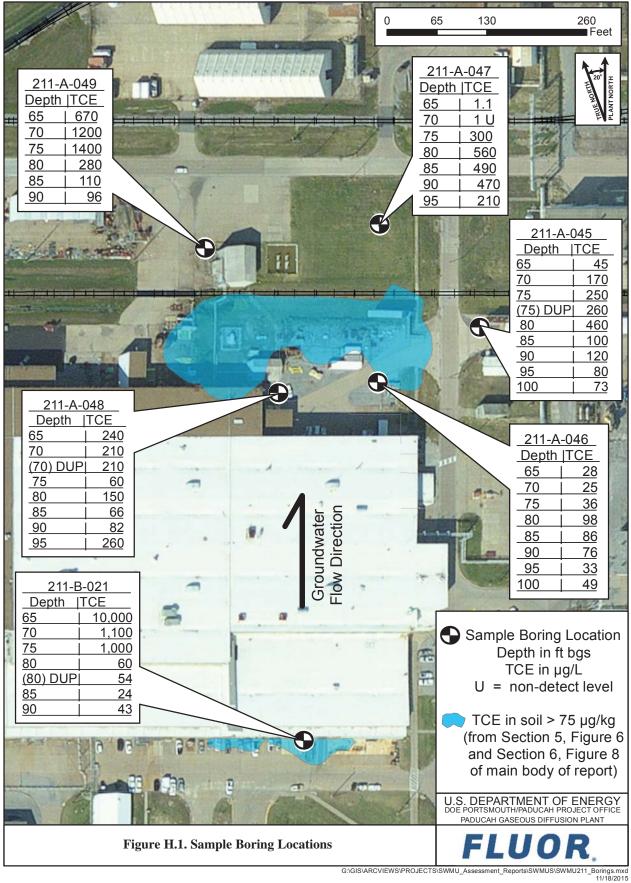
#### H.8.1 TCE ANALYSES

Table H.3 summarizes the comparisons of TCE analyses, consistent with the project decision rules. Sample depths are grouped into upper, middle, and lower RGA zones to yield the greatest downgradient difference (to minimize the chance of not recognizing a significant difference). Sample results may be included in the average of two adjacent RGA zones (upper, middle, or lower).

<sup>&</sup>lt;sup>4</sup> When the pump was set near the bottom of the auger string, entrained sediment plugged the pump screen. Setting the pump higher in the auger string provided a thicker water column for settling the sediments but increased the flooded volume to be purged.

| Somulo Boring  | Deletionshin                            | Plant Coordinates |        |  |  |
|--|---|-------------------|--------|--|--|
| Sample Boring  | Relationship                            | East              | North  |  |  |
| <ul><li>211-A-045</li><li>East side of SWMU 211-A</li></ul>        | Upgradient Location<br>of SWMU 211-A    | -4,890            | -2,060 |  |  |
| <ul><li>211-A-046</li><li>South side of SWMU 211-A</li></ul>       | Upgradient Location<br>of SWMU 211-A    | -5,030            | -2,145 |  |  |
| <ul><li>211-A-047</li><li>North side of SWMU 211-A</li></ul>       | Downgradient Location<br>of SWMU 211-A  | -5,030            | -1,955 |  |  |
| <ul><li>211-A-048</li><li>South side of SWMU 211-A</li></ul>       | Upgradient Location<br>of SWMU 211-A    | -5,180            | -2,135 |  |  |
| <ul><li>211-A-049</li><li>North side of SWMU 211-A</li></ul>       | Downgradient Location<br>of SWMU 211-A  | -5,260            | -1,955 |  |  |
| <ul><li>211-B-021</li><li>Internal Boring for SWMU 211-B</li></ul> | Beneath/"Downgradient"<br>of SWMU 211-B | -5,138            | -2,600 |  |  |

#### Table H.1. SWMUs 211-A and 211-B Sample Borings



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|                        | Depth Sampled        | Date      | Trichloroe | thene (ug/L) | 1 1-Dichloro | ethene (ug/L) | cis-1 2-Dichlo | roethene (ug/L) | cis-1,2-Dichloroethene/   | trans_1 2-Dich | loroethene (ug/L) | Vinyl Chl | oride (ug/L) |
|------------------------|----------------------|-----------|------------|--------------|--------------|---------------|----------------|-----------------|---------------------------|----------------|-------------------|-----------|--------------|
| Station                | (ft)                 | Collected | Result     | Oualifier    | Result       | Qualifier     | Result         | Qualifier       | Trichloroethene Ratio (%) | Result         | Qualifier         | Result    | Qualifier    |
| 211-A-045              | 65                   | 6/29/2015 | 45         | Qualifier    | 4.2          | Qualifier     | 2.5            | Quanner         | 6                         | 1              | U                 | 1         | U            |
| 211-A-045              | 70                   | 6/29/2015 | 170        |              | 22           |               | 7.8            |                 | 5                         | 1              | U                 | 1         | U            |
| 211-A-045              | 76<br>75             | 6/30/2015 | 250        |              | 39           |               | 13             |                 | 5                         | 0.36           | I                 | 1         | U            |
| 211-A-045              | (duplicate) 75       | 6/30/2015 | 260        |              | 40           |               | 13             |                 | 5                         | 0.38           | J                 | 1         | U            |
| 211-A-045              | (dupileate) 75<br>80 | 6/30/2015 | 460        |              | 49           |               | 19             |                 | 4                         | 0.33           | J                 | 1         | U            |
| 211-A-045              | 85                   | 6/30/2015 | 100        |              | 9.5          |               | 32             |                 | 32                        | 1              | J<br>U            | 1         | U            |
| 211 A 045<br>211-A-045 | 90                   | 6/30/2015 | 120        |              | 7.5          |               | 26             |                 | 22                        | 0.32           | I                 | 1         | U            |
| 211 A 045<br>211-A-045 | 95                   | 6/30/2015 | 80         |              | 2.4          |               | 20             |                 | 28                        | 1              | y<br>U            | 1         | U            |
| 211 A 045<br>211-A-045 | 100                  | 6/30/2015 | 73         |              | 5.7          |               | 19             |                 | 26                        | 1              | U                 | 1         | U            |
|                        |                      | 6/23/2015 | 28         |              | 2.2          |               |                |                 | 14                        | 1              | U                 | 1         | U            |
| 211-A-046              | 65<br>70             | 6/23/2015 |            |              | 3.4          |               | 4              |                 | 14                        | 1              |                   | 1         |              |
| 211-A-046              | 70                   | 6/24/2015 | 25         |              |              |               | 4.4            |                 | 28                        | 1              | U                 | 1         | U            |
| 211-A-046              | 75                   | 6/24/2015 | 36         |              | 3.3          |               | 10             |                 | 52                        | 1              | U                 | 1         | U            |
| 211-A-046              | 80                   |           | 98         |              | 11           |               | 51             |                 | 32                        | 1              | U                 | 1         | U            |
| 211-A-046              | 85                   | 6/24/2015 | 86         |              | 5.6          |               | 32             |                 | 25                        | 1              | U                 | 1         | U            |
| 211-A-046              | 90                   | 6/24/2015 | 76         |              | 2.3          |               | 19             |                 | 23                        | 1              | U                 | 1         | U            |
| 211-A-046              | 95                   | 6/24/2015 | 33         |              | 1.5          |               | 7.6            |                 | 25 29                     | 1              | U                 | 1         | U            |
| 211-A-046              | 100                  | 6/24/2015 | 49         |              | 2.6          |               | 14             |                 |                           | 1              | U                 | 1         | U            |
| 211-A-047              | 65                   | 6/24/2015 | 1.1        |              | 1            | U             | 1              | U               | 91                        | 1              | U                 | 1         | U            |
| 211-A-047              | 70                   | 6/25/2015 | 1          | U            | 1            | U             | 1              | U               | 100                       | 1              | U                 | 1         | U            |
| 211-A-047              | 75                   | 6/25/2015 | 300        |              | 58           |               | 29             |                 | 10                        | 0.54           | J                 | 1         | U            |
| 211-A-047              | 80                   | 6/25/2015 | 560        |              | 72           |               | 32             |                 | 6                         | 0.89           | J                 | 1         | U            |
| 211-A-047              | 85                   | 6/25/2015 | 490        |              | 71           |               | 34             |                 | /                         | 1.2            |                   | 1         | U            |
| 211-A-047              | 90                   | 6/25/2015 | 470        |              | 62           |               | 31             |                 |                           | 1.1            |                   | 1         | U            |
| 211-A-047              | 95                   | 6/25/2015 | 210        |              | 26           | -             | 49             | -               | 23                        | 1.3            |                   | 1         | U            |
| 211-A-048              | 65                   | 6/25/2015 | 240        |              | 29           |               | 740            |                 | 308                       | 0.8            | J                 | 79        |              |
| 211-A-048              | 70                   | 6/26/2015 | 210        |              | 21           | J             | 610            |                 | 290                       | 0.78           | J                 | 57        |              |
| 211-A-048              | (duplicate) 70       | 6/26/2015 | 210        |              | 20           |               | 640            |                 | 305                       | 0.69           | J                 | 60        |              |
| 211-A-048              | 75                   | 6/26/2015 | 60         |              | 15           |               | 49             |                 | 82                        | 0.34           | J                 | 3.5       |              |
| 211-A-048              | 80                   | 6/26/2015 | 150        |              | 56           |               | 81             |                 | 54                        | 0.62           | J                 | 1.6       |              |
| 211-A-048              | 85                   | 6/26/2015 | 66         |              | 21           |               | 45             |                 | 68                        | 0.36           | J                 | 1.4       |              |
| 211-A-048              | 90                   | 6/26/2015 | 82         |              | 15           |               | 45             |                 | 55                        | 0.45           | J                 | 0.65      | J            |
| 211-A-048              | 95                   | 6/27/2015 | 260        |              | 22           | J             | 49             |                 | 19                        | 0.41           | J                 | 0.96      | J            |
| 211-A-049              | 65                   | 6/30/2015 | 670        |              | 1,400        |               | 56             |                 | 8                         | 1              | U                 | 1.9       |              |
| 211-A-049              | 70                   | 7/1/2015  | 1,200      |              | 2,100        |               | 79             |                 | 7                         | 0.47           | J                 | 3         |              |
| 211-A-049              | 75                   | 7/1/2015  | 1,400      |              | 2,200        |               | 77             |                 | 6                         | 0.54           | J                 | 3.2       |              |
| 211-A-049              | 80                   | 7/1/2015  | 280        |              | 360          |               | 44             |                 | 16                        | 0.49           | J                 | 0.76      | J            |
| 211-A-049              | 85                   | 7/1/2015  | 110        |              | 59           |               | 42             |                 | 38                        | 0.39           | J                 | 1         | U            |
| 211-A-049              | 90                   | 7/1/2015  | 96         | <u>.</u>     | 50           |               | 36             |                 | 38                        | 1              | U                 | 1         | U            |
| 211-B-021              | 65                   | 6/27/2015 | 10,000     |              | 1.1          |               | 210            |                 | 2                         | 0.6            | J                 | 1         | U            |
| 211-B-021              | 70                   | 6/29/2015 | 1,100      |              | 0.31         | J             | 26             |                 | 2                         | 1              | U                 | 1         | U            |
| 211-B-021              | 75                   | 6/29/2015 | 1,000      |              | 1            | U             | 28             |                 | 3                         | 1              | U                 | 1         | U            |
| 211-B-021              | 80                   | 6/29/2015 | 60         |              | 1            | U             | 2.4            |                 | 4                         | 1              | U                 | 1         | U            |
| 211-B-021              | (duplicate) 80       | 6/29/2015 | 54         |              | 1            | U             | 2.2            |                 | 4                         | 1              | U                 | 1         | U            |
| 211-B-021              | 85                   | 6/29/2015 | 24         |              | 1            | U             | 1.6            |                 | 7                         | 1              | U                 | 1         | U            |
| 211-B-021              | 90                   | 6/29/2015 | 43         |              | 1            | U             | 1.5            |                 | 3                         | 1              | U                 | 1         | U            |

 Table H.2. Volatile Organic Compound Analyses for the 2015 Groundwater Investigation of the Remedial Design Support Investigation (Continued)

| Date      |                        | Quality Control | Trichloroe | richloroethene (ug/L) 1,1-Dichloroethene (ug/L |        | oethene (ug/L) | cis-1,2-Dichloroethene (ug/L) |           | <i>trans</i> -1,2-Dichloroethene (ug/L) |           | Vinyl Chloride (ug/L) |           |
|-----------|------------------------|-----------------|------------|--|--------|----------------|-------------------------------|-----------|---|-----------|-----------------------|-----------|
| Collected | Station(s)             | Sample Type     | Result     | Qualifier                                      | Result | Qualifier      | Result                        | Qualifier | Result                                  | Qualifier | Result                | Qualifier |
| 6/23/15   | 211-A-046              | Rinseate        | 1          | U  | 1      | U              | 1                             | U         | 1                                       | U         | 1                     | U         |
| 0/23/13   | 211-A-040              | Trip Blank      | 1          | U  | 1      | U              | 1                             | U         | 1                                       | U         | 1                     | U         |
| 6/24/15   | 211-A-046<br>211-A-047 | Trip Blank      | 1          | U  | 1      | U              | 1                             | U         | 1                                       | U         | 1                     | U         |
| 6/25/15   | 211-A-047<br>211-A-048 | Trip Blank      | 1          | U  | 1      | U              | 1                             | U         | 1                                       | U         | 1                     | U         |
|           |                        | Field Blank     | 1          | U  | 1      | U              | 1                             | U         | 1                                       | U         | 1                     | U         |
| 6/26/2015 | 211-A-048              | Rinseate        | 1          | U  | 1      | U              | 1                             | U         | 1                                       | U         | 1                     | U         |
|           |                        | Trip Blank      | 1          | U  | 1      | U              | 1                             | U         | 1                                       | U         | 1                     | U         |
| 6/27/2015 | 211-A-048<br>211-B-021 | Trip Blank      | 1          | U  | 1      | U              | 1                             | U         | 1                                       | U         | 1                     | U         |
| 6/29/2015 | 211-A-045<br>211-B-021 | Trip Blank      | 1          | U  | 1      | U              | 1                             | U         | 1                                       | U         | 1                     | U         |
|           | 011 0 0 15             | Field Blank     | 1          | U  | 1      | U              | 1                             | U         | 1                                       | U         | 1                     | U         |
| 6/30/15   | 211-A-045<br>211-A-049 | Rinseate        | 1          | U  | 1      | U              | 1                             | U         | 1                                       | U         | 1                     | U         |
|           | 211-7-047              | Trip Blank      | 1          | U  | 1      | U              | 1                             | U         | 1                                       | U         | 1                     | U         |
| 7/1/15    | 211-A-049              | Trip Blank      | 1          | U  | 1      | U              | 1                             | U         | 1                                       | U         | 1                     | U         |

|                             | D  | T  |                                    | Decisio   | n Rules  |
|-----------------------------|--|--|------------------------------------|---|--|
| RGA Zone<br>(depth in feet) | Downgradient<br>TCE<br>Average <sup>a</sup><br>(ppb) | Upgradient<br>TCE<br>Average <sup>a</sup><br>(ppb) | Difference of<br>Averages<br>(ppb) | Difference of<br>Averages <<br>Approximately<br>400 ppb | 11,000 ppb ><br>Difference of<br>Averages<br>> 400 ppb |
| East SWMU 211-A             | 211-A-047  | 211-A-045  |                                    |   |  |
| Upper (65–75)               | 101  | 155  | -54                                | Х   |  |
| Middle (75–90)              | 455  | 233  | 223                                | Х   |  |
| Lower (90–95)               | 340  | 100  | 240                                | Х   |  |
|                             | 211-A-047  | 211-A-046  |                                    |   |  |
| Upper (65–75)               | 101  | 30   | 71                                 | Х   |  |
| Middle (75–90)              | 455  | 74   | 381                                | Х   |  |
| Lower (90–95)               | 340  | 55   | 286                                | Х   |  |
| West SWMU 211-A             | 211-A-049  | 211-A-048  |                                    |   |  |
| Upper (65–70)               | 935  | 225  | 710                                |   | Х  |
| Middle (75–80)              | 840  | 105  | 735                                |   | Х  |
| Lower (85–90)               | 103  | 74   | 29                                 | Х   |  |
| SWMU 211-B                  | 211-B-021  |  |                                    |   |  |
| Upper (65)                  | 10,000   | NA <sup>b</sup>                                    |                                    |   | ~ X <sup>c</sup>                                       |
| Middle (70-75)              | 1,050  | NA   |                                    |   | Х  |
| Lower (80-90)               | 42   | NA   |                                    | Х   |  |

Table H.3. Assessment of SWMU 211-A and 211-B Sample Results

<sup>a</sup> Duplicate results were not used in calculating average concentrations.

<sup>b</sup> An upgradient sample boring was not sampled for SWMU 211-B.

<sup>c</sup> The sum of the analysis result and error range is 11,100 ppb.

In the east SWMU 211-A area, the difference of average upgradient and downgradient TCE levels is less than the lower criterion of approximately 400 ppb used in the decision rules. In the west SWMU 211-A area, the difference falls between the approximately 400 ppb and 11,000 ppb criteria for remedial decisions at SWMUs 211-A and 211-B. The different results of the east and west areas of SWMU 211-A provide a basis for focusing remedial action components of the selected remedy for SWMU 211-A.

At SWMU 211-B, the analyses for three upper RGA samples from depths of 65 ft, 70 ft, and 75 ft depth substantially exceed the 400 ppb action level. Moreover, the analysis for the sample at 65 ft depth—10,000 ppb with a control limit range (error range) of 1,100 ppb—approximates the project criterion for recognizing the presence of DNAPL (11,000 ppb).

The objective of the 2015 groundwater investigation of the RDSI was to assess the contribution of the SWMUs to levels of TCE and related VOCs in RGA groundwater. The field investigation used a biased sampling approach, characterizing groundwater quality in upgradient and downgradient areas at SWMU 211-A and sampling directly beneath SWMU 211-B, where upgradient levels of TCE and related VOCs are anticipated to be low and where sampling is inaccessible in the near-downgradient area due to the proximity of the C-720 Building. Separate decision rules exist for SWMUs 211-A and 211-B, but the data set was intended to be evaluated holistically. The data support a straightforward analysis of SWMU 211-A. The CSM for SWMU 211-A is validated. TCE analyses for SWMU 211-B unequivocally indicate a significant impact at the SWMU: DNAPL may be present in either the UCRS or the RGA, and the CSM may be invalid.

#### H.8.2 OTHER VOLATILE ORGANIC COMPOUND ANALYSES

The decision rules do not address the analyses for 1,1-DCE; *cis*-1,2-DCE; *trans*-1,2-DCE; and vinyl chloride. However, an assessment of this data provides useful context for understanding the groundwater flow system at the C-720 Building and the area of SWMUs 211-A and 211-B.

The relationships of TCE and *cis*-1,2-DCE in sample borings 211-A-046 and 211-A-047 are consistent with expectations for background and upgradient/downgradient associations. (Levels of *trans*-1,2-DCE and vinyl chloride are less than 2 ppb).

- Upgradient sample boring 211-A-046 has a uniformly low level of TCE (<100 ppb) with *cis*-1,2-DCE/TCE ratios > 10%, indicative of a longer contaminant residence time in the RGA.
- The upper portion of downgradient boring 211-A-047 (samples for 65 ft and 70 ft depths) is uniquely devoid of VOCs (1.1 ppb or less combined VOCs), suggestive of vertical flow to 70 ft depth with no contribution of contamination from the UCRS.
- Between 75 ft and 90 ft in sample boring 211-A-047, TCE levels spike to 300 ppb or greater with *cis*-1,2-DCE/TCE ratios ≤ 10%, indicative of a close upgradient source and lesser contaminant residence time.

A similar "downgradient to contamination" pattern is apparent in 211-A-045, with lowest TCE values in the 65 ft sample but highest TCE values in the 70 ft to 80 ft samples (170 to 460 ppb) and with *cis*-1,2-DCE/TCE ratios of 6% or less (65 to 80 ft). If the source of the shallow contamination in 211-A-045 is SWMU 211-A, then local groundwater flow has a strong easterly component.

Groundwater at 211-A-048, the upgradient sample boring for the west side of SWMU 211-A, has an upgradient contaminant source.

- Soils analyses from the SWMUs 211-A and 211-B RDSI of 2012 and 2013 document very low levels of VOC contamination in the area UCRS soils.
- Groundwater analyses from the 2015 phase of the RDSI have highest TCE levels (210 ppb to 240 ppb<sup>5</sup>) and *cis*-1,2-DCE levels (610 ppb to 740 ppb) in the samples from 65 ft and 70 ft depths. Ratios of *cis*-1,2-DCE/TCE range from 290% to 308% in the samples from 65 ft and 70 ft depths.

This ratio suggests the occurrence of active anaerobic degradation of TCE, as does relatively high levels of vinyl chloride (57–79 ppb) from 65 and 70 ft depths.<sup>6</sup> Anaerobic conditions may be supported by locally reduced UCRS recharge due to the area's paved surface and the sample boring's location immediately to the north (downgradient) of the C-720 Building.

Both TCE and 1,1-DCE trends in sample boring 211-A-049 are suggestive of a "downgradient to contamination" relationship.

<sup>&</sup>lt;sup>5</sup> Excluding the bottom RGA sample (95 ft) TCE result of 260 ppb.

<sup>&</sup>lt;sup>6</sup> Field measurements for the groundwater samples from 211-A-048 document high dissolved oxygen levels (1.97 to 11.72 ppm), which are incompatible with anaerobic conditions. High entrained sediment content prevented use of a flow cell for field measurements: the measurements were made in a cup sample. Dissolved oxygen levels appear to have been biased high during field measurements.

- The highest TCE and 1,1-DCE contaminant levels were found in the samples at 70 and 75 ft deep (1,200 ppb and 1,400 ppb TCE and 2,100 and 2,200 ppb 1,1-DCE).
- Lesser contaminant levels at the 65 ft depth (670 ppb TCE and 1,400 ppb 1,1-DCE) reflect the influence of UCRS recharge.
- Ratios of *cis*-1,2-DCE/TCE are 8% or less between 65 and 75 ft deep, consistent with minimal contaminant residence time in the RGA and the presence of a nearby source zone.

The lesser *cis*-1,2-DCE levels in 211-A-049 (highest level of 79 ppb) compared to 211-A-048 (highest level of 740 ppb) indicate 211-A-049 is not directly downgradient of 211-A-048. Sample borings 211-A-048 and 211-A-049 are downgradient to different sources; however, the upgradient/downgradient comparison of TCE levels of the decision rules would not differ significantly with lower upgradient TCE levels. The occurrence of elevated levels of 1,1-DCE in groundwater samples from 211-A-049 is consistent with the west side of the SWMU 211-A source zone, as defined in the RDSI of 2012 and 2013. UCRS soils of the west side contained appreciable levels of both TCE and 1,1-DCE.

Dissolved RGA contaminant trends at SWMU 211-B, notably TCE and *cis*-1,2-DCE, are consistent with a UCRS contaminant source in the area of 211-B-021. TCE and *cis*-1,2-DCE levels are highest in the 65 ft depth sample (10,000 ppb TCE and 210 ppb *cis*-1,2-DCE) and drop to approximately 10% of the concentrations in the samples at 70 ft and 75 ft, showing the influence of mixing of vertical flow from the UCRS with the lateral flow that predominates in the RGA.

#### H.9. CONCLUSIONS

The 2015 phase of the SWMUs 211-A and 211-B investigation sampled groundwater from the RGA in 5-ft intervals from a depth of 65 ft to the base of the RGA in all six proposed locations. A holistic review of the data, as summarized above, indicates that the investigation data are appropriate for assessing the impact of SWMUs 211-A and 211-B to dissolved TCE levels in the RGA.

The SWMU 211-B sample results are consistent with a UCRS source zone impacting the RGA. The shallowest groundwater result for TCE (65 ft depth) approximates the established project criterion for the recognition of the presence of DNAPL, which would be inconsistent with the CSM basis of the ROD (DOE 2012). The available remedies of the ROD did not consider the possibility of the presence of DNAPL at or near SWMU 211-B. According to the decision rules for SWMU 211-B, the FFA parties must confer to evaluate the impact of the potential for DNAPL. Future decommissioning of the C-720 Building may allow opportunity to sample adjacent soils beneath the building (and currently inaccessible) and reduce the uncertainty with regard to the extent of TCE contamination at SWMU 211-B, including the presence of DNAPL.

The sample results of SWMU 211-A are consistent with the CSM. SWMU 211-A is contributing TCE levels in excess of 400 ppb, but less than 11,000 ppb on the west side only. The SWMU 211-A decision rules direct implementation of enhanced bioremediation with interim LUCs and long-term monitoring (Alternative 8). These results support focused application of enhanced bioremediation on the west side.

Results of the 2015 phase of the investigation indicate DNAPL may be present at SWMU 211-B and the CSM may be invalid. SWMU 211-B is upgradient of SWMU 211-A. The project decision rules do not consider the implications of the invalidation of the CSM at SWMU 211-B upon the remedial actions at SWMU 211-A. 211-A-048, the upgradient sample boring for the west side of SWMU 211-A, appears to

be impacted by an upgradient contaminant source. That contaminant source may be SWMU 211-B or another source underlying the C-720 Building. Further discussions are warranted among the FFA parties with regard to the TCE source located upgradient of SWMU 211-A, the possibility that anaerobic degradation is affecting this source, and on the timing of the SWMU 211-A remedial action.

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## ATTACHMENT

# FIELD MEASUREMENTS AND BAROMETRIC PRESSURE

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#### Field Measurements and Barometric Pressure

| Station            | Date<br>Collected | Depth<br>Sampled<br>(ft) | Height of<br>Top of Auger<br>(approx. inches) | Open Hole<br>Depth<br>(ft) | Purge Volume<br>(gal/% flooded<br>volume <sup>7</sup> ) | Starting<br>Depth to Water<br>(ft) | Barometric<br>Pressure<br>(inch/Hg) |  |
|--------------------|-------------------|--------------------------|---|----------------------------|---|------------------------------------|-------------------------------------|--|
|                    | 6/00/2015         | 65                       | 12  | 65.3                       | 7.25 gal/ 60%   | 33.05                              | 20.02                               |  |
|                    | 6/29/2015         | 70                       | 14  | 70.6                       | 12.25 gal/ 80%  | 43.37                              | 29.92                               |  |
|                    |                   | 75                       | 14  | 74.5                       | 22.25 gal/150%  | 47.29                              | 29.96                               |  |
| 211 4 045          |                   | 80                       | 14  | 79.8                       | 23.75 gal/160%  | 47.02                              |                                     |  |
| 211-A-045          | C/20/2015         | 85                       | 14  | 84.1                       | 20.75 gal/140%  | 47.75                              | 29.92                               |  |
|                    | 6/30/2015         | 90                       | 20  | 89.7                       | 18.25 gal/120%  | 47.27                              |                                     |  |
|                    |                   | 95                       | 14  | 94.5                       | 15.0 gal/100%   | 47.66                              | 29.94                               |  |
|                    |                   | 100                      | 15  | 99.3                       | 20.25 gal/130%  | 47.80                              | 29.96                               |  |
|                    | 6/23/2015         | 65                       | 12  | 65.6                       | 6.0 gal/ 80%  | 46.37                              | 29.96                               |  |
|                    | 0/23/2015         | 70                       | 12  | 70.0                       | 20.0 gal/130%   | 45.13                              | 29.96                               |  |
|                    |                   | 75                       | 12  | 74.7                       | 20.0 gal/130%   | 46.75                              | 29.89                               |  |
| 211 4 046          |                   | 80                       | 12  | 79.5                       | 20.0 gal/130%   | 49.47                              | 29.86                               |  |
| 211-A-046          | 6/24/2015         | 85                       | 12  | 84.3                       | 20.0 gal/130%   | 47.39                              | 20.97                               |  |
|                    | 6/24/2015         | 90                       | 12  | 89.3                       | 25.0 gal/170%   | 47.60                              | 29.87                               |  |
|                    |                   | 95                       | 12  | 94.3                       | 22.0 gal/150%   | 47.74                              | 29.90                               |  |
|                    |                   | 100                      | 12  | 100.0                      | 2.75 gal/ 20%   | 61.35                              | 29.91                               |  |
|                    | 6/24/2015         | 65                       | 12  | 65.1                       | 2.0 gal/ 10%  | 45.50                              | 29.91                               |  |
|                    | 6/25/2015         | 70                       | 12  | 69.0                       | 10.0 gal/ 70%   | 44.69                              |                                     |  |
| 211-A-047          |                   | 75                       | 12  | 74.8                       | 20.0 gal/130%   | 46.28                              | 20.97                               |  |
|                    |                   | 80                       | 12  | 80.0                       | 22.0 gal/150%   | 48.12                              | 29.87                               |  |
|                    | 6/25/2015         | 85                       | 12  | 84.8                       | 32.0 gal/210%   | 47.87                              |                                     |  |
|                    |                   | 90                       | 12  | 90.0                       | 21.0 gal/140%   | 47.51                              | 29.90                               |  |
|                    |                   | 95                       | 12  | 94.4                       | 21.5 gal/140%   | 48.20                              | 29.96                               |  |
|                    | 6/25/2015         | 65                       | 12  | 64.8                       | 9.5 gal/ 60%  | 38.63                              | 29.91                               |  |
|                    |                   | 70                       | 10  | 70.5                       | 9.5 gal/ 60%  | 43.70                              |                                     |  |
|                    |                   | 75                       | 14  | 75.0                       | 20.5 gal/140%   | 49.31                              | 29.87                               |  |
| 211-A-048          | 6/26/2015         | 80                       | 12  | 79.0                       | 23.75 gal/160%  | 48.10                              |                                     |  |
|                    |                   | 85                       | 12  | 84.2                       | 23.0 gal/150%   | 47.68                              | 20.00                               |  |
|                    |                   | 90                       | 12  | 89.5                       | 24.0 gal/160%   | 48.12                              | 29.90                               |  |
|                    | 6/27/2015         | 95                       | 14  | 95.1                       | 21.5 gal/140%   | 49.18                              | 29.91                               |  |
|                    | 6/30/2015         | 65                       | 14  | 64.6                       | 15.5 gal/200%   | 48.78                              | 29.96                               |  |
|                    |                   | 70                       | 24  | 70.0                       | 21.5 gal/190%   | 47.15                              |                                     |  |
| <b>0</b> 11 4 0 40 |                   | 75                       | 24  | 74.8                       | 22.75 gal/200%  | 46.91                              |                                     |  |
| 211-A-049          | 7/1/2015          | 80                       | 24  | 79.0                       | 21.25 gal/190%  | 46.84                              | 30.00                               |  |
|                    |                   | 85                       | 24  | 84.3                       | 17.75 gal/160%  | 48.75                              |                                     |  |
|                    |                   | 90                       | 24  | 89.0                       | 21.0 gal/140%   | 48.46                              |                                     |  |
|                    | 6/27/2015         | 65                       | 12  | 65.5                       | 16.5 gal/210%   | 27.07                              | 29.96                               |  |
|                    |                   | 70                       | 10  | 68.6                       | 13.25 gal/120%  | 43.48                              | 20.01                               |  |
| 011 D 001          |                   | 75                       | 14  | 75.4                       | 20.5 gal/140%   | 48.97                              | 29.91                               |  |
| 211-B-021          | 6/29/2015         | 80                       | 14  | 78.0                       | 25.0 gal/170%   | 45.03                              | 29.97                               |  |
|                    |                   | 85                       | 12  | 84.5                       | 24.0 gal/160%   | 46.58                              |                                     |  |
|                    |                   | 90                       | 16  | 89.5                       | 17.0 gal/110%   | 46.91                              | 29.92                               |  |

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 $<sup>^{7}</sup>$  Flooded volume refers to the volume of the HSAs below the packer.

| Station   | Depth<br>Sampled<br>(ft) | Conductivity<br>(µmho/cm) | Dissolved<br>Oxygen<br>(mg/L) | Oxidation-<br>Reduction<br>Potential (mV) | pH<br>(Std Units) | Temp<br>(deg F) | Turbidity*<br>(NTU) |
|-----------|--------------------------|---------------------------|-------------------------------|---|-------------------|-----------------|---------------------|
|           | 65                       | 1370                      | 4.16                          | 291                                       | 7.84              | 77.0            | 5999                |
|           | 70                       | 1258                      | 6.04                          | 163                                       | 6.71              | 75.8            | 5999                |
|           | 75                       | 1023                      | 5.87                          | 529                                       | 7.52              | 67.9            | 2000                |
| 211 4 045 | 80                       | 735                       | 8.05                          | 112                                       | 7.46              | 68.9            | 2000                |
| 211-A-045 | 85                       | 527                       | 6.11                          | 204                                       | 7.38              | 71.2            | 5999                |
|           | 90                       | 434                       | 2.63                          | 156                                       | 7.94              | 72.5            | 5999                |
|           | 95                       | 454                       | 2.61                          | 173                                       | 6.56              | 73.4            | 5999                |
|           | 100                      | 425                       | 7.37                          | 89  | 7.39              | 72.2            | 5999                |
|           | 65                       | 875                       | 1.80                          | 250                                       | 6.26              | 86.1            | 5999                |
|           | 70                       | 947                       | 2.37                          | 155                                       | 6.96              | 75.4            | 5999                |
|           | 75                       | 834                       | 2.95                          | -168                                      | 6.67              | 70.5            | 5999                |
| 211 4 046 | 80                       | 555                       | 3.04                          | 175                                       | 6.22              | 72.7            | 2000                |
| 211-A-046 | 85                       | 514                       | 2.90                          | 186                                       | 6.36              | 75.4            | 2000                |
|           | 90                       | 507                       | 3.32                          | 160                                       | 6.92              | 78.6            | 1734                |
|           | 95                       | 338                       | 3.59                          | 166                                       | 6.93              | 79.6            | 5999                |
|           | 100                      | 546                       | 7.18                          | 100                                       | 7.17              | 78.7            | 2000                |
|           | 65                       | 234                       | 4.43                          | 339                                       | 6.82              | 83.7            | 5999                |
|           | 70                       | 1139                      | 3.64                          | 154                                       | 6.25              | 69.3            | 1118                |
|           | 75                       | 657                       | 3.67                          | 110                                       | 6.58              | 71.1            | 5999                |
| 211-A-047 | 80                       | 630                       | 7.84                          | 142                                       | 7.26              | 69.8            | 5999                |
|           | 85                       | 633                       | 3.41                          | 328                                       | 6.51              | 73.4            | 2000                |
|           | 90                       | 657                       | 3.75                          | 334                                       | 6.96              | 74.7            | 5999                |
|           | 95                       | 613                       | 6.85                          | 317                                       | 7.05              | 74.5            | 5999                |
|           | 65                       | 422                       | 6.49                          | 92  | 7.95              | 74.9            | 5999                |
|           | 70                       | 477                       | 1.97                          | 122                                       | 6.99              | 77.0            | 615                 |
|           | 75                       | 671                       | 11.72                         | 253                                       | 6.52              | 72.0            | 5999                |
| 211-A-048 | 80                       | 646                       | 7.35                          | 241                                       | 6.26              | 72.7            | 2456                |
|           | 85                       | 477                       | 4.60                          | 101                                       | 7.71              | 76.9            | 5999                |
|           | 90                       | 456                       | 2.22                          | 131                                       | 7.12              | 79.9            | 2000                |
|           | 95                       | 671                       | 6.34                          | 161                                       | 6.56              | 64.3            | 5999                |
|           | 65                       | 336                       | 4.52                          | 129                                       | 7.31              | 71.2            | 2000                |
|           | 70                       | 491                       | 5.50                          | 199                                       | 6.69              | 68.6            | 1312                |
| 211 4 040 | 75                       | 506                       | 3.68                          | 235                                       | 5.83              | 68.6            | 1010                |
| 211-A-049 | 80                       | 440                       | 5.97                          | 233                                       | 5.96              | 68.2            | 5999                |
|           | 85                       | 450                       | 2.53                          | 139                                       | 7.84              | 68.8            | 2000                |
|           | 90                       | 441                       | 4.06                          | 125                                       | 8.51              | 70.0            | 5999                |
|           | 65                       | 1407                      | 2.48                          | 49  | 7.64              | 85.6            | 5999                |
|           | 70                       | 422                       | 2.49                          | -103                                      | 6.39              | 69.8            | 5999                |
| 211 D 021 | 75                       | 337                       | 4.75                          | 33  | 6.45              | 71.4            | 5999                |
| 211-B-021 | 80                       | 310                       | 5.83                          | 37  | 7.25              | 74.7            | 2000                |
|           | 85                       | 236                       | 5.71                          | 36  | 8.04              | 74.9            | 2000                |
|           | 90                       | 373                       | 1.78                          | 93  | 7.18              | 81.5            | 200                 |

#### Field Measurements and Barometric Pressure

\*The value of 5999 is the upper limit of the range of the instrument.